

# Enhanced Snake Plain Aquifer Model

Version 2.1

## Uncertainty Analysis

Idaho Department of Water Resources

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## Abstract

The Enhanced Snake Plain Aquifer Model Version 2.0 (ESPAM2.0) was developed by the Idaho Department of Water Resources (IDWR), with oversight from the Eastern Snake Hydrologic Modeling Committee (ESHMC). After completion of ESPAM2.0 mistakes were identified in the water budget in the Mud Lake area. The mistakes were fixed and the model recalibrated using the repaired water budget resulting in ESPAM2.1.

During model development the ESHMC considered completing an uncertainty analysis the third highest priority in producing ESPAM2.0. The process of deciding how to evaluate predictive uncertainty was more complicated than deciding that evaluating predictive uncertainty was necessary. The ESHMC eventually chose a limited analysis that involved imposing a stress at eight locations on the eastern Snake Plain, and determining the impact of parameter uncertainty on key predictions using a procedure proposed by Doherty (2010) and Doherty and others (2010). This technique locates the maximum and minimum values for the selected prediction by adjusting model parameters, while still keeping the model calibrated. The technique identifies how well the calibration dataset constrains the selected predictions but not the probability of any one prediction being true.

The results of this analysis indicate that about 82% (14/17) of the analyses had low predictive uncertainty, about 18% (3/17) of the uncertainty analyses identified predictions with uncertainty greater than 0.10 (difference between fraction of maximized impact and minimized impact realized at the target reach). Interestingly all the predictions with high uncertainty evaluated the impact of centroids northeast of American Falls Reservoir on the near-Blackfoot-to-Minidoka reach of the Snake River; however, not all centroids northeast of American Falls Reservoir registered high uncertainty for their impact on the near-Blackfoot-to-Minidoka reach. The hydrographs of Snake River reach-gains contain significant noise (erroneous data), and the IDWR suspects this noise contributes to the observed uncertainty since the model cannot match the noise. The IDWR experimented with including both filtered and unfiltered reach-gains and found that including filtered reach-gains in the calibration dataset reduced the predictive uncertainty range by about 37%. The IDWR proposes using both filtered and unfiltered Snake River gains during model calibration in future versions of the ESPA Model.

## Introduction

The eastern Snake Plain Aquifer (ESPA) extends from Ashton, Idaho in the northeast to King Hill, Idaho in the southwest (Figure 1). The Enhanced Snake Plain Aquifer Model Version 2.0 (ESPAM2.0) was developed by the Idaho Department of Water Resources (IDWR) with oversight from the Eastern Snake Hydrologic Modeling Committee (ESHMC) to incorporate new data and model enhancements to improve the previous model (ESPAM1.1). After calibration of ESPAM2.0, mistakes in the water budget in the Mud Lake area were discovered, repaired and the model recalibrated. The resulting model is referred to as ESPAM2.1. Details of the model are provided in the Final Report (TBD).

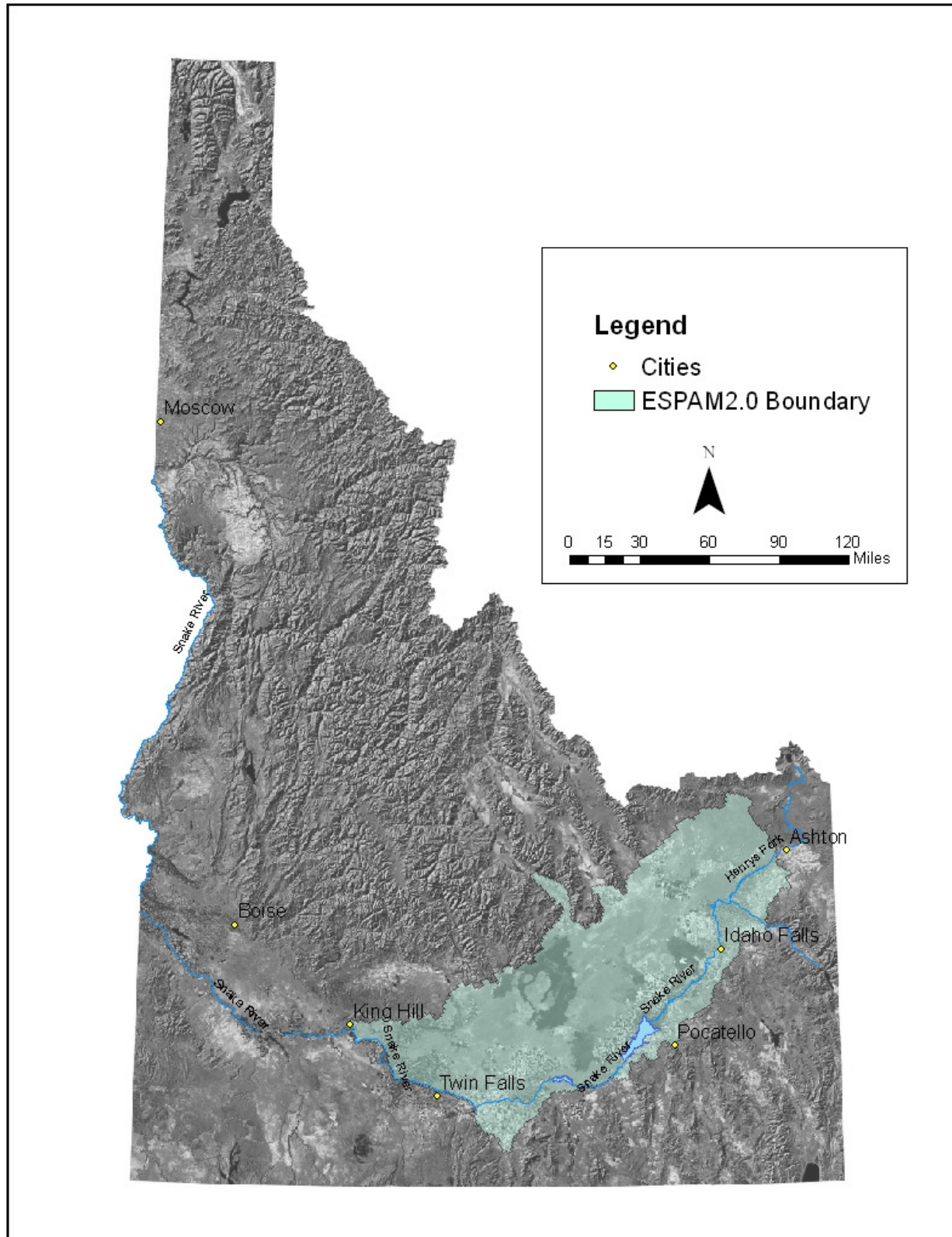


Figure 1. Location of eastern Snake Plain Aquifer.



An understanding of a model's predictive uncertainty is fundamental to the use of the model in support of decision making. Various procedures for evaluating predictive uncertainty have been suggested ranging from a sensitivity analysis to a complex Monte Carlo analysis (Doherty and others, 2010; <http://www.idwr.idaho.gov/Browse/WaterInfo/ESPAM/ESHMC%20Updated%20White%20Paper/>). In a traditional sensitivity analysis, selected model inputs are varied, and the associated changes in model outputs are recorded. Monte Carlo analyses require many model realizations, each of which is recalibrated and used to make key predictions. The set of predictions are then used to generate probability distributions. Doherty and others (2010) present a number of techniques that may be used to complete predictive uncertainty analyses.

In 2007, the ESHMC identified goals for development and calibration of ESPAM2.0, and the committee members independently ranked the components that they considered most important. Completing an uncertainty analysis was ranked as the third highest priority for ESPAM2.0. In the November 2009 ESHMC meeting, the committee chose to evaluate predictive uncertainty using PEST (Doherty, 2010) following the procedure outlined by Doherty (2003). In the February 2010 ESHMC meeting this decision was modified to use the nonlinear analysis proposed by Doherty (2010). During the March 2011 ESHMC meeting, the committee unanimously agreed to proceed with a predictive uncertainty analysis immediately after calibration of ESPAM2.0. In the June 2011 ESHMC meeting, the committee chose to reduce the scope of the analysis because an exhaustive uncertainty analysis for a complex model like the ESPAM2.0 would be time-prohibitive. The committee chose a limited predictive uncertainty analysis that involved imposing a stress at a centroid within each of eight areas on the ESPA, and determining uncertainty for the impact of the stress on two springs and two river reaches. The eight areas chosen were: Water District 100, 110, 120, 130, 140, 33, 34, and the Rexburg Bench, hereafter referred to as Water District 99, or WD099. The chosen springs were Blue Lake and Clear Lakes, and the chosen river reaches were near-Blackfoot-to-Minidoka and Ashton-to-Rexburg (Figure 2).

The uncertainty analysis commenced in August 2011 and continued until August 2012. Calibration run E120116A008, referred to as ESPAM2.0, was completed in March 2012, so several of the uncertainty analyses were conducted using a preliminary calibration run. The ESHMC concluded that one of the preliminary runs should be rerun with E120116A008 to assess the changes due to different calibration runs. While the uncertainty analysis was in progress, the ESHMC decided to further limit the scope and only analyze uncertainty at one spring, Clear Lakes, and one river reach, near-Blackfoot-to-Minidoka.

The first eight characters in the 11 character calibration run name identifies the water budget used, for example E120116A. The last three characters indicate the calibration run conducted using that particular water budget, for example 008. Thus E110712A002 is the second calibration run conducted with water budget E110712A and E120116A008 is the eighth calibration run conducted with water budget E120116A.

After calibration of ESPAM2.0, mistakes in the water budget in the Mud Lake area were discovered, repaired and the model recalibrated. The corrected water budget is E121025A and the resulting model is E121025A001, commonly referred to as ESPAM2.1.

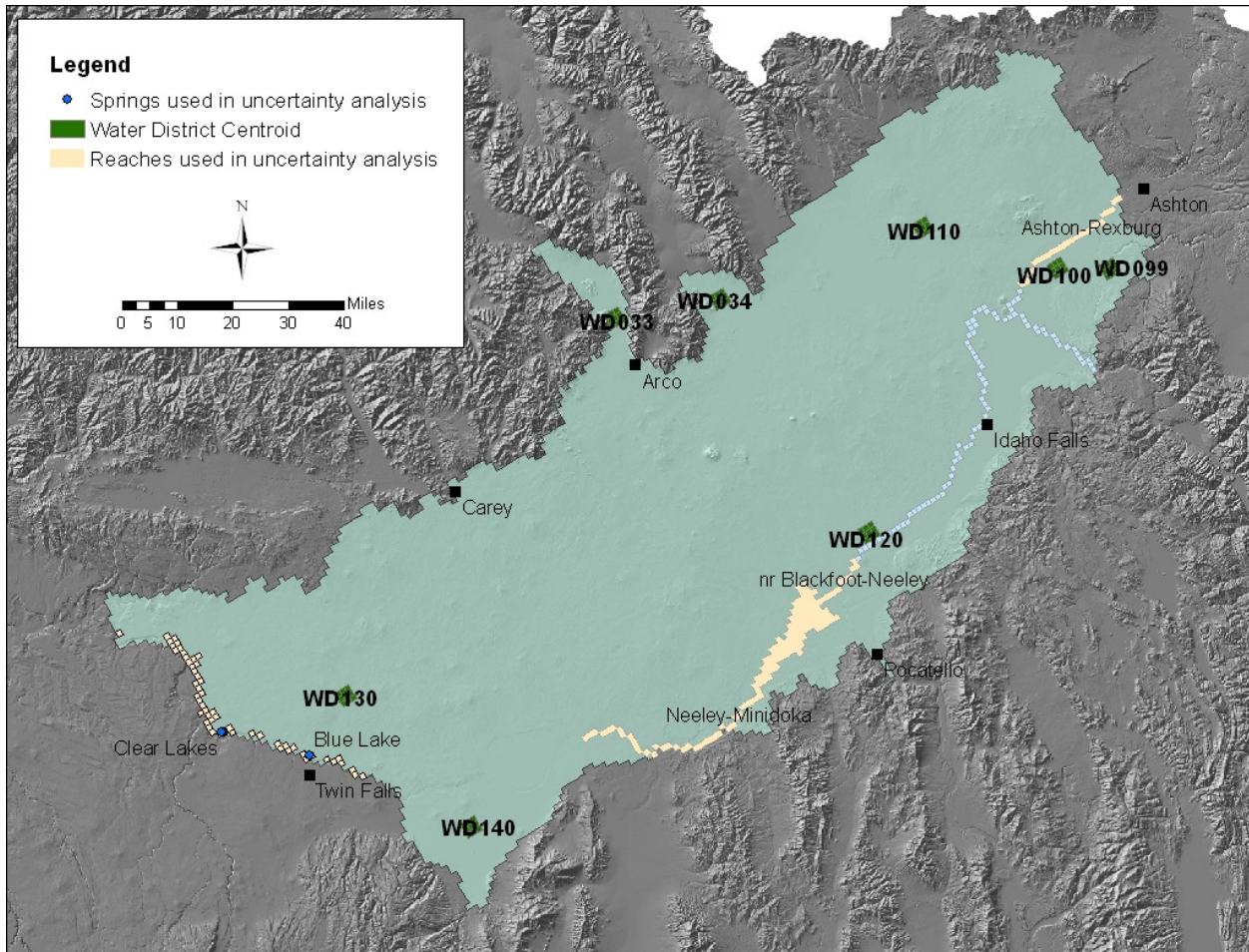


Figure 2. Water District centroids and springs and river reaches.

## Methodology

Models are calibrated by adjusting parameters to reduce the discrepancy between model outputs and field observations. The discrepancies are encapsulated in an “objective function”; defined as the weighted sum of squared differences between field observations and model outputs. Generally, the topology of the objective function in parameter space is shaped like a long, narrow valley of nearly equal objective function values, with the objective function minimum placed somewhere in the bottom of the valley. The parameter distribution that describes this long narrow valley calibrates the model. Thus the model calibration is not unique. Normally, as in the case of ESPAM2.1, a single set of parameters is chosen as “The Model” (i.e. E121025A001 ) and used to make predictions. Given this long narrow valley in the objective function, an obvious question is, “what would have been the prediction if another set of parameters lying along the valley bottom were chosen?” An effective way to investigate the variability of a model prediction while maintaining goodness of fit between model outputs and field observations is with a constrained maximization/minimization technique similar to the procedure proposed by Doherty (2010) and Doherty and others (2010). This technique keeps the model calibrated while identifying the

critical values along the parameter-space valley where the selected prediction is either maximized or minimized.

The following is the procedure used to identify how correlations in adjustable parameters can impact the selected predictions.

- 1) Identify the centroid of the irrigated lands within the water district or selected areas. The centroids are not intended to represent the water districts in this analysis, they are intended to be widely distributed on the ESPA, and constrained to areas where irrigation is taking place.
- 2) Prepare the model files necessary to run the prediction, including a stress file constructed using the 3x3 cell centroid identified in step one (1).
- 3) Make a copy of the PEST control file. The PEST control file contains all of the adjustable parameters and their bounds, and all the field observations. Since the entire PEST control file is copied, every parameter adjustable in a calibration run will also be adjustable in the predictive uncertainty analysis, and every field observation used as a calibration target will also be used as a target in the predictive uncertainty analysis. The following adjustments (items 4 – 12) were made to the PEST control file.
- 4) Replace the word 'regularization' with the word 'prediction' on the third line.
- 5) Increase the number of observations by one (1) because the prediction will be a new observation.
- 6) Increase the number of observation groups by one (1) because there will now be an observation group 'predict'.
- 7) Increase the number of instruction files by one (1) because PEST will now be required to monitor the prediction.
- 8) Add 'predict' to the list of observation groups.
- 9) Add an observation representing the prediction to the observation section. Any weight and target observation value can be provided because PEST ignores the weight and target observation value for any observation in the 'predict' group when it is run in predictive analysis mode.
- 10) Change the model command line to reflect the name of the batch file used to run the model and the prediction.
- 11) Add the name of the new instruction file and the output file it will read to the list of files used to read model output.
- 12) Add a 'predictive analysis' section to the control file. This will include NPREDMAXMIN, PD0, PD1, and PD2. NPREDMAXMIN instructs PEST to either maximize (+1) or minimize (-1) the prediction of interest. PD0 is a value of the objective function (phi) which is considered calibrated. Because the shape of the PD0 envelope can be complex, it is extremely hard for PEST to identify a parameter set that lies exactly on the boundary. Therefore, PD0 must be greater than phi for the calibrated model, but only slightly greater. The value supplied for PD1 (which must be slightly greater than PD0) is a value PEST will consider "close enough". If the sum-of-the-squared residuals is above PD2, PEST tries to minimize the objective function until the objective function is below PD2, at which point PEST begins searching for either the maximum or minimum value for the prediction at PD0.

Thus, during a predictive uncertainty analysis run, PEST will: A) run MKMOD, B) run MODFLOW, C) compare model output with field observations in the same manner as in a calibration run, D) compare

the sum-of-the-squared residuals ( $\phi$ ) from this run with PD0, E) make a model run in superposition mode containing only the 3x3 stress file constructed during steps 1 and 2, F) collect the predicted impact at the target spring or river reach, and G) compare this prediction with the previous maximum (or minimum) prediction and save the value, if it is a new maximum (or minimum) and if  $\phi$  for this run is less than PD1.

Doherty (2010) recommends that  $\phi$  from the calibrated model  $< PD0 < PD1 < PD2$  and that PD0 should only be slightly larger than  $\phi$  for the calibrated model (1 or 2% larger). Doherty (2010) further states that PD1 should only be slightly larger than PD0 (1 or 2% larger), and PD2 should be generally 1.5 to 2 times PD0. Table 1 shows the  $\phi$ , PD0, PD1, and PD2 values used in this scenario with calibration run E120116A008 and E121025A001. In both cases PD0 is 1.5 % larger than  $\phi$ , PD1 is 1.5 % larger than PD0, and PD2 is 1.5 times larger than PD0. Functionally, assigning PD0 and PD1 values a little larger than the calibrated  $\phi$  allows PEST enough latitude to explore parameter space and locate correlated parameters that might impact the selected prediction.

**Table 1.  $\phi$ , PD0, PD1, and PD2 values used for predictive uncertainty analysis with calibration run E120115A008 and E121025A001.**

Model	$\phi$	PD0	PD1	PD2
E120116A008	26517	26915	27312	39776
E121025A001	26613	27012	27417	39919

A comprehensive predictive uncertainty analysis would yield a probability distribution of the difference between model output and actual aquifer response for the selected predictions. To accomplish such a goal, the analysis would have to interrogate all sources of uncertainty including conceptual model uncertainty, model parameter uncertainty and measurement uncertainty. The maximization/minimization procedure employed in this analysis provides some measure of predictive uncertainty while still being performable within a reasonable time frame. In lieu of a probability distribution, the maximization/minimization analysis provides upper and lower bounds for the probability distribution, with output from “The Model” supplying the most likely outcome. The maximization/minimization approach employed in this analysis addresses sources of uncertainty due to correlated parameters, it does not address conceptual model errors or the impact of measurement error; however, confidence in field observations may be reflected in the assigned measurement weights.

## Results

As shown in Table 2, 19 analyses have been completed to evaluate the maximum and minimum impact of stress applied at the eight centroids on Clear Lakes and the near-Blackfoot-to-Minidoka reach of the Snake River as well as one analysis to determine the maximum and minimum impact for the centroid of Water District 130 on the Ashton-to-Rexburg reach. The column in Table 2 titled “Calibrated Impact” represents the fraction of the total impact realized in the target reach at steady state.

**Table 2. Constrained maximized/minimized uncertainty analyses conducted with ESPAM2.0 and 2.1. Calibrated Impact represents the fraction of the total impact at the centroid that was realized in the target reach.**

Centroid	Reach	Calibrated Impact	Maximized Impact	Minimized Impact	Range	Model Version
WD033	Clear Lakes	0.01	0.01	0.01	0.001	E120116A008
WD033	nr Blackfoot-Minidoka	0.61	0.62	0.61	0.009	E120116A008
WD034	Clear Lakes	0.03	0.03	0.00	0.030	E110712A002
WD034	nr Blackfoot-Minidoka	0.68	0.86	0.32	0.537	E120116A008
WD034	nr Blackfoot-Minidoka	0.49	0.76	0.43	0.331	E121025A001
WD099	Clear Lakes	0.00	0.00	0.00	0.001	E120116A008
WD099	nr Blackfoot-Minidoka	0.16	0.30	0.03	0.267	E120116A008
WD100	Clear Lakes	0.00	0.00	0.00	0.000	E120116A008
WD100	nr Blackfoot-Minidoka	0.20	0.20	0.20	0.000	E120116A008
WD110	Clear Lakes	0.00	0.00	0.00	0.000	E110712A002
WD110	nr Blackfoot-Minidoka	0.26	0.27	0.26	0.006	E120116A008
WD120	Clear Lakes	0.00	0.01	0.00	0.005	E110712A002
WD120	nr Blackfoot-Minidoka	0.67	0.91	0.55	0.363	E120116A008
WD130	Ashton-Rexburg	0.01	0.01	0.01	0.000	E120116A008
WD130	Clear Lakes	0.07	0.07	0.07	0.004	E110712A002
WD130	Clear Lakes	0.08	0.08	0.07	0.012	E121025A001
WD130	nr Blackfoot-Minidoka	0.22	0.22	0.15	0.067	E120116A008
WD140	Clear Lakes	0.05	0.05	0.04	0.002	E120116A008
WD140	nr Blackfoot-Minidoka	0.35	0.35	0.35	0.003	E120116A008

The column in Table 2 titled “Range” represents the difference between the “Maximized Impact” and “Minimized Impact”. Impact differences are used in this table rather than percent change because, from a model development perspective, uncertainty will always exist, thus the more meaningful metric is the fraction of the total impact, not the percent change. For example, the Calibrated Impact for the centroid of WD120 on Clear Lakes is 0.005, the Maximized Impact is 0.009, and the Minimized Impact is 0.004. The Maximized Percent Change is 80%  $((0.009-0.005)/0.005)$  and the Minimized Percent Change is -20%  $((0.004-0.005)/0.005)$ . The Predictive Uncertainty range in percentage is 100% (80% - (-20%)). In this example, 100% uncertainty sounds problematic; however, this analysis indicates that the model cannot remain calibrated and increase the impact at Clear Lakes to more than 0.009. Unless something is wrong with the hydrogeologic conceptualization upon which ESPAM2.0 and ESPAM2.1 are based, the impact for the centroid of WD120 upon Clear Lakes will remain small. In this example, 100% uncertainty does not accurately reflect the fact that we are certain that at least 99% of the impact is not realized at Clear Lakes. It is only after the impact differences (range) becomes large that the uncertainty becomes a weakness worth pursuing during model development.

The majority of the analyses presented in Table 2 conducted with ESPAM2.0 and earlier models resulted in relatively tight predictive uncertainty ranges. Three analyses resulted in ranges greater than 0.10: The



centroid of WD034 to near-Blackfoot-to-Minidoka, the centroid of WD099 to near-Blackfoot-to-Minidoka and the centroid of WD120 to near-Blackfoot-to-Minidoka (Figure 2). All of these Water District centroids are northeast of American Falls Reservoir, and all of these analyses involve the near-Blackfoot-to-Minidoka reach. The Snake River reach-gain observations contain significant noise (erroneous data) as shown in Figure 3. The noisy data may be allowing PEST some latitude because the model output will never successfully match the noise.

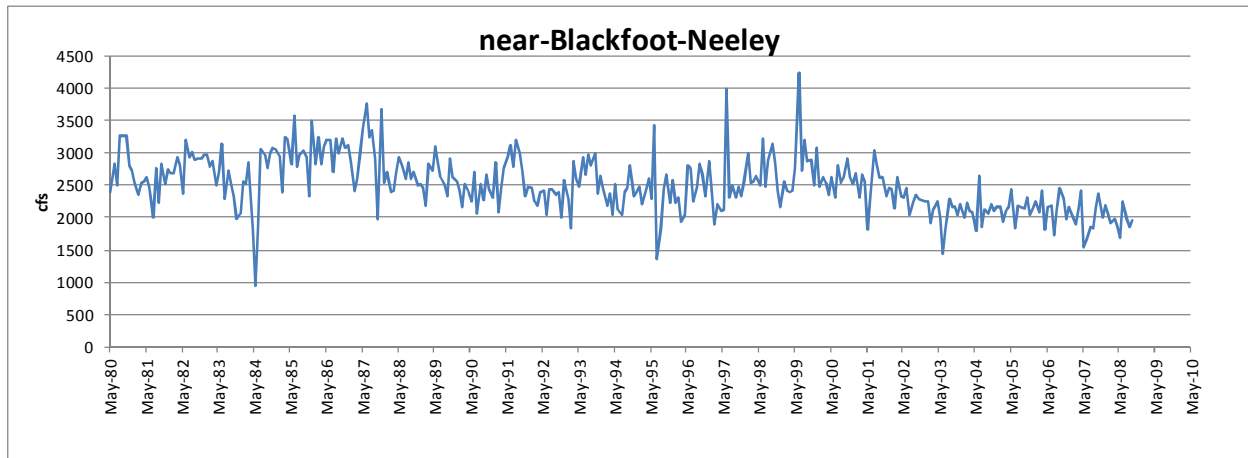


Figure 3. Observed reach-gains between the near Blackfoot and the Neeley gages.

Mistakes were identified in all water budgets used in Table 2 up to E121025A. After correcting these mistakes and producing a new water budget (E121025A) and calibrating ESPAM2.1 (E121025A001). The ESHMC asked IDWR to conduct predictive uncertainty analyses using ESPAM2.1 to compare with previously conducted analyses. The IDWR selected the impact of the centroid for WD034 on near-Blackfoot-to-Minidoka and the impact for the centroid of WD130 on Clear Lakes. These analyses provided comparisons with two different water budgets (E110712A and E120116A), two different target reaches (near-Blackfoot-to-Minidoka and Clear Lakes), an analysis that has a range greater than 0.10 and an analysis that has a range less than 0.10. These analyses are highlighted in gray in Table 2.

In some respects the comparison analyses conducted with ESPAM2.1 are similar:

- Both runs conducted using the WD130 centroid and Clear Lakes indicate that the calibration data constrained the prediction,
- Both runs conducted using the centroid for WD034 and the near-Blackfoot-to-Minidoka reach indicated that the calibration data did not constrain the prediction as tightly as desired.

These similarities show that the elevated uncertainty associated with the near-Blackfoot-to-Minidoka exists after repairing the Mud Lake mistakes.

In some respects the comparison analyses identify differences:

- The ESPAM2.1 impact of the WD130 centroid on Clear Lakes increased from 0.07 to 0.08 and the range increased from 0.004 to 0.012.
- The ESPAM2.1 impact of the WD034 centroid on near-Blackfoot-to-Minidoka decreased from 0.68 to 0.49 and the range decreased from 0.537 to 0.331.

The change in impact with ESPAM2.1 identified in both analyses indicates that the model adjusted physical properties to adapt to changes in where stress is applied in the model. These changes also resulted in changes in predictive uncertainty as evidenced by the change in range. Adjustments such as this are expected in response to changes in the water budget.

### Filtered/Unfiltered Reach-Gain Test

The fact that high predictive uncertainty is tied to river reach-gains suggests that the reach-gain calibration targets need to be improved. A Butterworth filter (Butterworth, 1930) is available with PEST and can be applied to remove the noise from the observation data. Even though model output will not contain noise, model output will need to be processed with the same filter prior to comparison with the filtered observations. The noise associated with these reach-gain data suggests that the model is not currently supplied with detailed information concerning seasonal fluctuations through the reach-gain data, and filtering these data will not improve the seasonal information available to the model.

In an attempt to evaluate the impact of data noise on predictive uncertainty, the IDWR conducted an analysis using both filtered and unfiltered reach-gains. This analysis was conducted with ESPAM2.0 (E120116A008) prior to the repair of the Mud Lake mistakes. The steps involved in conducting the analysis include:

1. Interpolate reach-gain data to a constant sampling interval
2. Determine the cutoff frequency
3. Add filtered reach-gains to the calibration targets.
4. Recalibrate the model using both filtered and unfiltered Snake River reach-gain targets.
5. Rerun at least one of the predictive uncertainty analyses.

The Butterworth filter will only work on a time series with a constant sample interval. The reach-gain data is monthly, and months do not have a constant number of days. Therefore, the field observations must be interpolated to a constant interval. The chosen interval was 30.4 days.

The Butterworth filter may be used as a high pass, low pass or band pass filter. The data in Figure 3 contains high frequency noise, so the filter should be designed to remove the high frequency noise and pass the low frequency data through for use in model calibration. An event that occurs once a year has a frequency of 1 per year or 1/365.25 days. The noise in Figure 3 has a frequency of at least 1/365.25 days. This cutoff frequency, or the boundary between the pass band and the stop band, must be identified and provided to the filter.

Figure 4 shows the field observations, interpolated data, and data filtered with cutoff frequencies of 1/365.25 day (1 per 1 year), 1/730.5 day (1 per 2 years) and 1/1826/25 day (1 per 5 years). The cutoff frequency of 1 per 5 years does a better job of removing the noise than the 1 per 1 year or 1 per 2 year cutoffs.



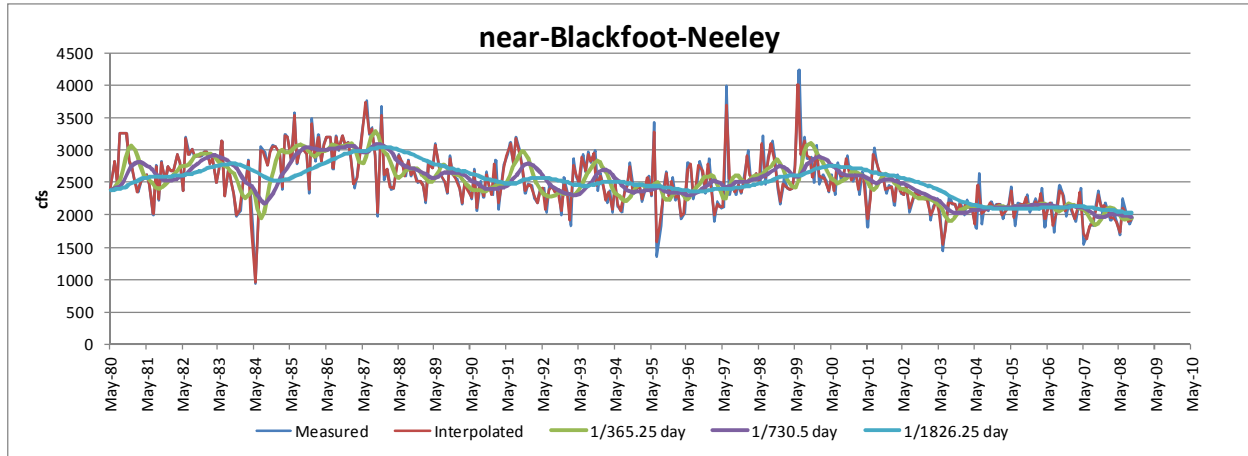


Figure 4. Measured, interpolated, and filtered data for near -Blackfoot-Neeley reach-gains.

The reach-gains filtered using a cutoff frequency of 1/5yr were added to the calibration targets and E120116A008 was recalibrated resulting in model E120116Afilt. Table 3 shows the impact on the predictive uncertainty range. The predictive uncertainty range was reduced by about 37%.

Table 3. Results of the IDWR filtered/unfiltered reach-gain test.

Centroid	Reach	Calibrated Impact	Maximized Impact	Minimized Impact	Range	Model Version
WD034	nr Blackfoot-Minidoka	0.682	0.862	0.324	0.537	E120116A008
WD034	nr Blackfoot-Minidoka	0.542	0.812	0.475	0.338	E120116Afilt

## Summary, Conclusions and Recommendations

A comprehensive predictive uncertainty analysis could not be conducted in a reasonable timeframe, so the ESHMC chose to conduct a maximization/minimization uncertainty analysis. In lieu of a probability distribution, the maximization/minimization analysis provides upper and lower bounds for the probability distribution, with output from the ESHMC-chosen calibrated model supplying the most likely outcome.

All of the analyses with a range greater than 0.10 involve the near-Blackfoot-to-Minidoka reach. This indicates that the available data do not adequately constrain the model calibration concerning this prediction. The IDWR recommends that the reach-gain targets should include both filtered and unfiltered reach-gains for future calibrations of ESPAM and that the reach-gain data be analyzed in an attempt to determine the cause of the noise, and remove the noise, if possible.

None of the analyses involving Clear Lakes resulted in significant uncertainty. Perhaps this is because the total impact at Clear Lakes is necessarily small, so the net change cannot be large, or perhaps this is

because there is less noise in the spring discharge observations, and the available data adequately constrain the model calibration.

None of the analyses involving centroids within Water District 130 or Water District 140 resulted in significant uncertainty. A possible explanation for this is that most of the impact is dispersed amongst the springs and cannot be shifted elsewhere, if true, the available data are adequately constraining the model calibration.

The impact from centroids within Water District 100 and Water District 110 showed very little uncertainty. Perhaps this is because the model will not calibrate unless a significant portion of the impact from these districts is absorbed by the Ashton-to-Rexburg reach, if so, the available data adequately constrain the model calibration.

## Appendix Descriptions

Appendix A contains a map showing the centroid and spring or river reach in which the impact is observed for each of the 19 analyses included in Table 2. Each map is followed by pie charts illustrating how the steady state impact was apportioned between the river reaches and springs: 1) for the calibrated model and for the minimum prediction, and 2) for the calibrated model and for the maximum prediction. Bar charts illustrating fractional change in the adjustable parameters for each prediction are also included. The fractional change was computed by:

$$(prediction - calibration) / calibration$$

Where: *prediction* is the parameter value used in the maximum/minimum prediction model and *calibration* is the parameter value used in the calibrated model.

Appendix B contains maps pie charts, and bar charts similar to Appendix A for the analysis included in Table 3. Appendix C contains a list of the adjustable parameters. Appendix D contains a color ramp that can be used to relate the colors in the pie charts to individual springs and river reaches. Appendix E contains reviewer comments followed by the IDWR's response.

## References

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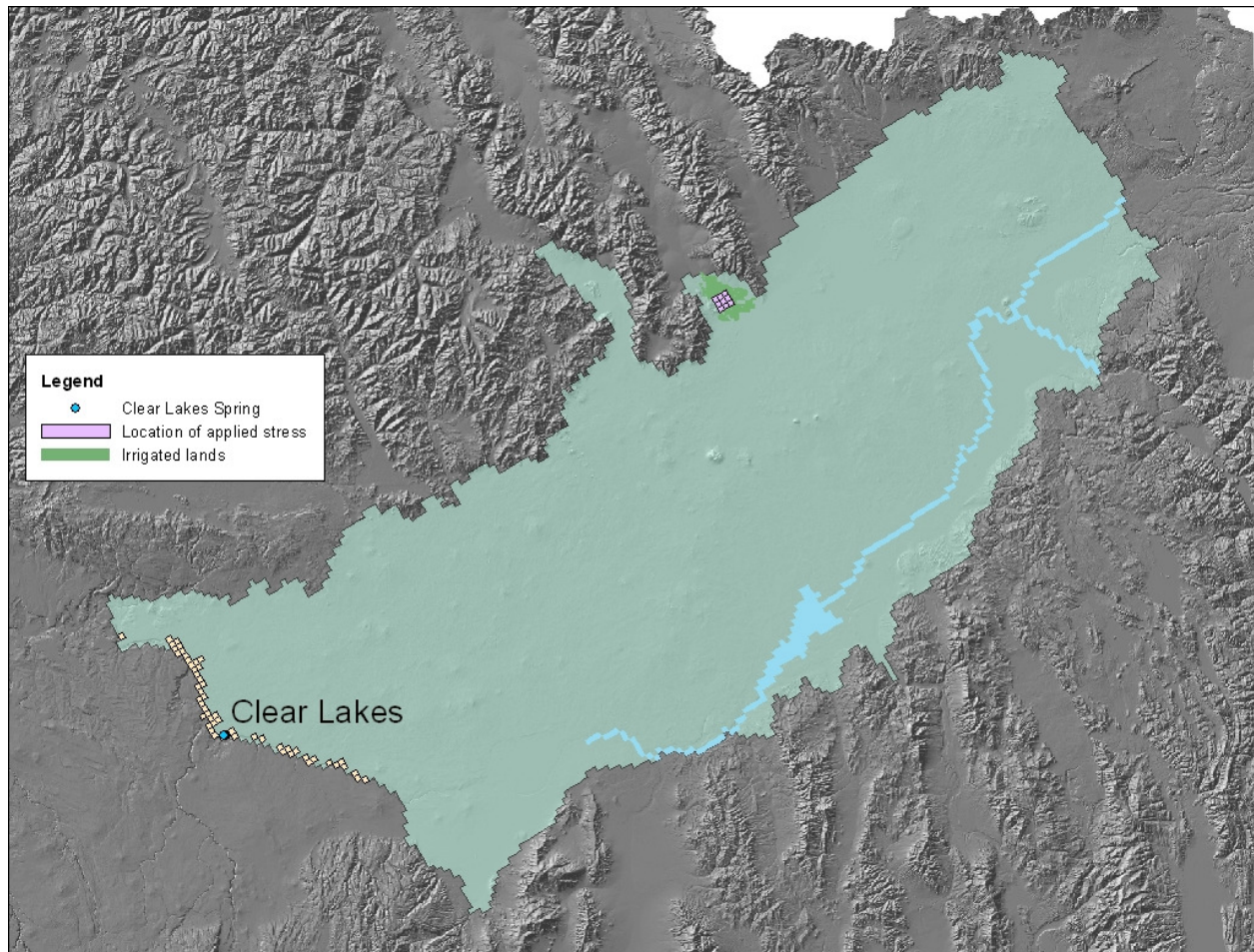
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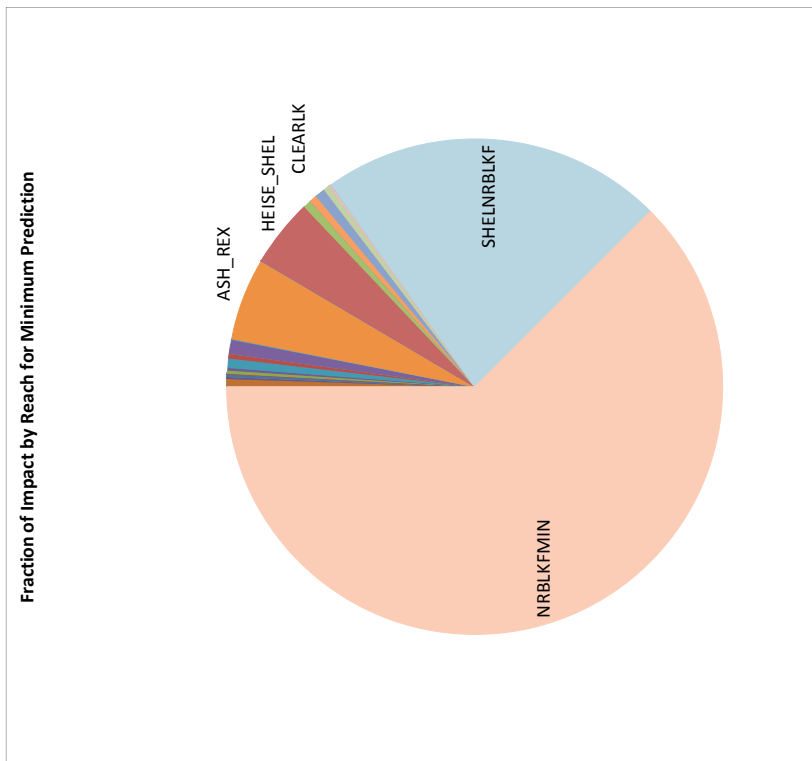
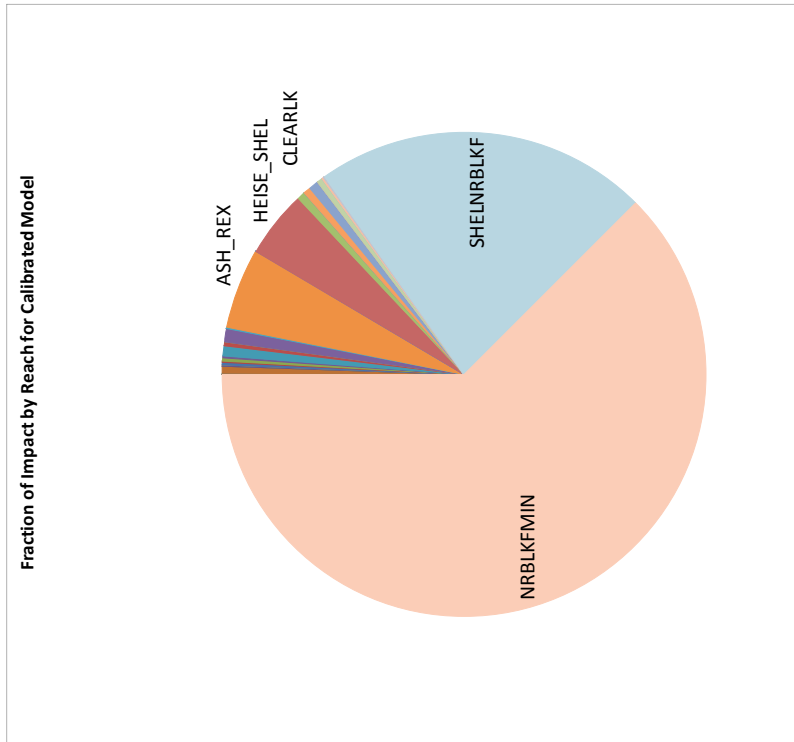
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## **Appendix A; Maps, Pie Diagrams and Bar Charts**

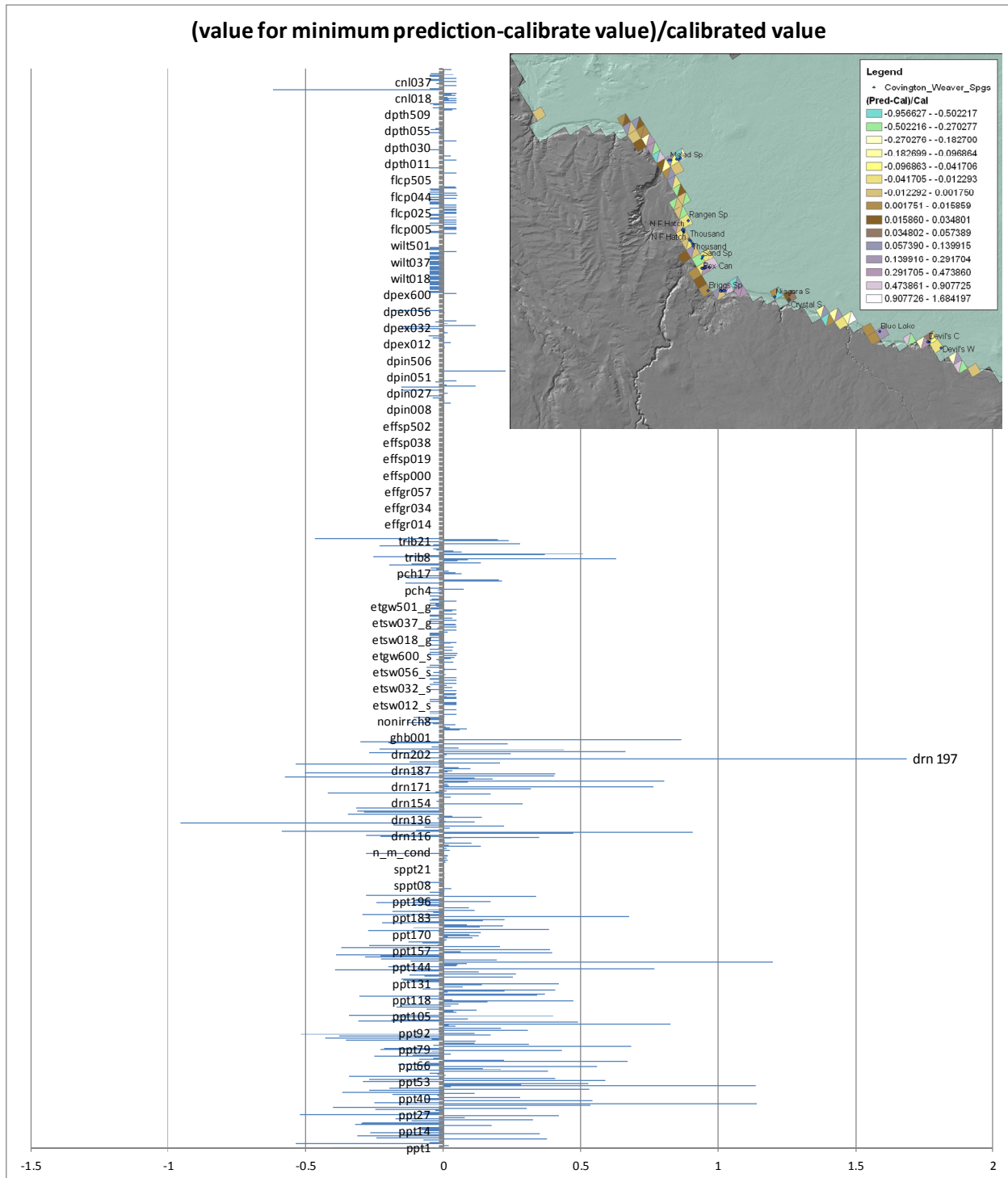
Impact of Water District 33 on Clear Lakes using calibration run E120116A008.



Impact of Water District 33 on Clear Lakes using calibration run E120116A008.

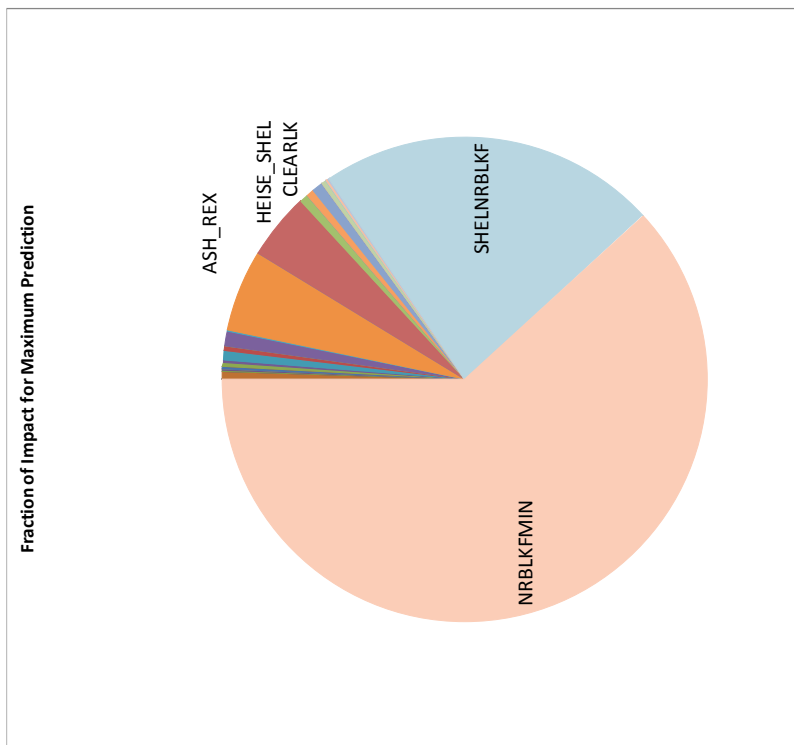
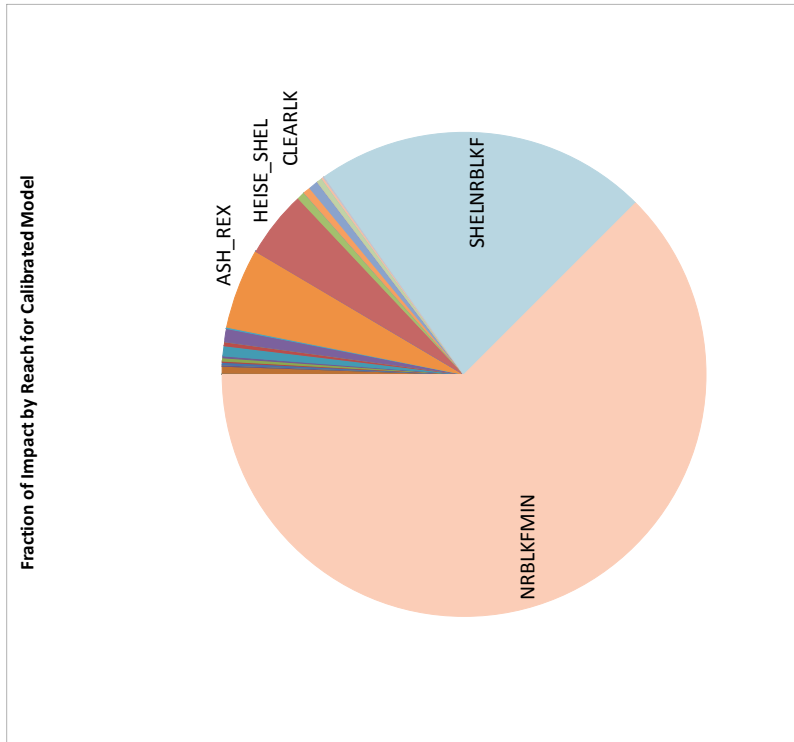


Impact of Water District 33 on Clear Lakes using calibration run E120116A008.

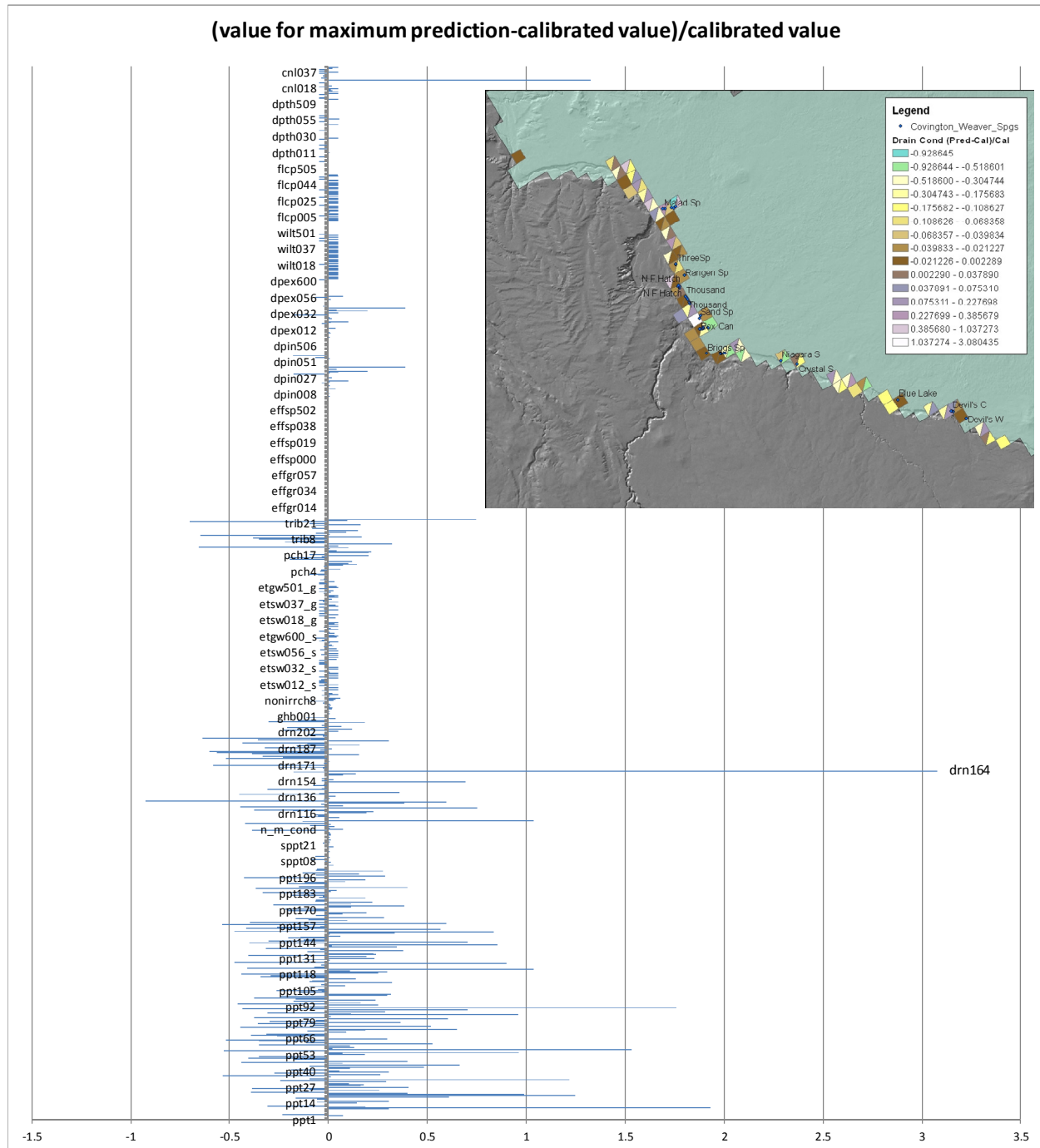




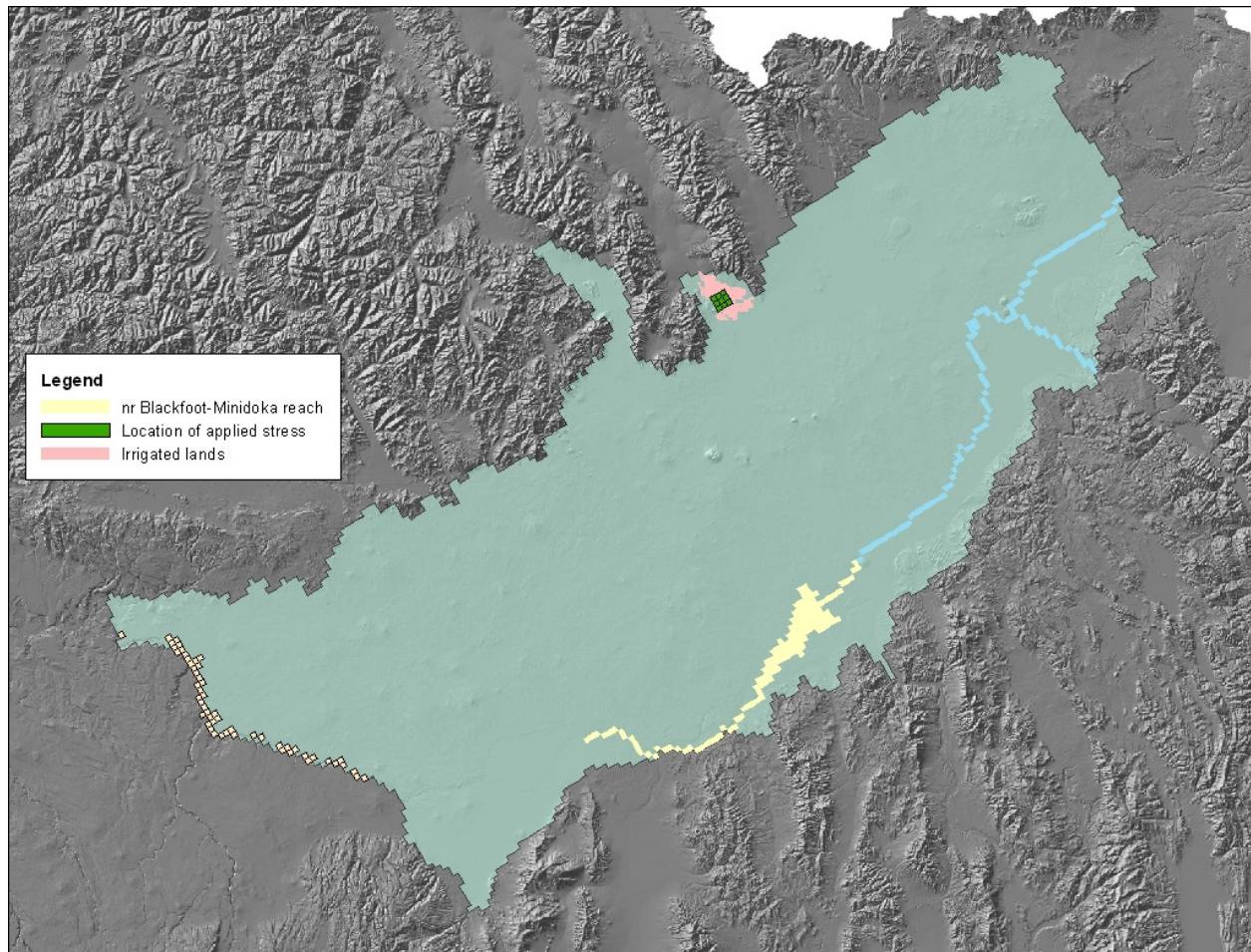
Impact of Water District 33 on Clear Lakes using calibration run E120116A008.



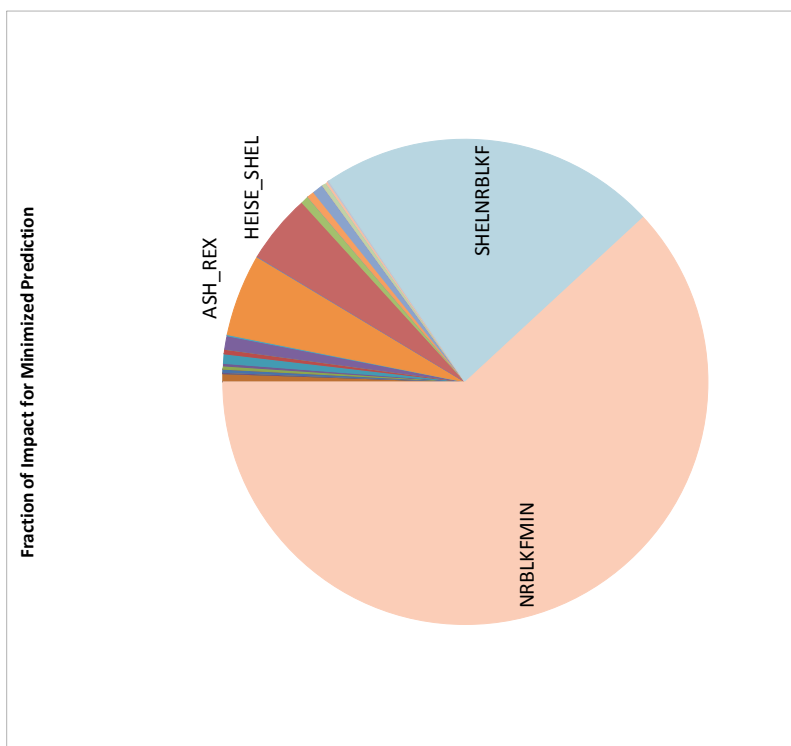
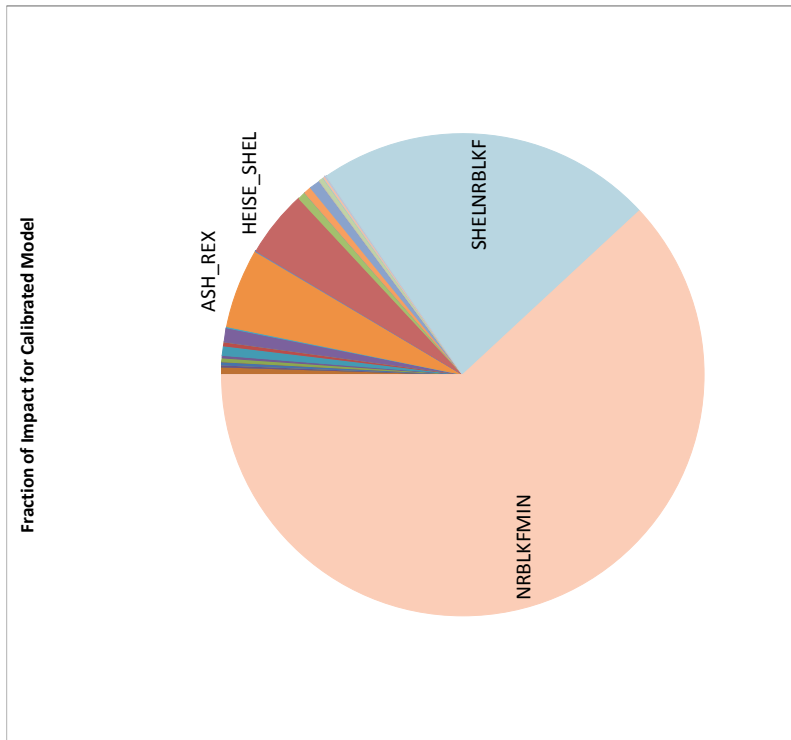
Impact of Water District 33 on Clear Lakes using calibration run E120116A008.



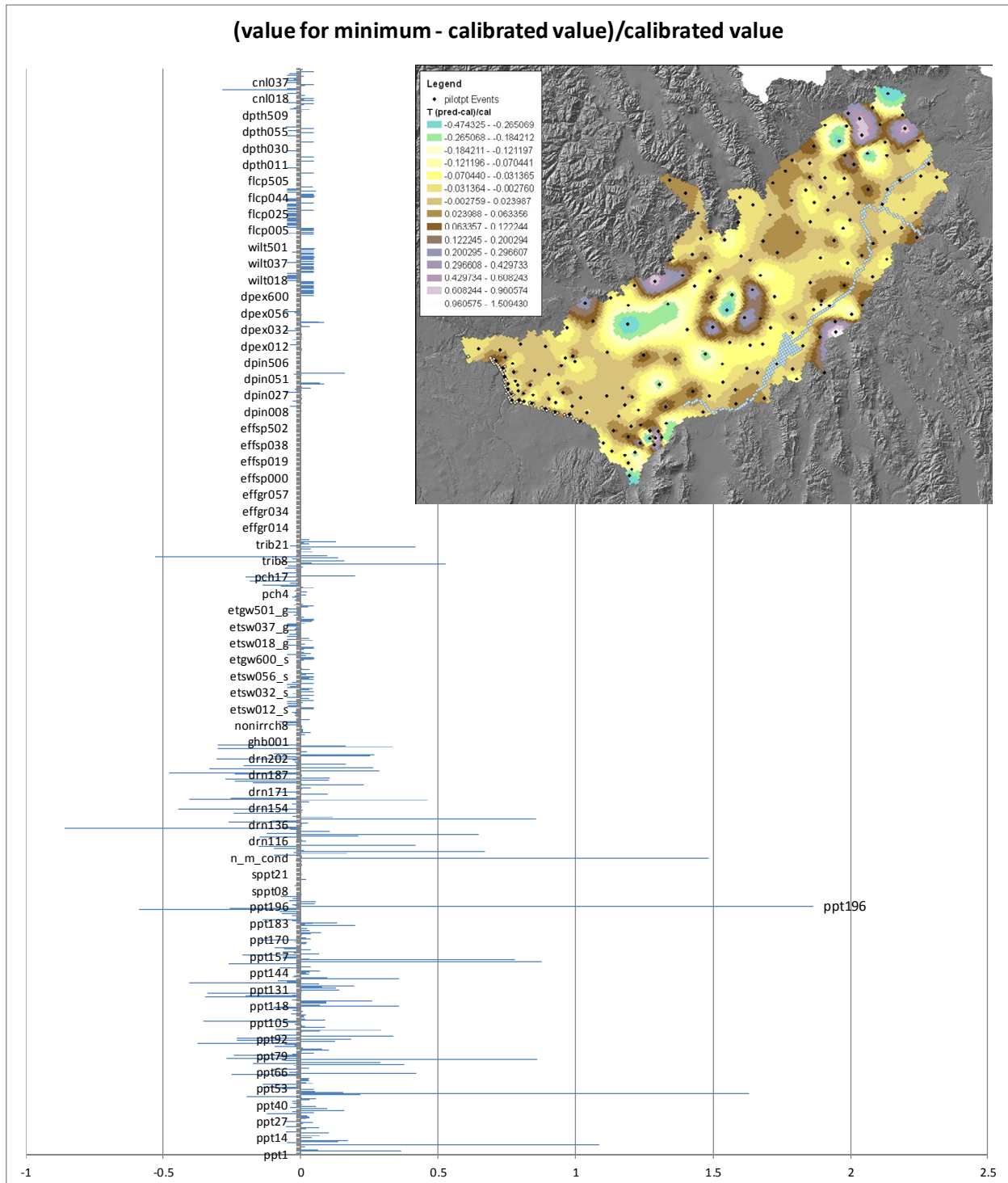
Impact of Water District 33 on nr Blackfoot-Minidoka using calibration run E120116A008.



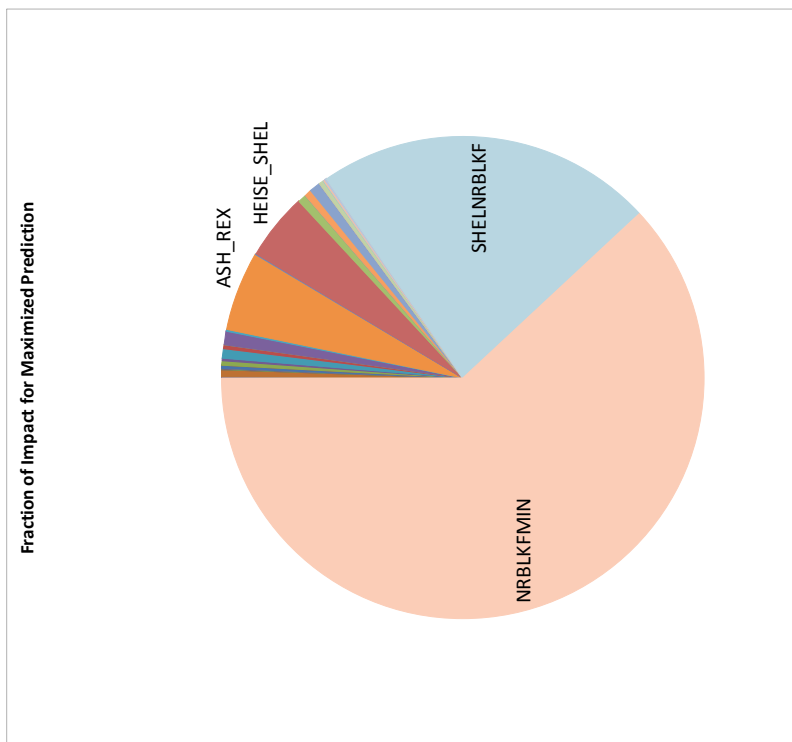
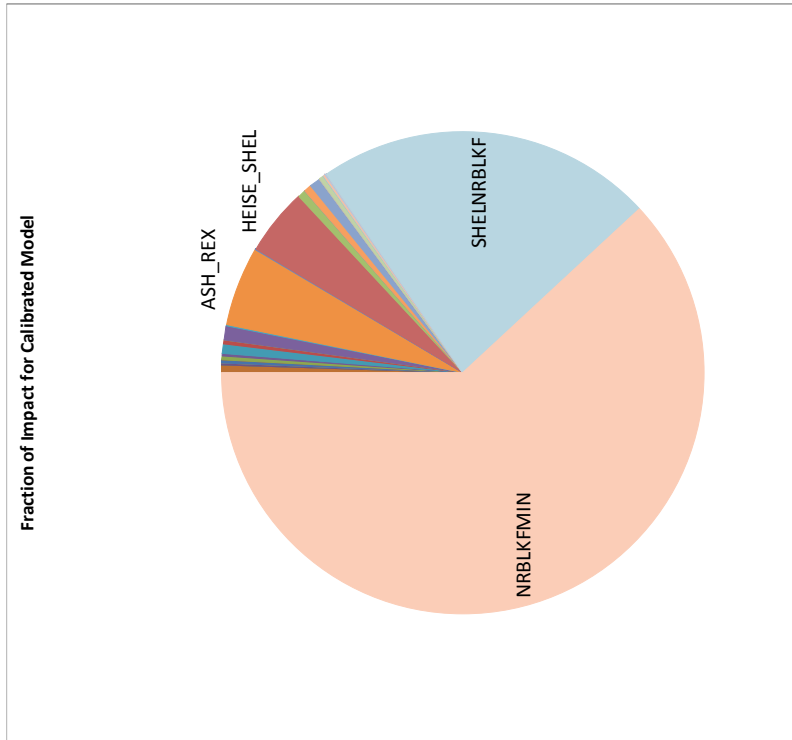
Impact of Water District 33 on nr Blackfoot-Minidoka using calibration run E120116A008.



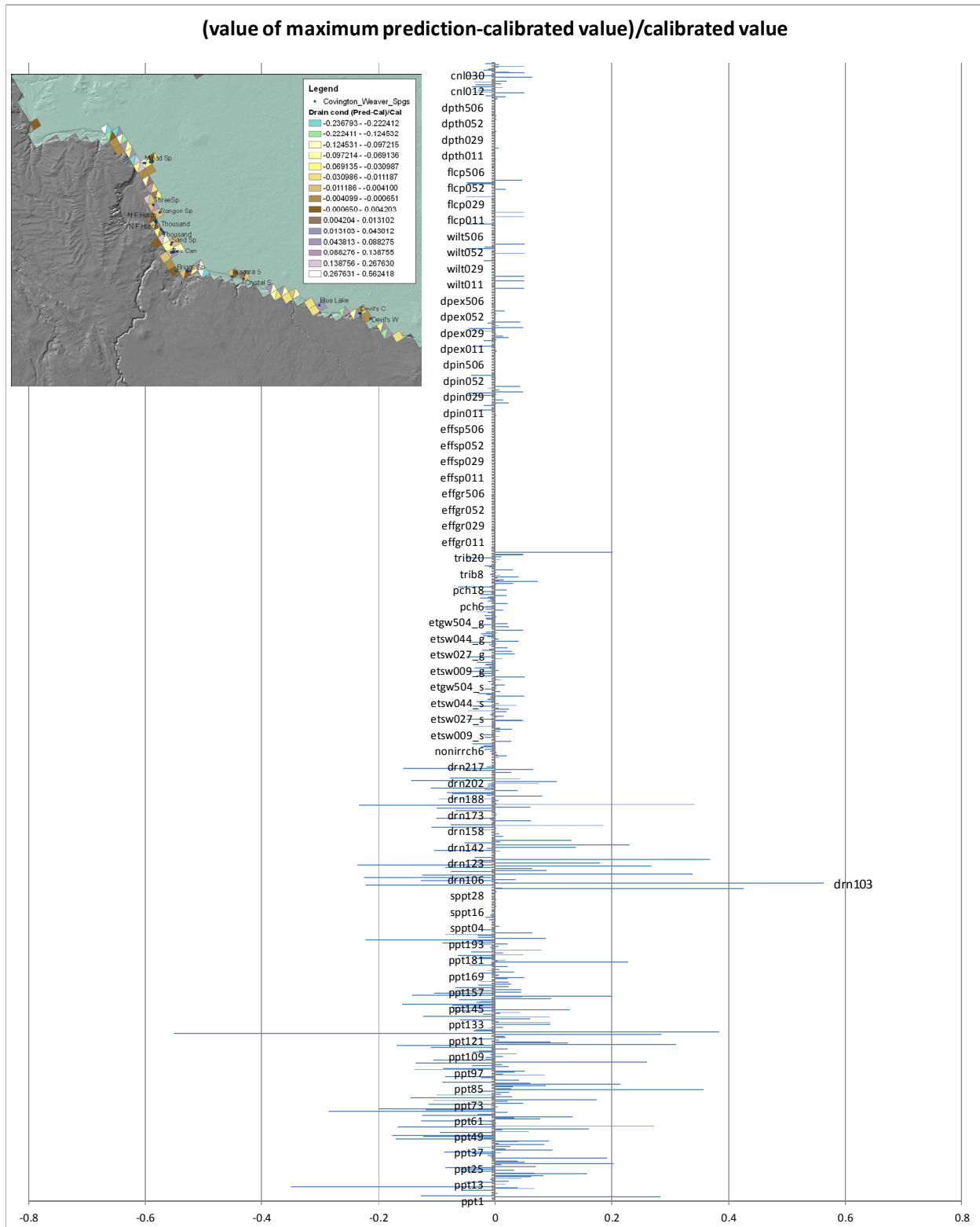
Impact of Water District 33 on nr Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 33 on nr Blackfoot-Minidoka using calibration run E120116A008.

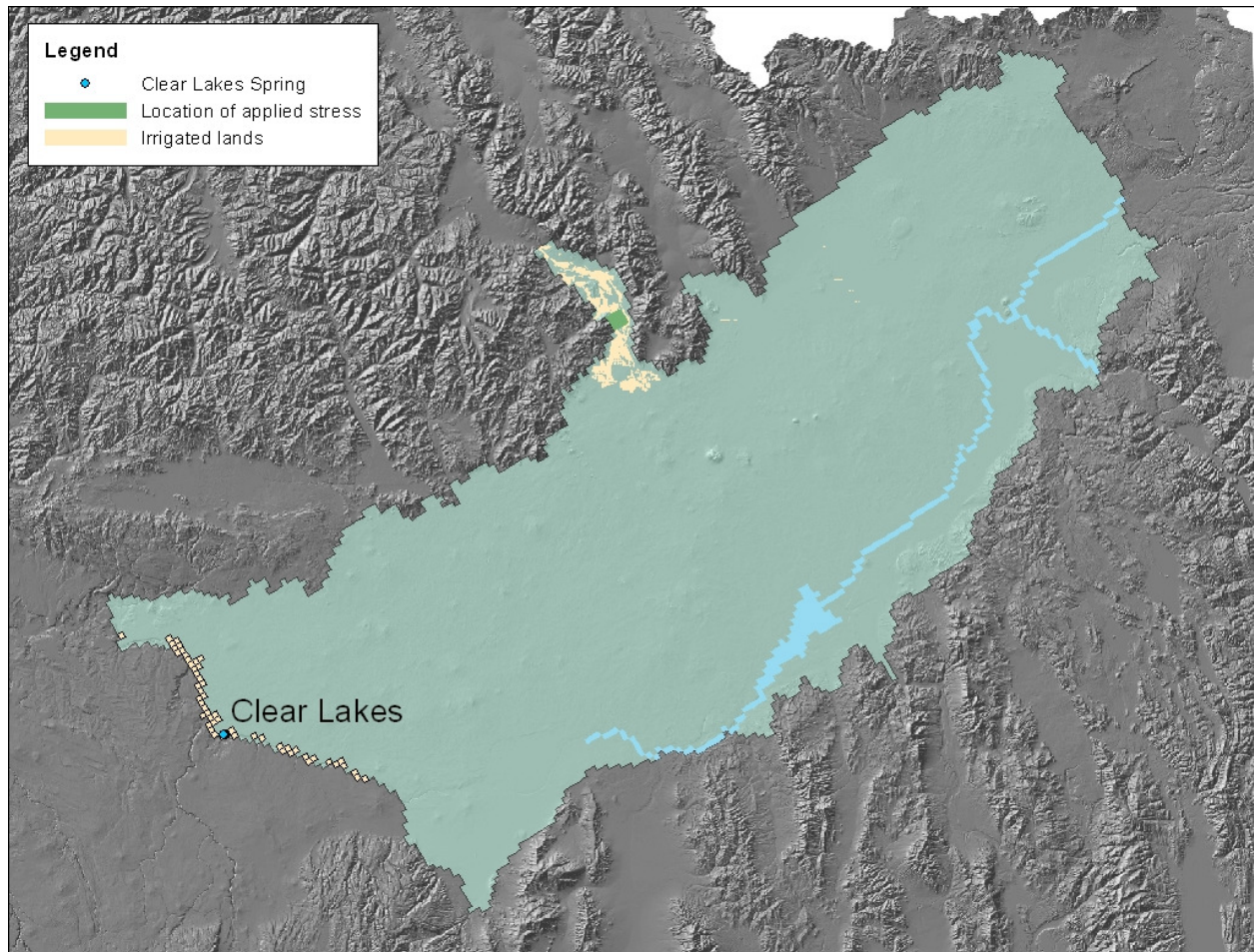


Impact of Water District 33 on nr Blackfoot-Minidoka using calibration run E120116A008.

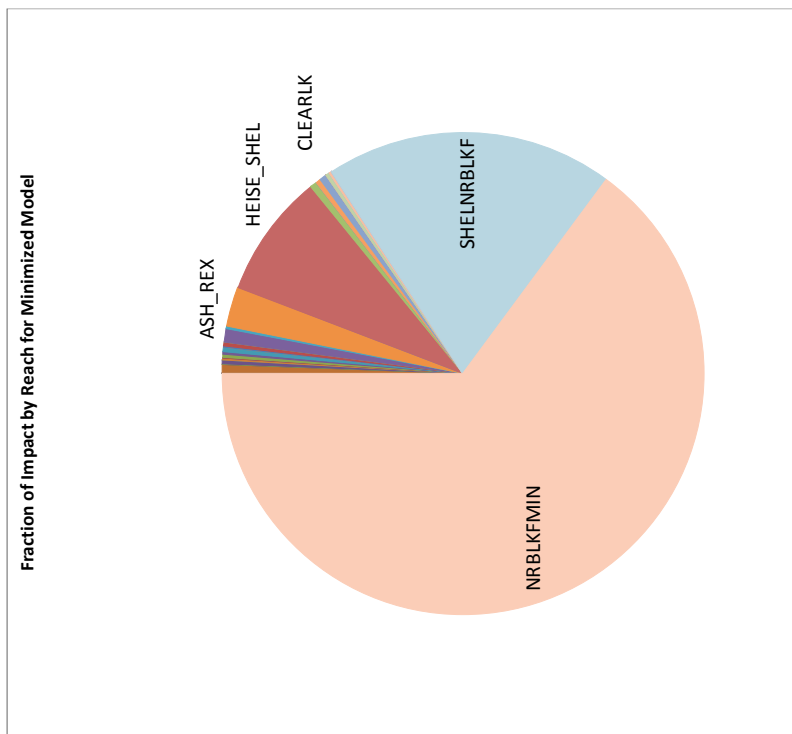
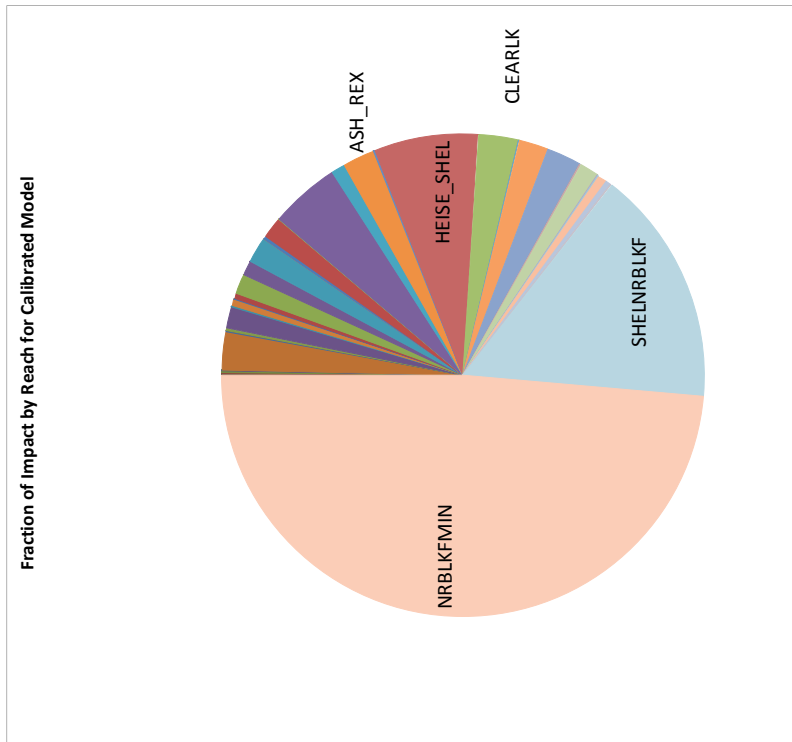




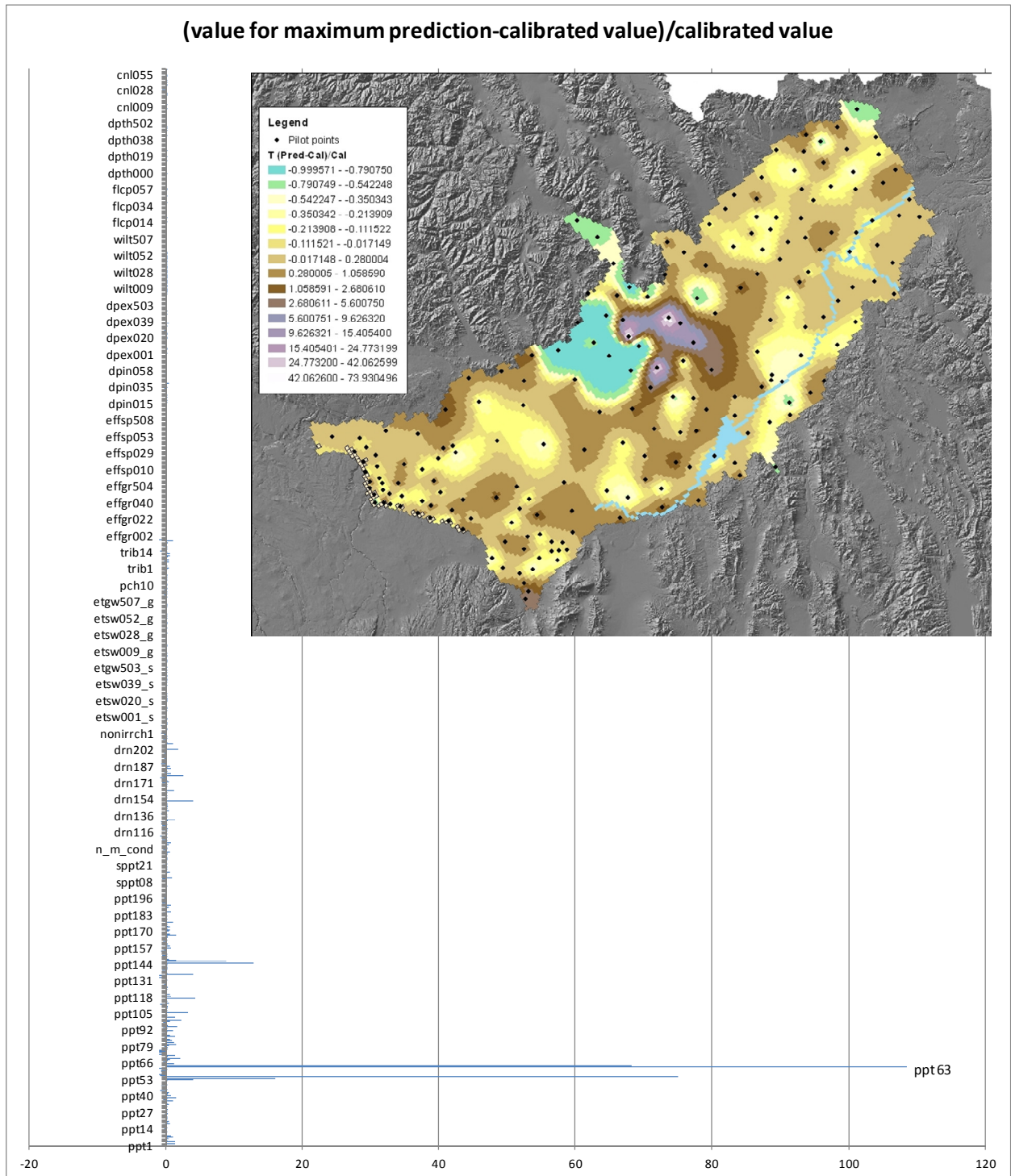
Impact of Water District 34 on Clear Lakes using calibration run E110712A001.



Impact of Water District 34 on Clear Lakes using calibration run E110712A001.

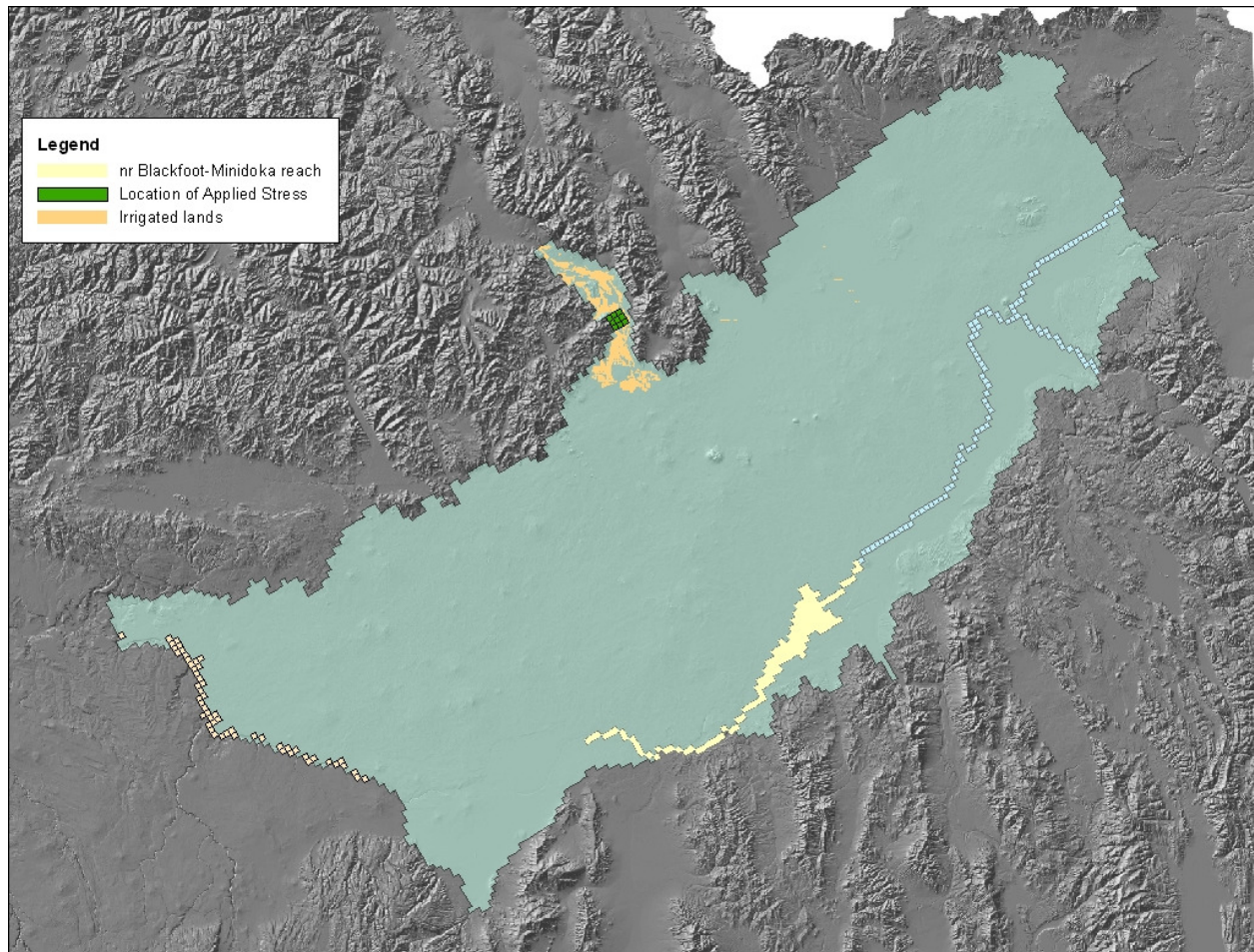


Impact of Water District 34 on Clear Lakes using calibration run E110712A001.

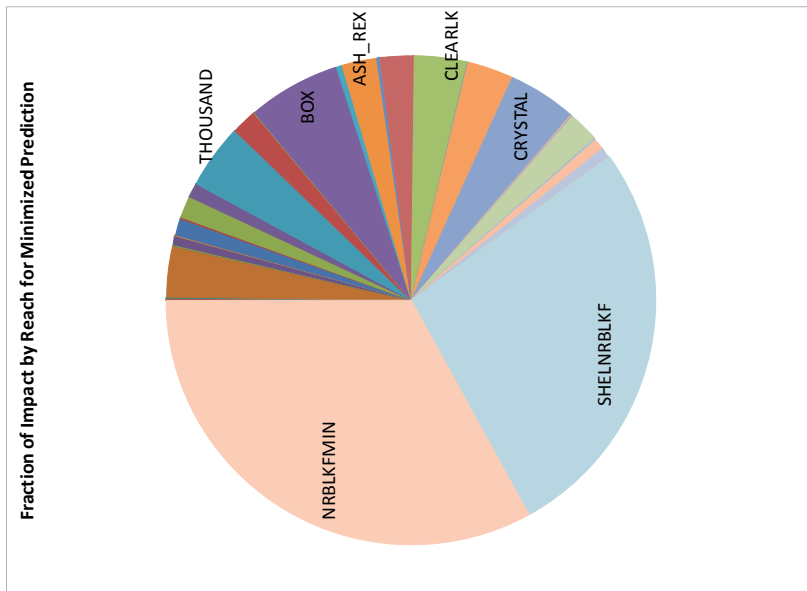
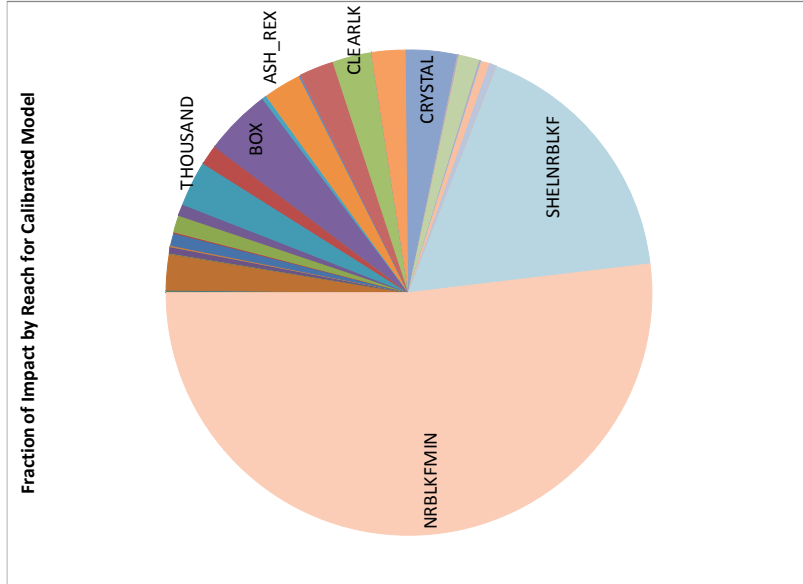




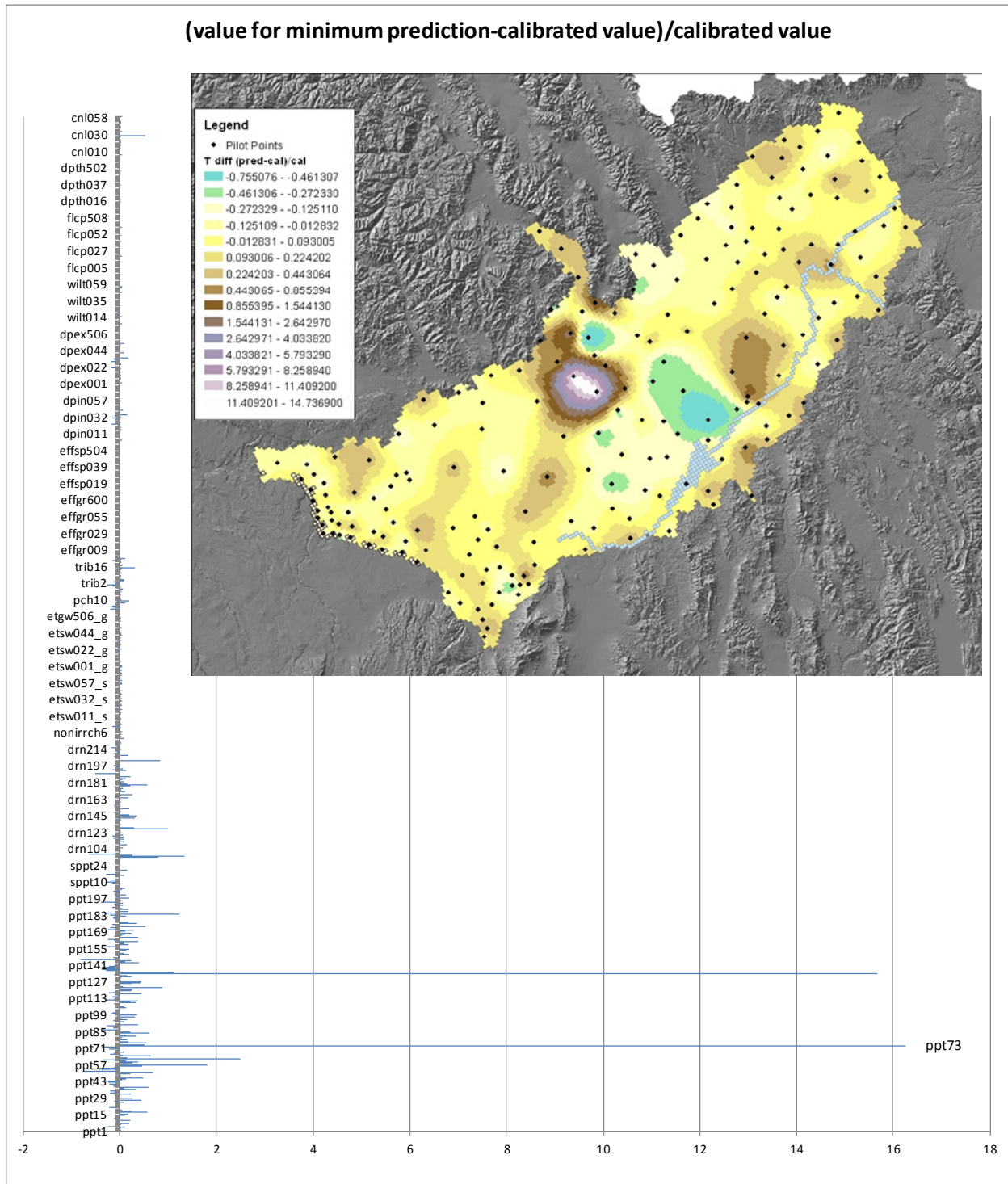
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



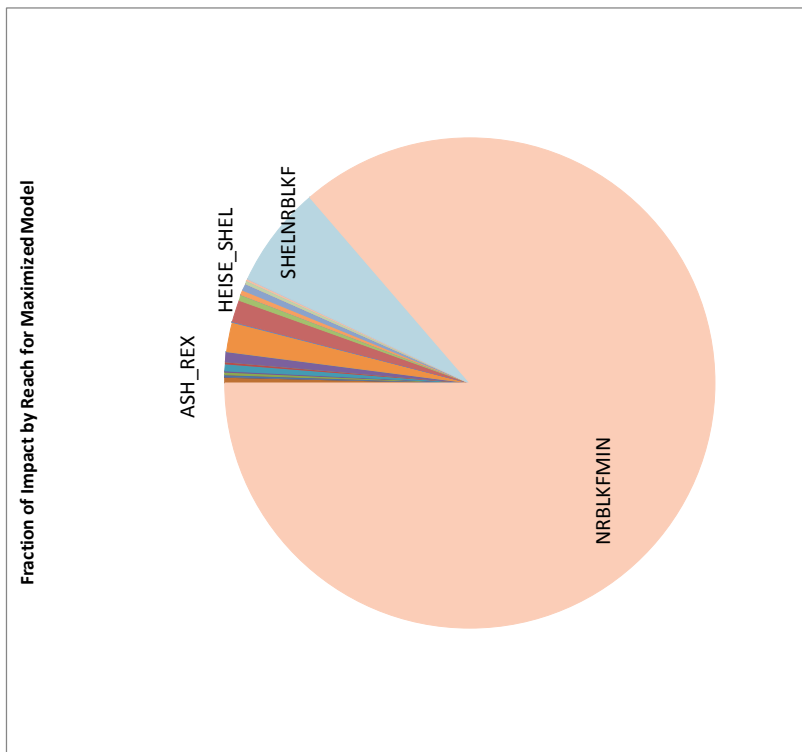
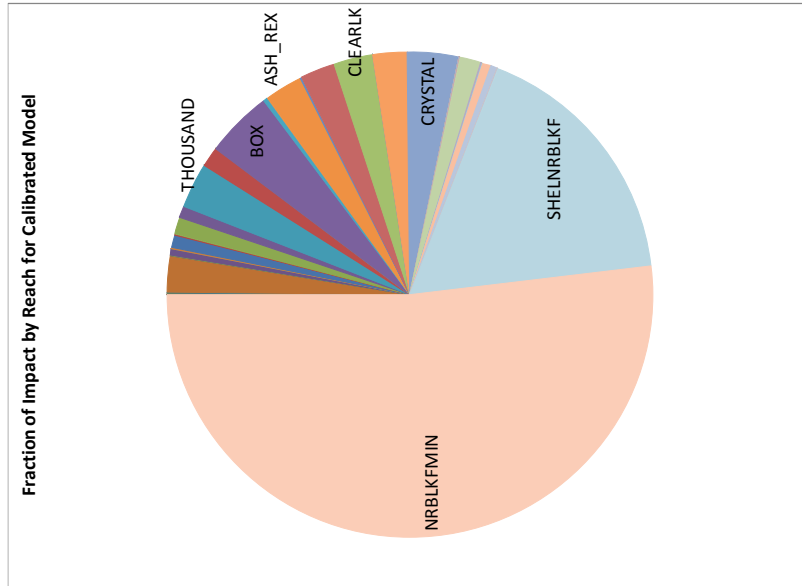
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.

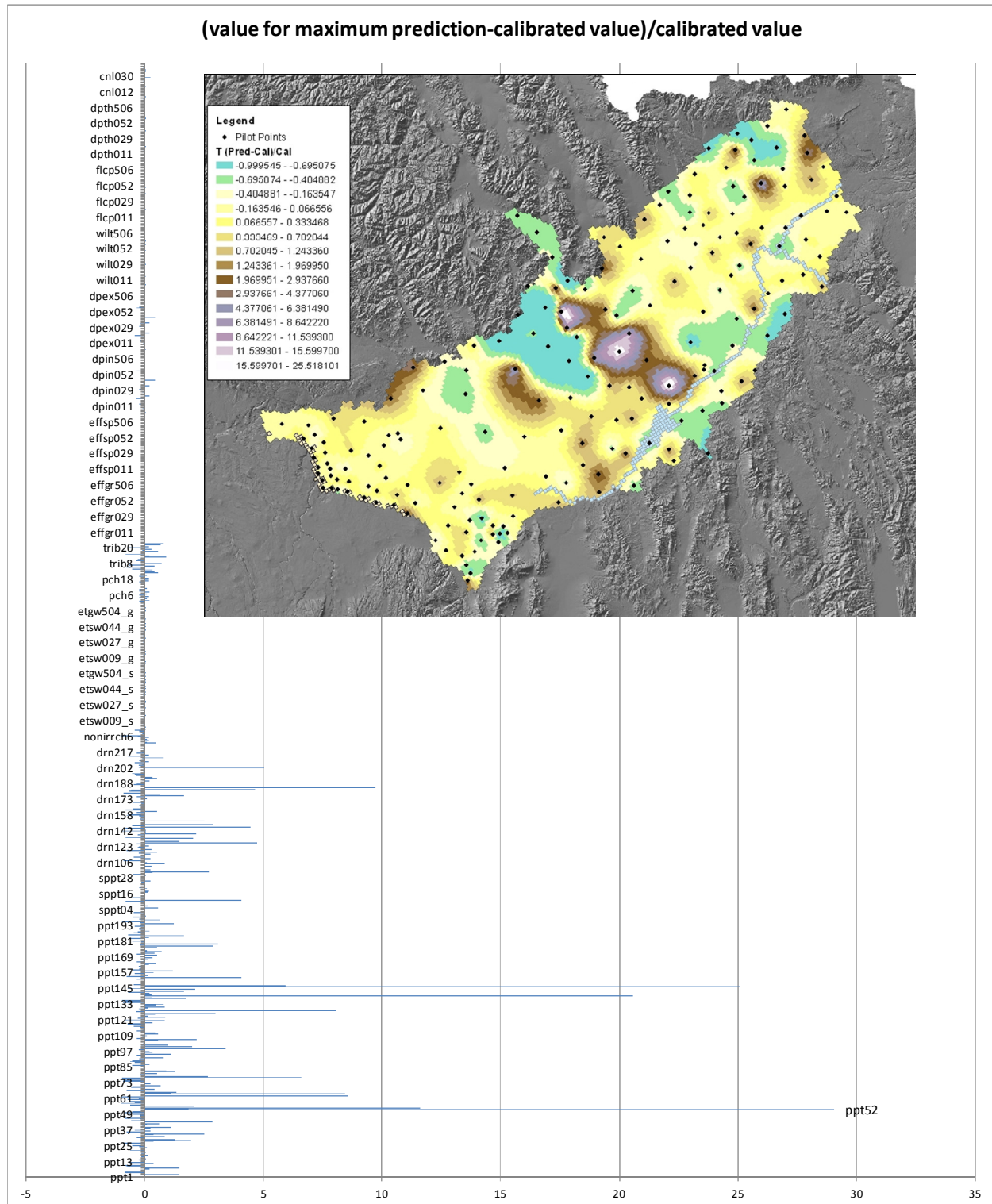


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.

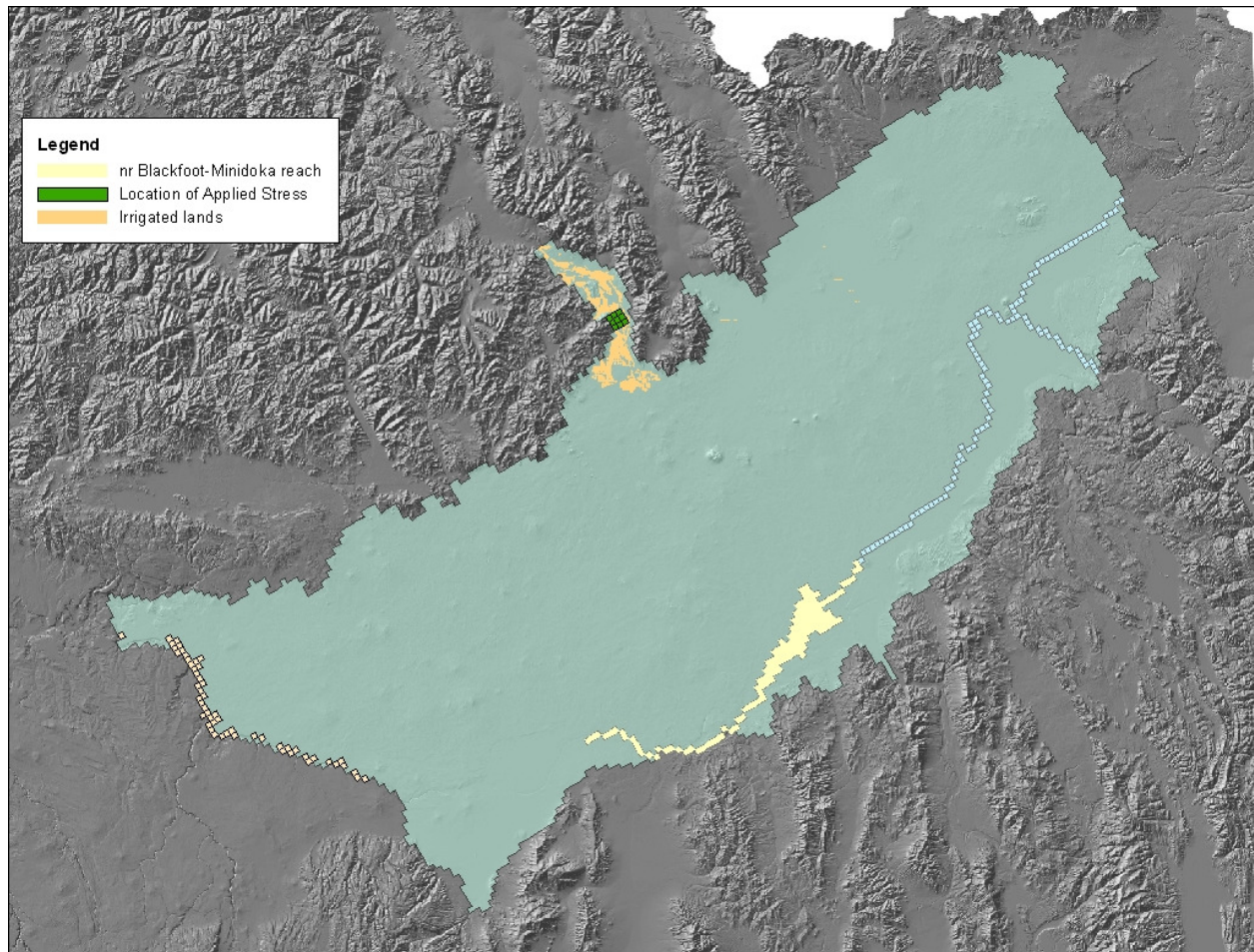




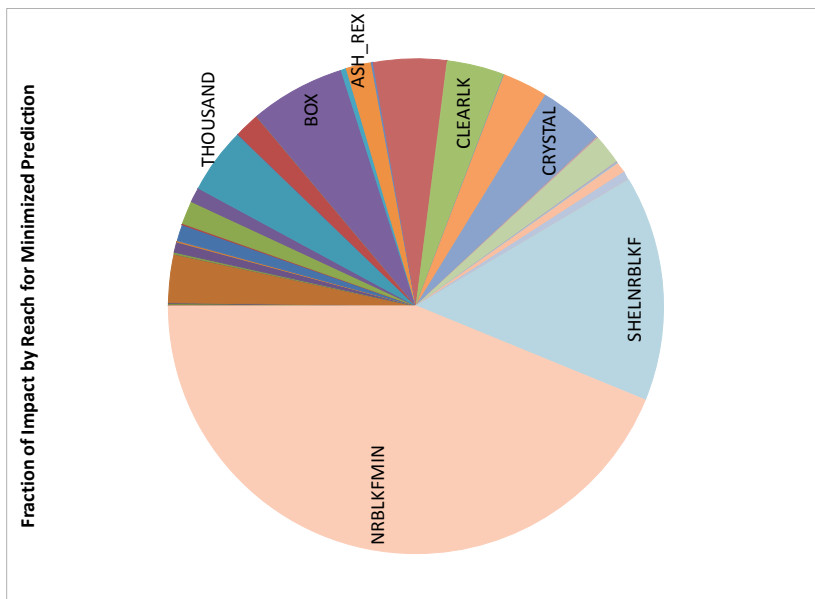
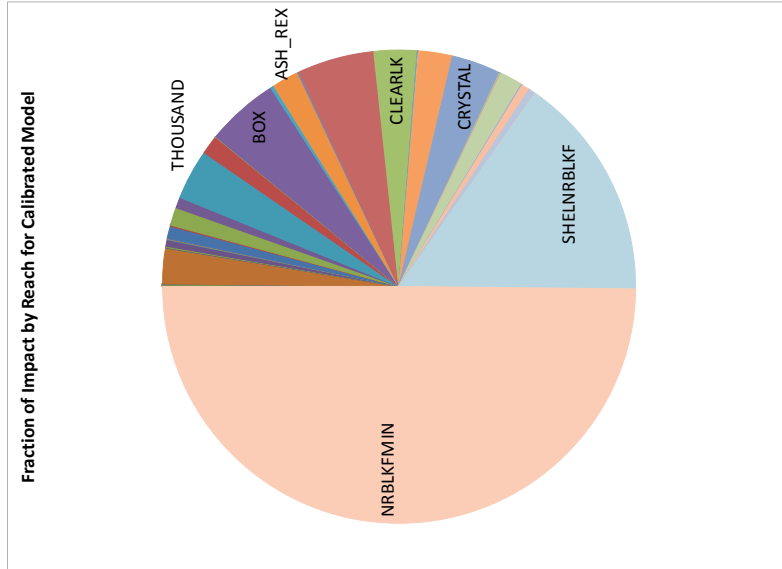
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E121025A001.

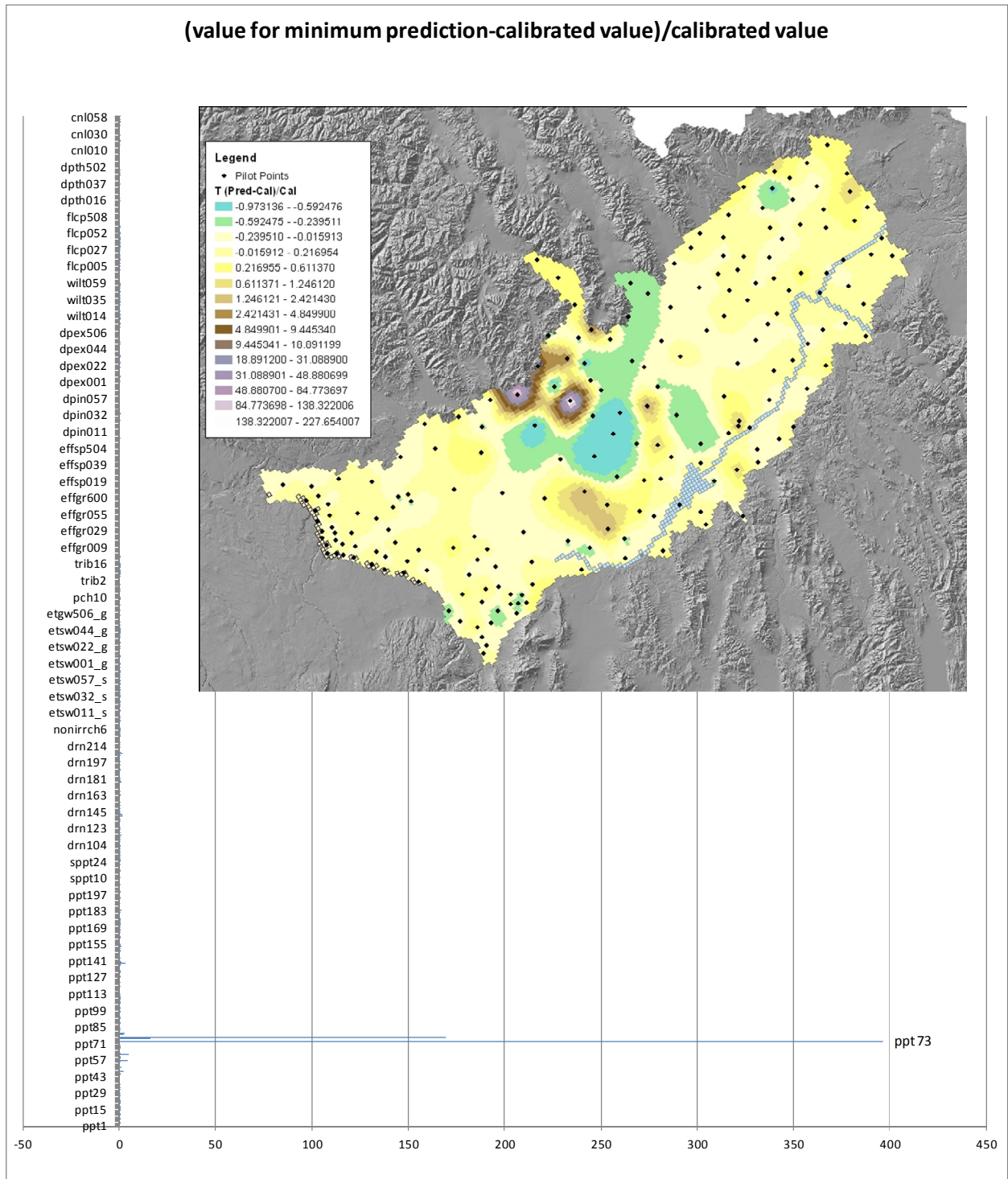


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E121025A001.

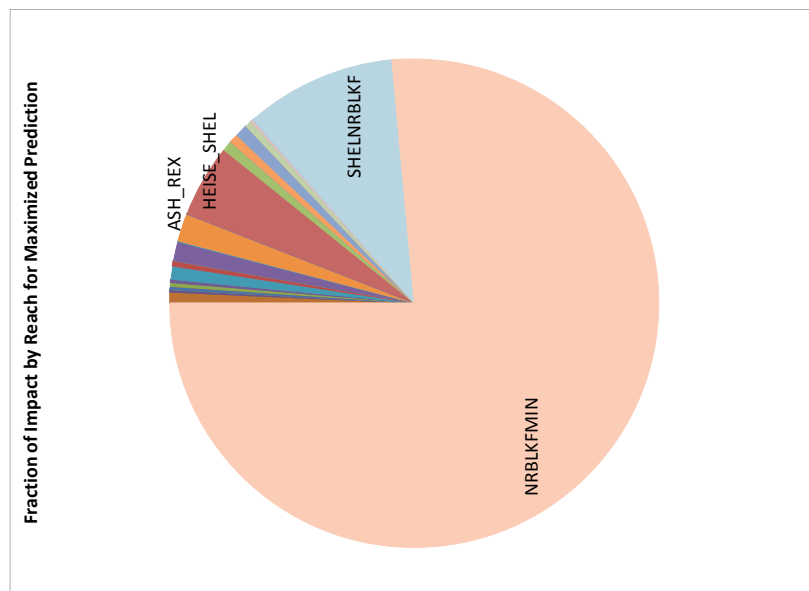
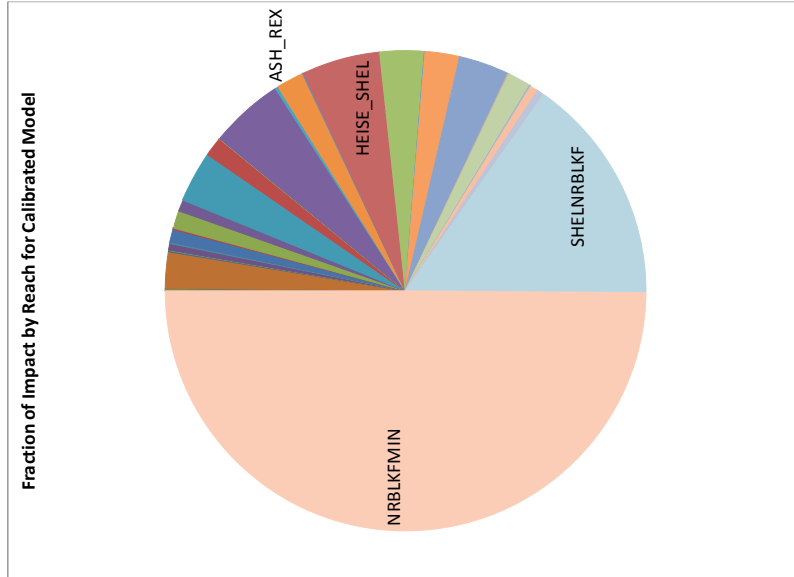




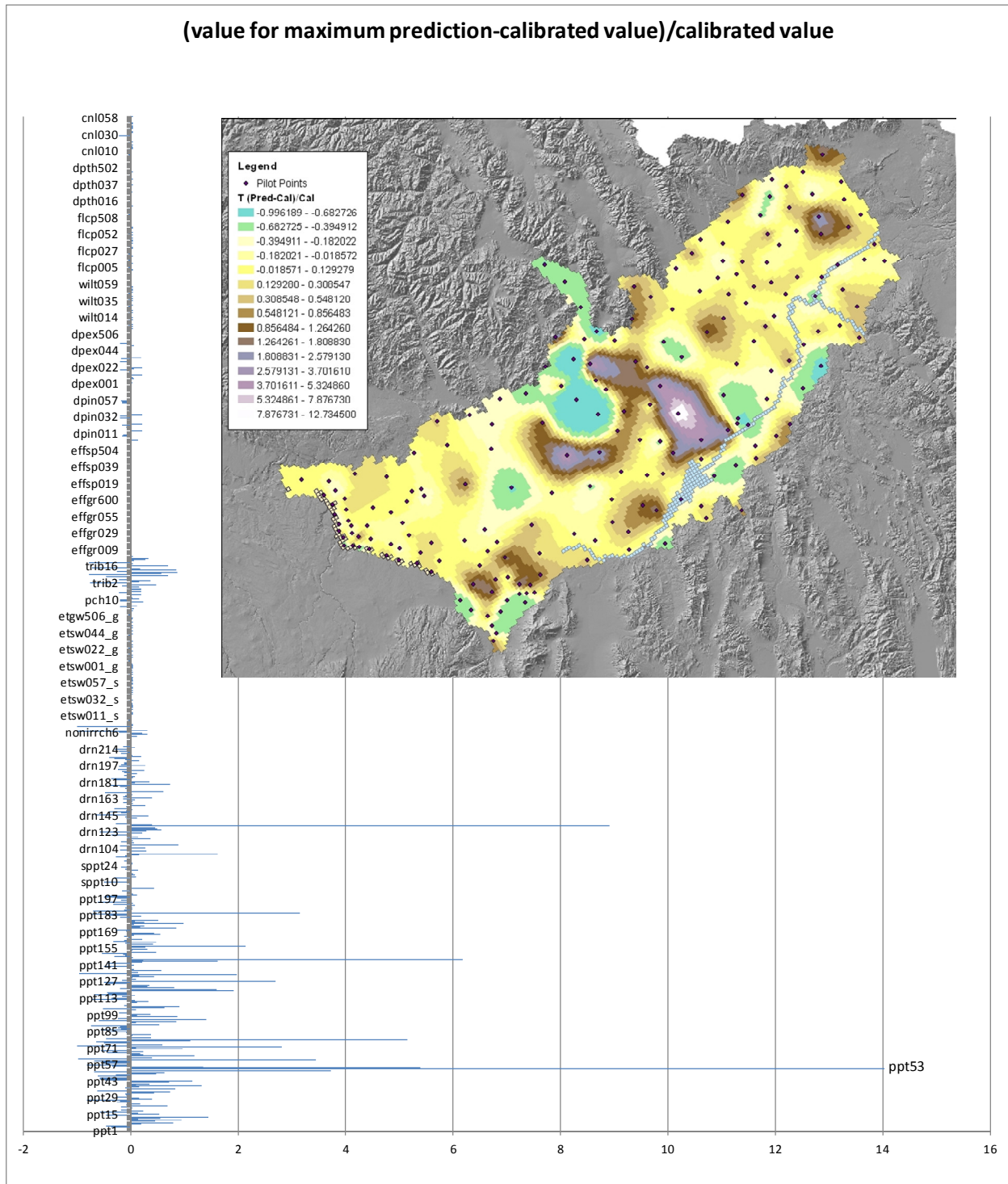
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E121025A001.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E121025A001.

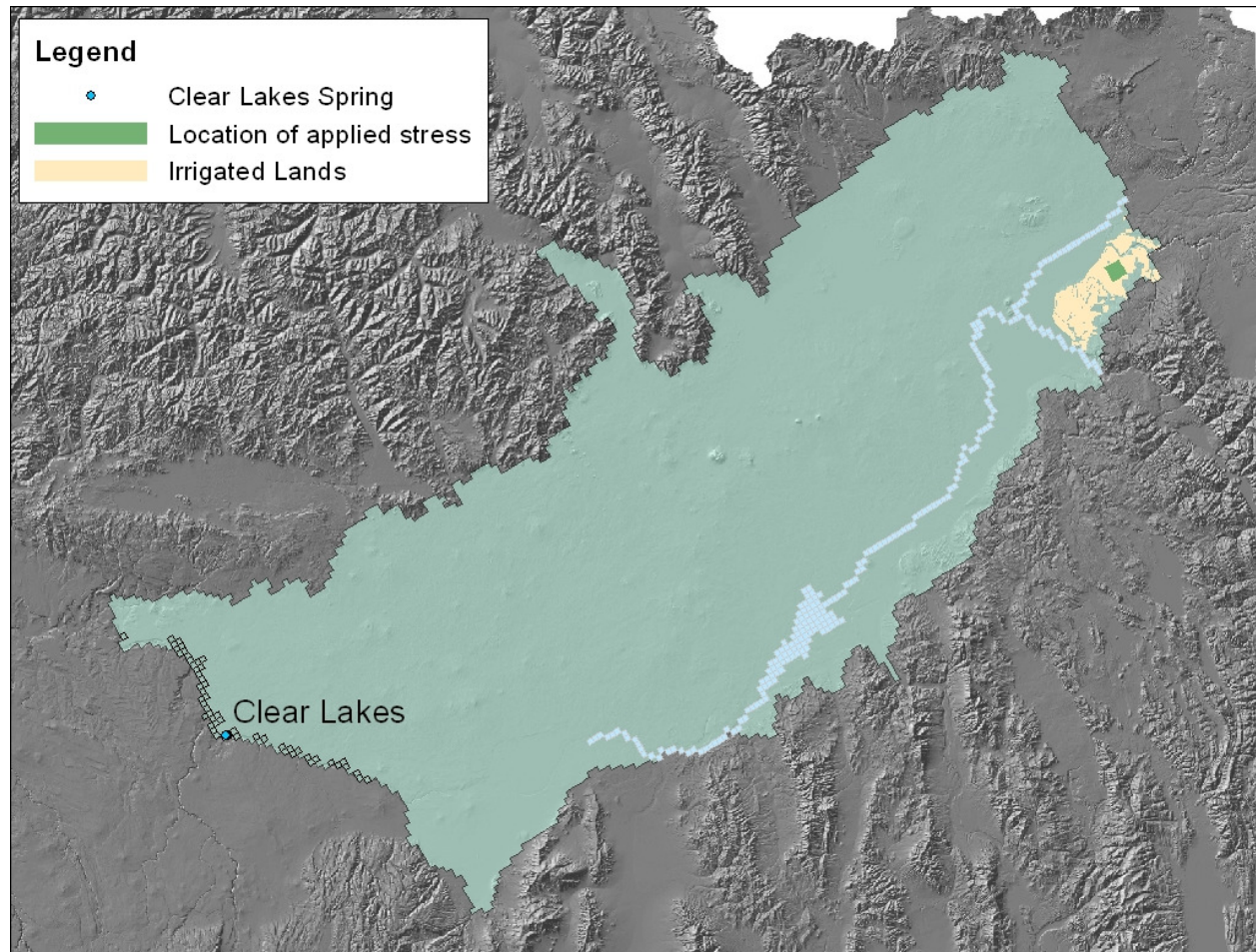


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E121025A001.



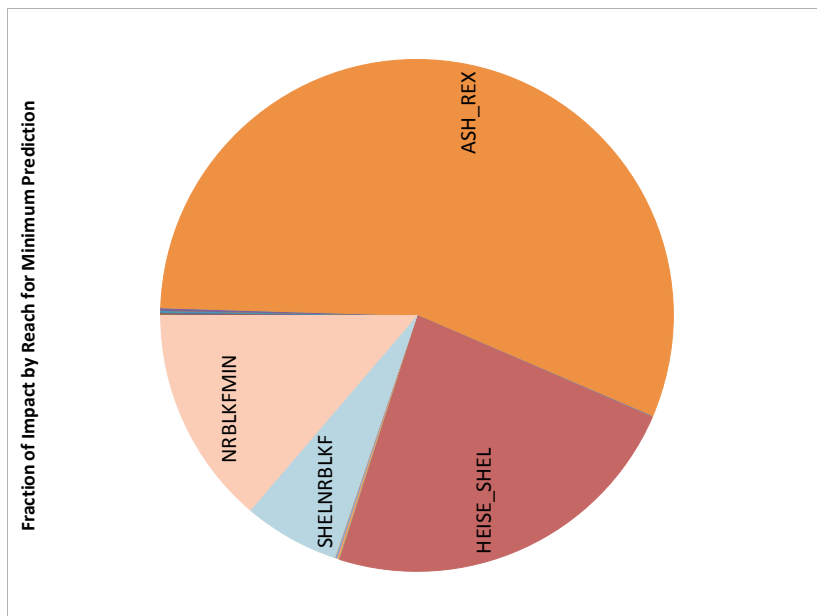
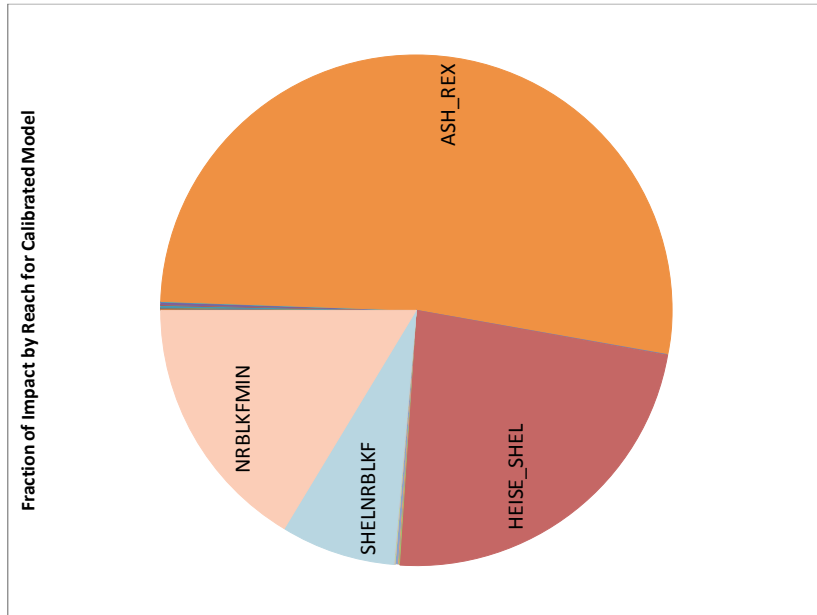


Impact of Water District 99 (Rexburg Bench) on near Clear Lakes using calibration run E120116A008.

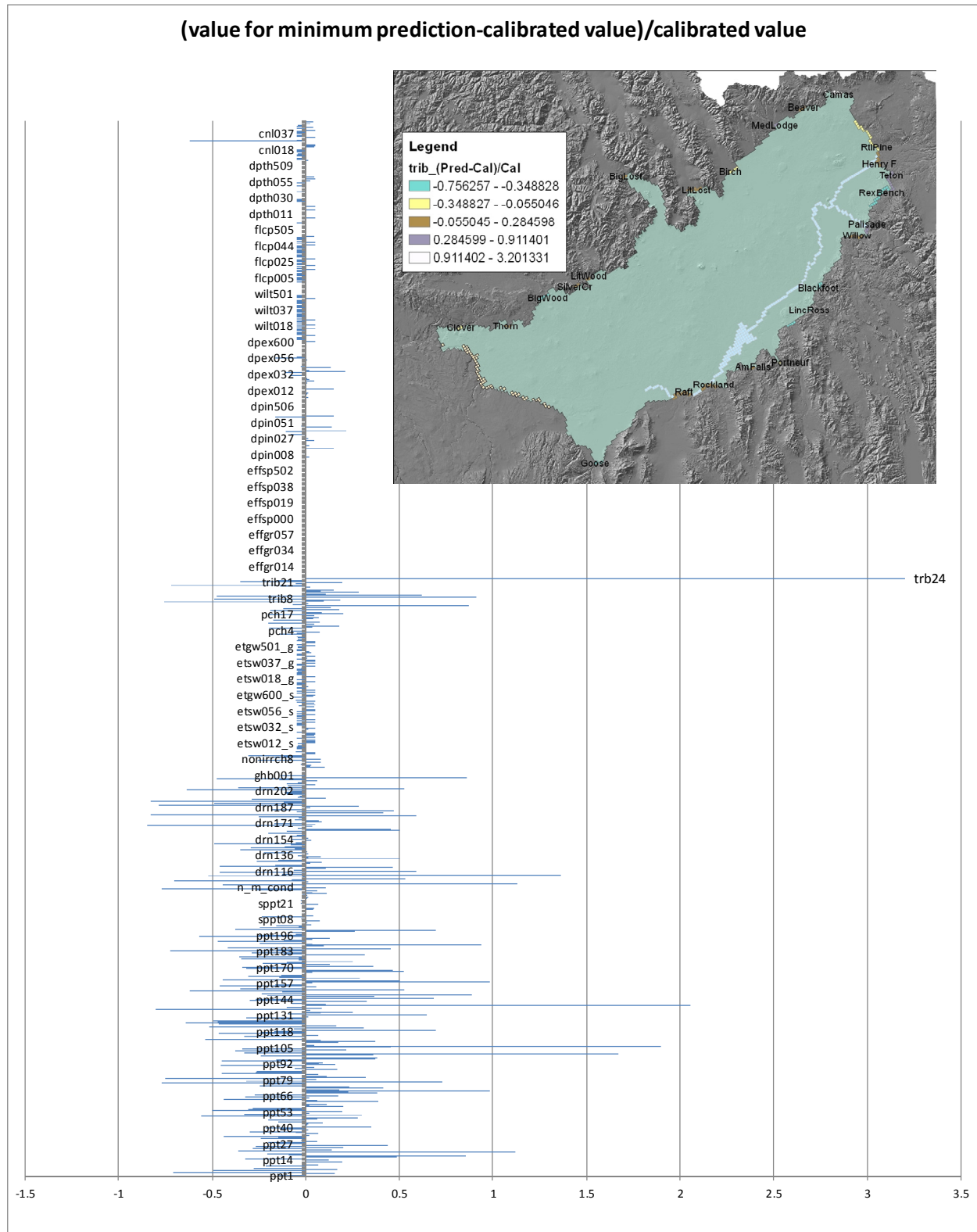




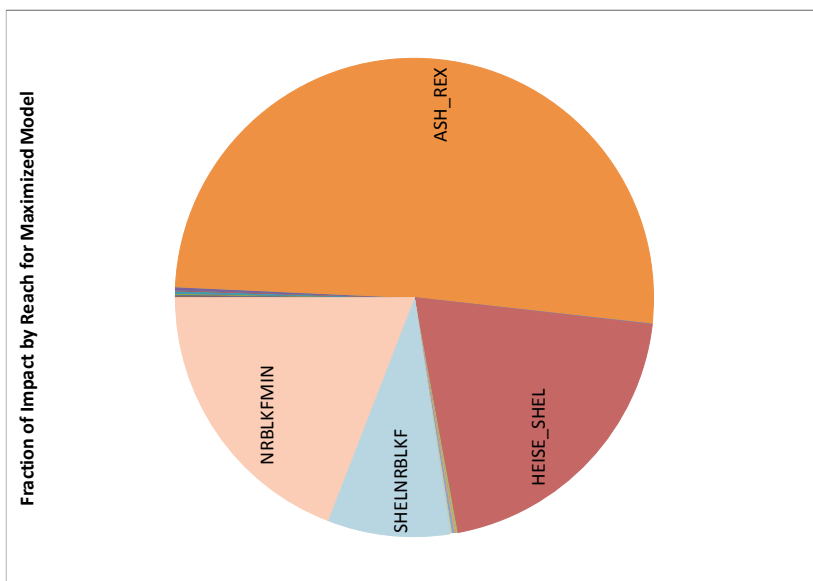
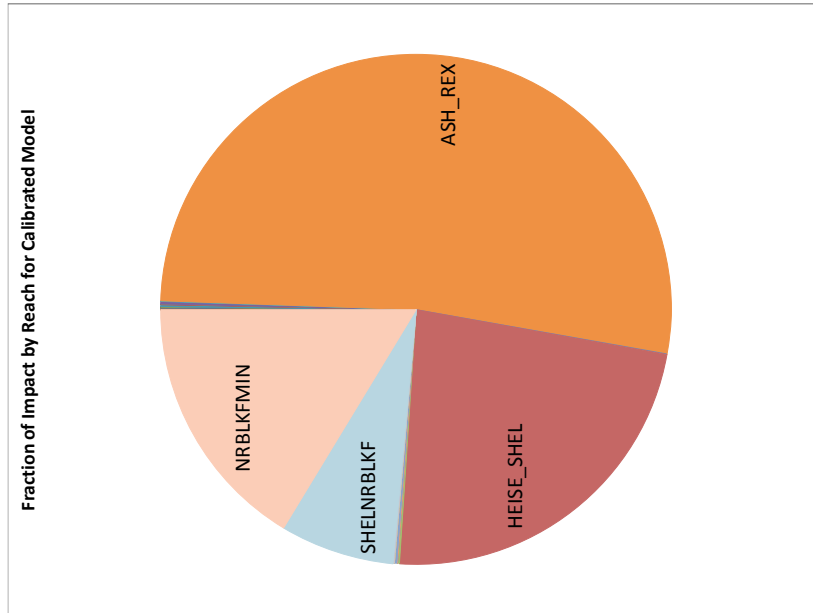
Impact of Water District 99 (Rexburg Bench) on near Clear Lakes using calibration run E120116A008.



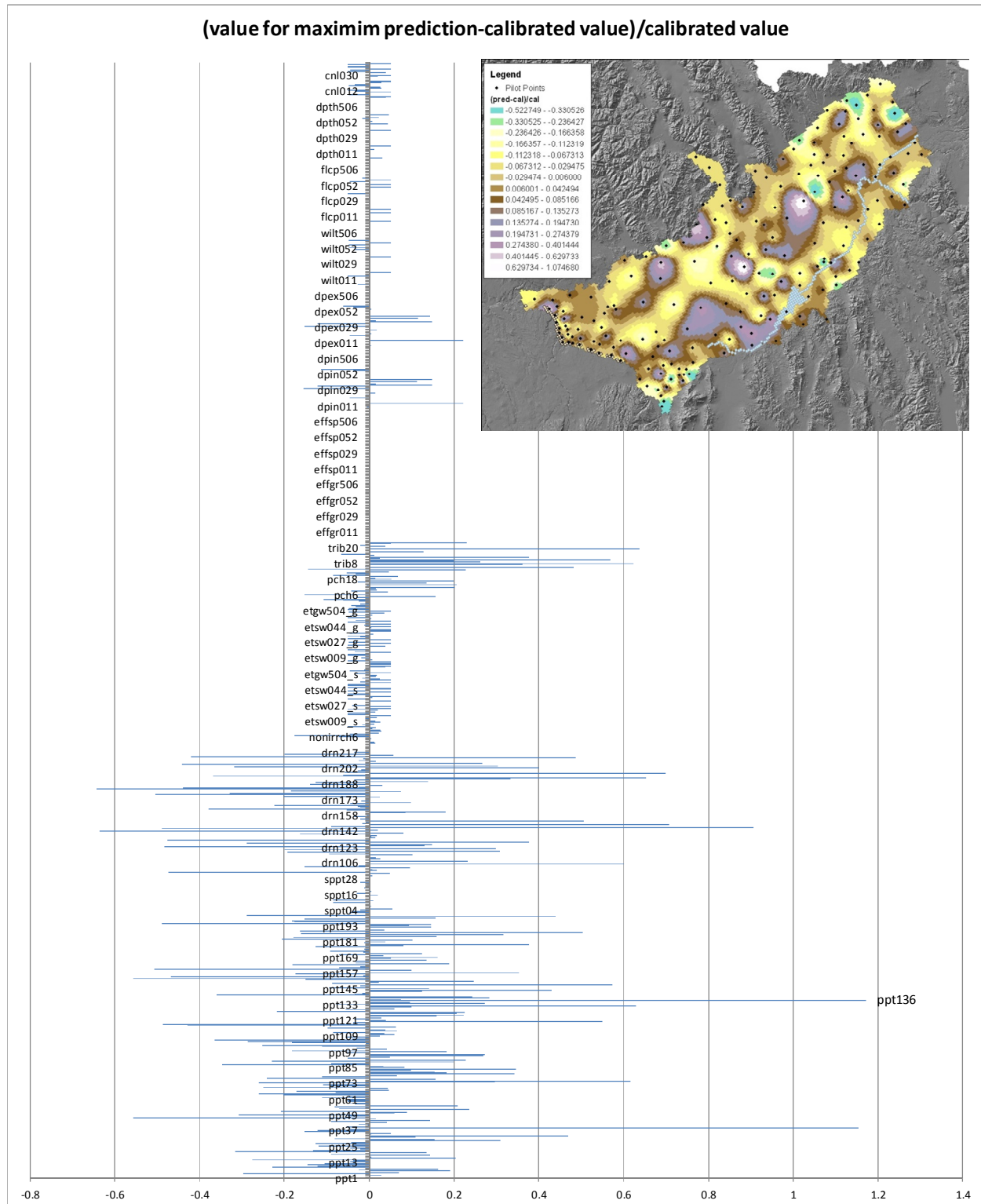
Impact of Water District 99 (Rexburg Bench) on near Clear Lakes using calibration run E120116A008.



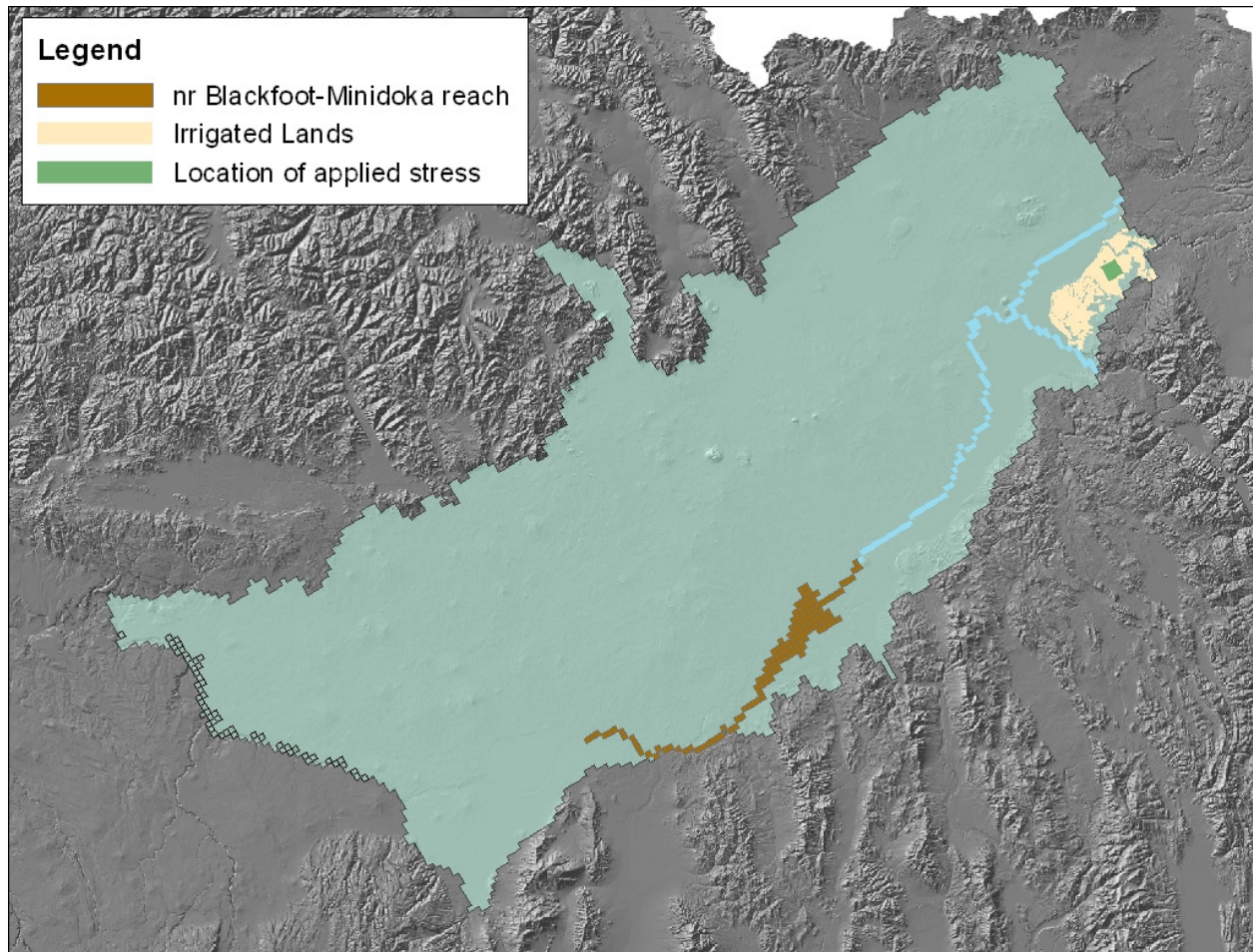
Impact of Water District 99 (Rexburg Bench) on near Clear Lakes using calibration run E120116A008.



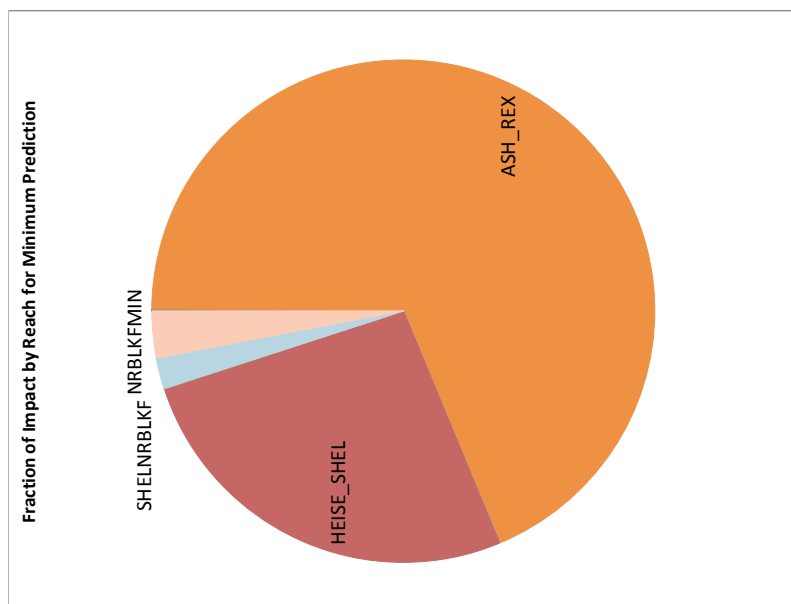
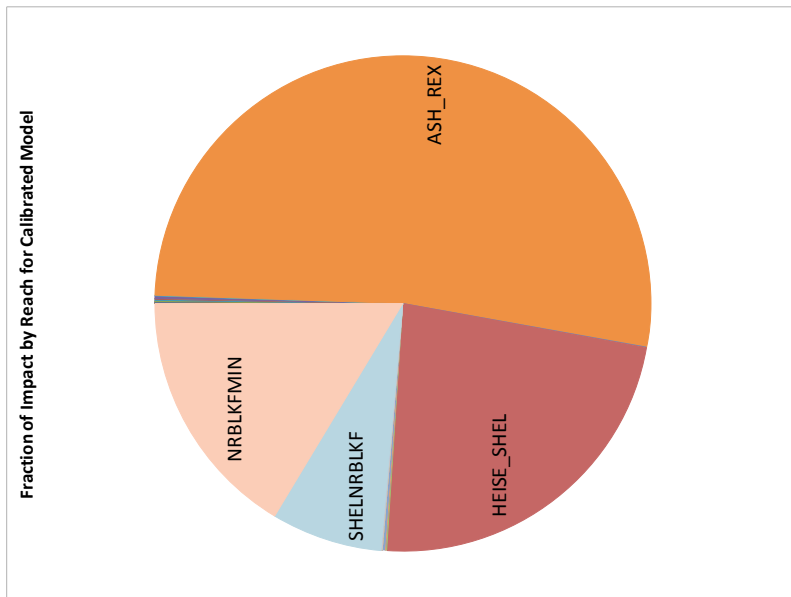
Impact of Water District 99 (Rexburg Bench) on near Clear Lakes using calibration run E120116A008.



Impact of Water District 99 (Rexburg Bench) on near Blackfoot-Minidoka using calibration run E120116A008.

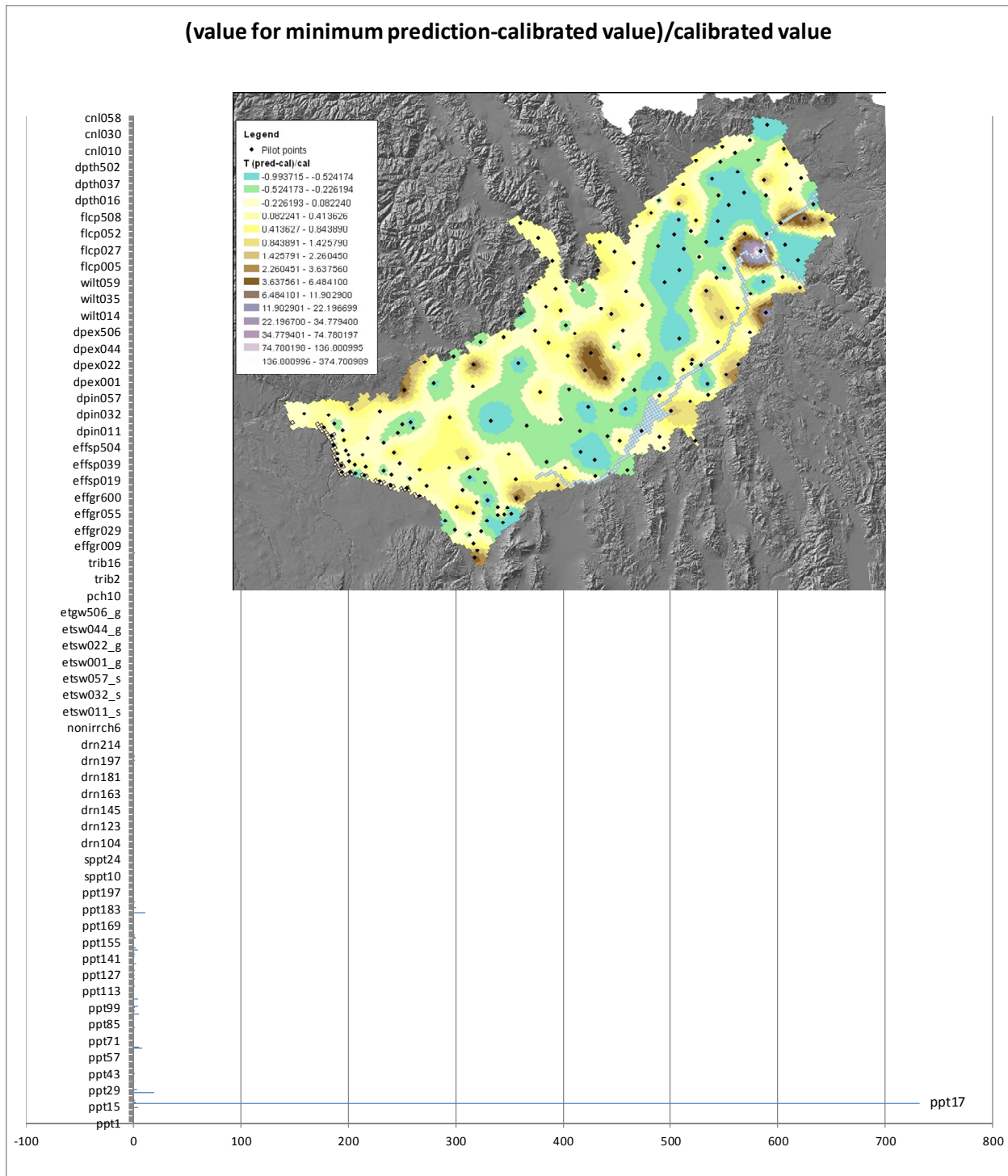


Impact of Water District 99 (Rexburg Bench) on near Blackfoot-Minidoka using calibration run E120116A008.



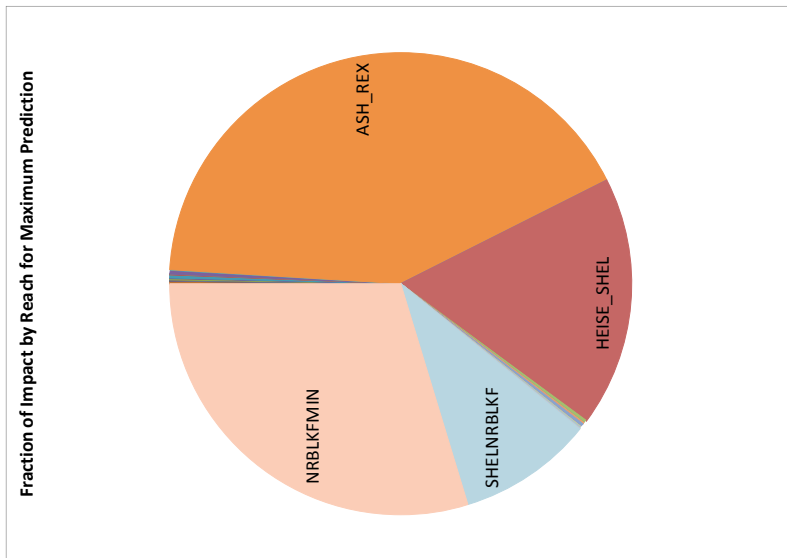
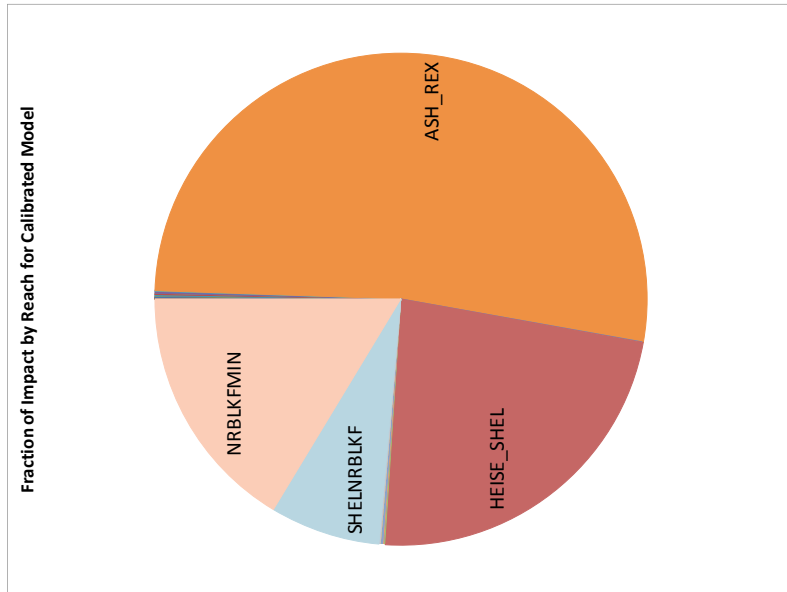


Impact of Water District 99 (Rexburg Bench) on near Blackfoot-Minidoka using calibration run E120116A008.

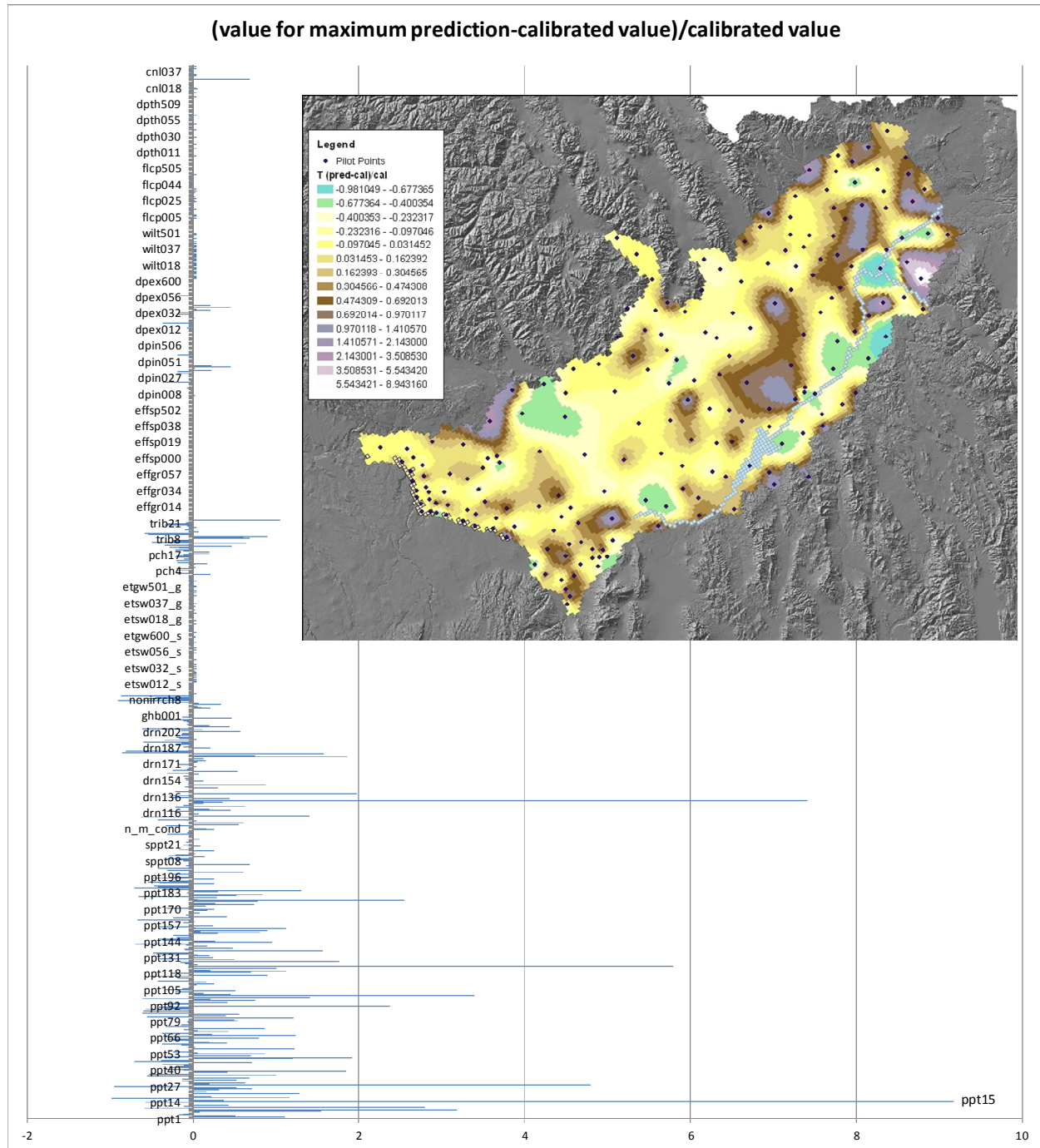




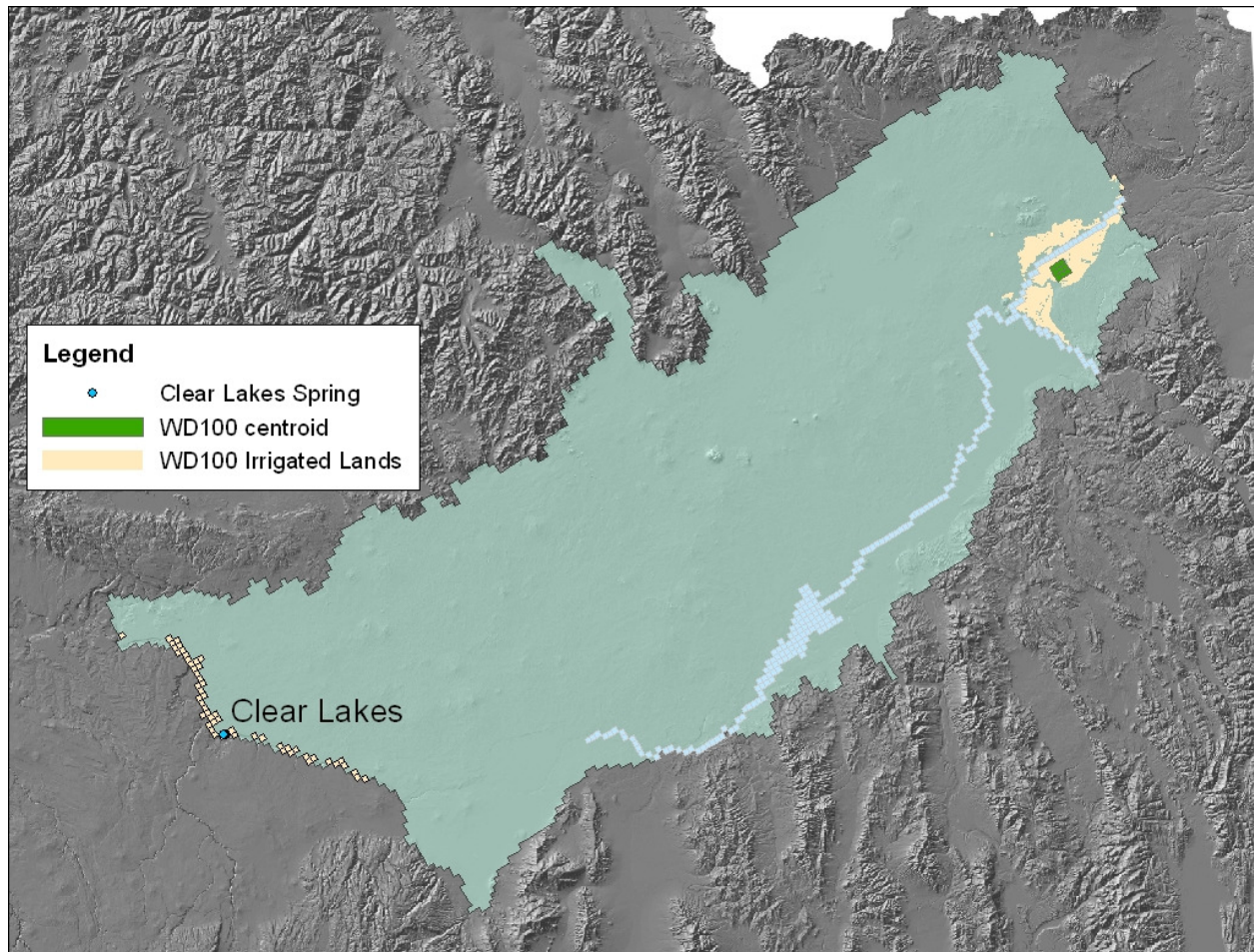
Impact of Water District 99 (Rexburg Bench) on near Blackfoot-Minidoka using calibration run E120116A008.



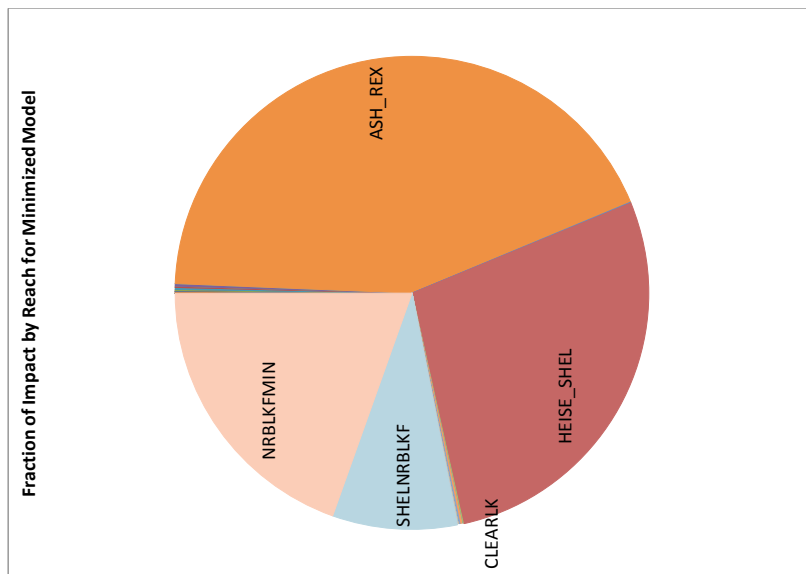
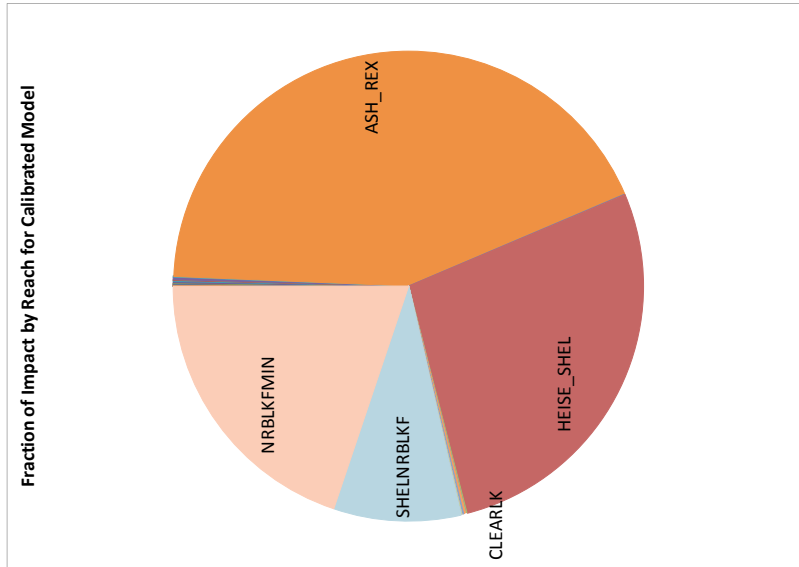
Impact of Water District 99 (Rexburg Bench) on near Blackfoot-Minidoka using calibration run E120116A008.



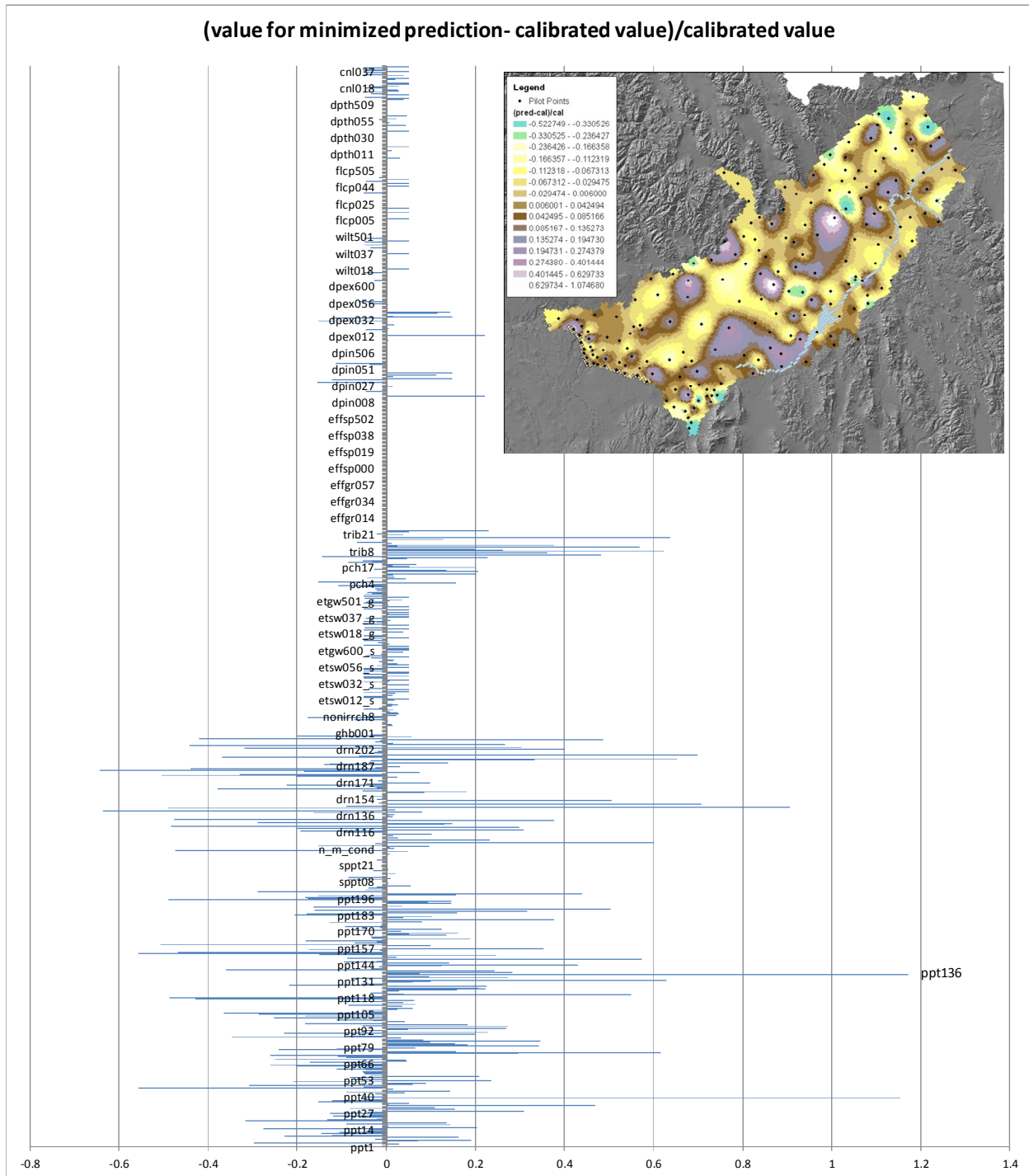
Impact of Water District 100 on Clear Lakes Spring using calibration run E120116A008.



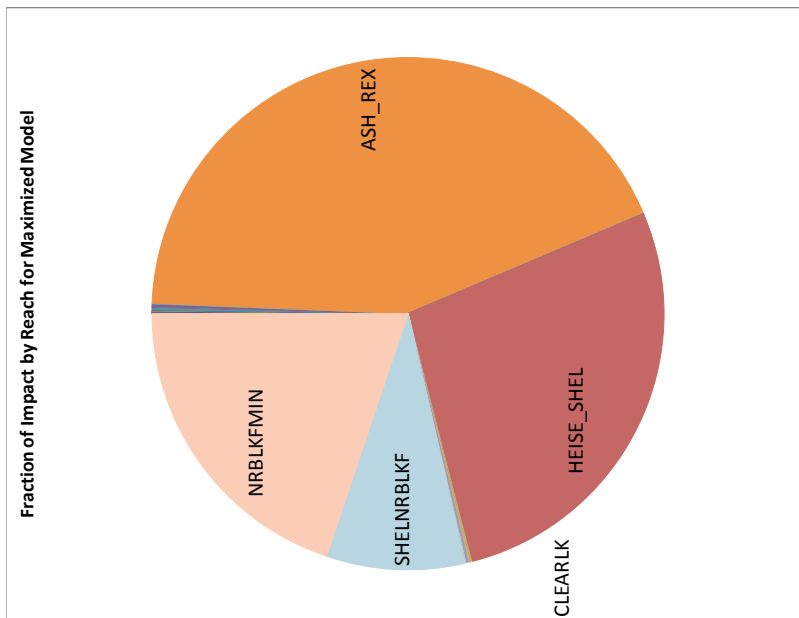
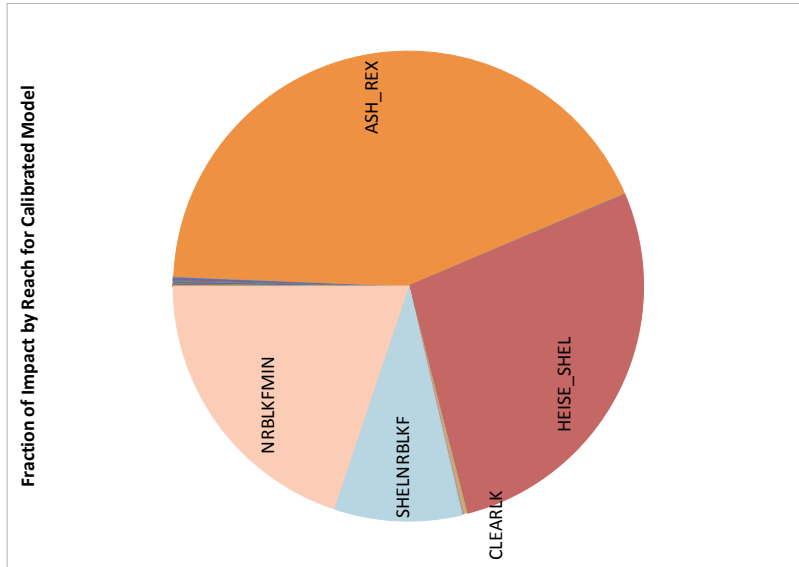
Impact of Water District 100 on Clear Lakes Spring using calibration run E120116A008.



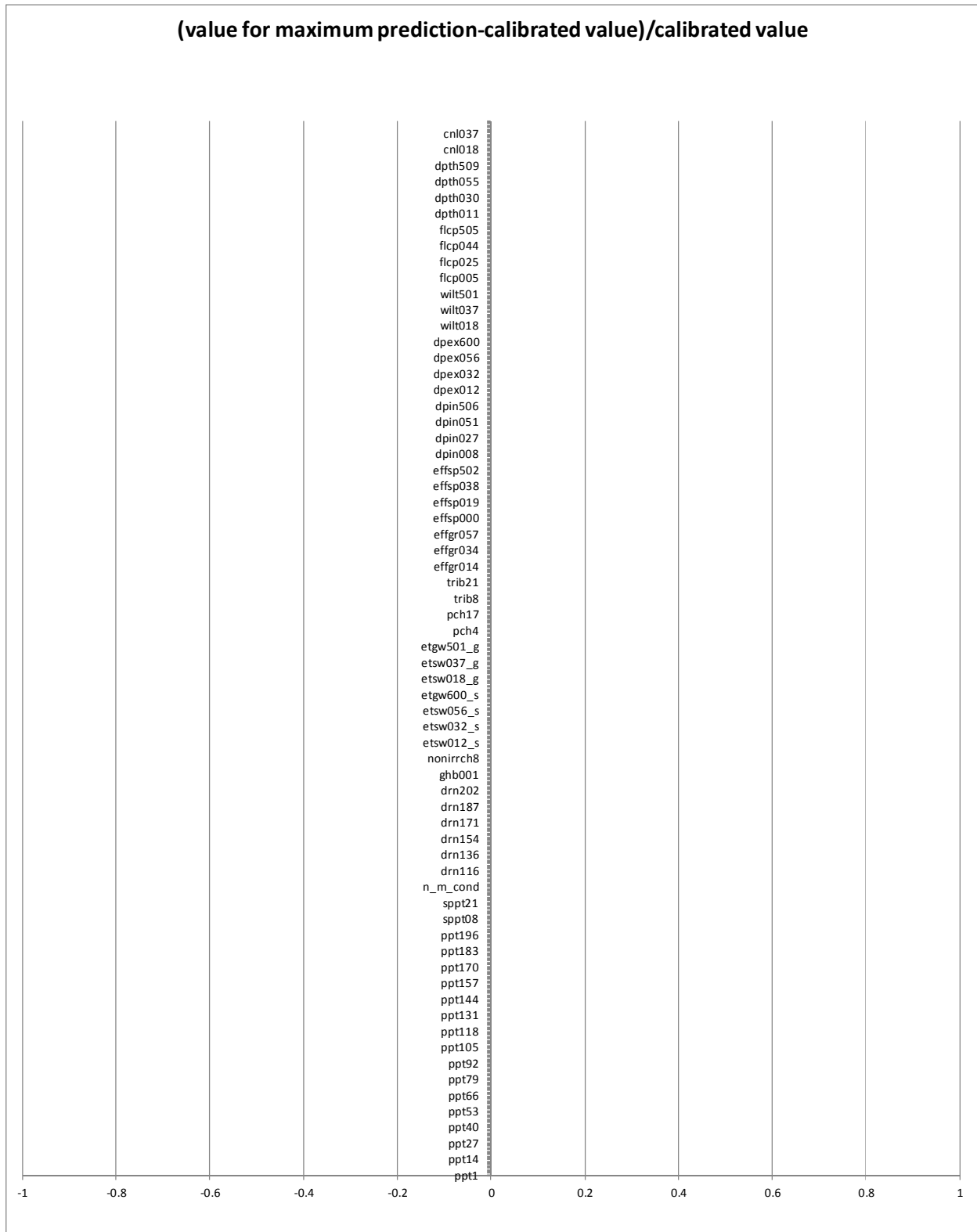
Impact of Water District 100 on Clear Lakes Spring using calibration run E120116A008.



Impact of Water District 100 on Clear Lakes Spring using calibration run E120116A008.

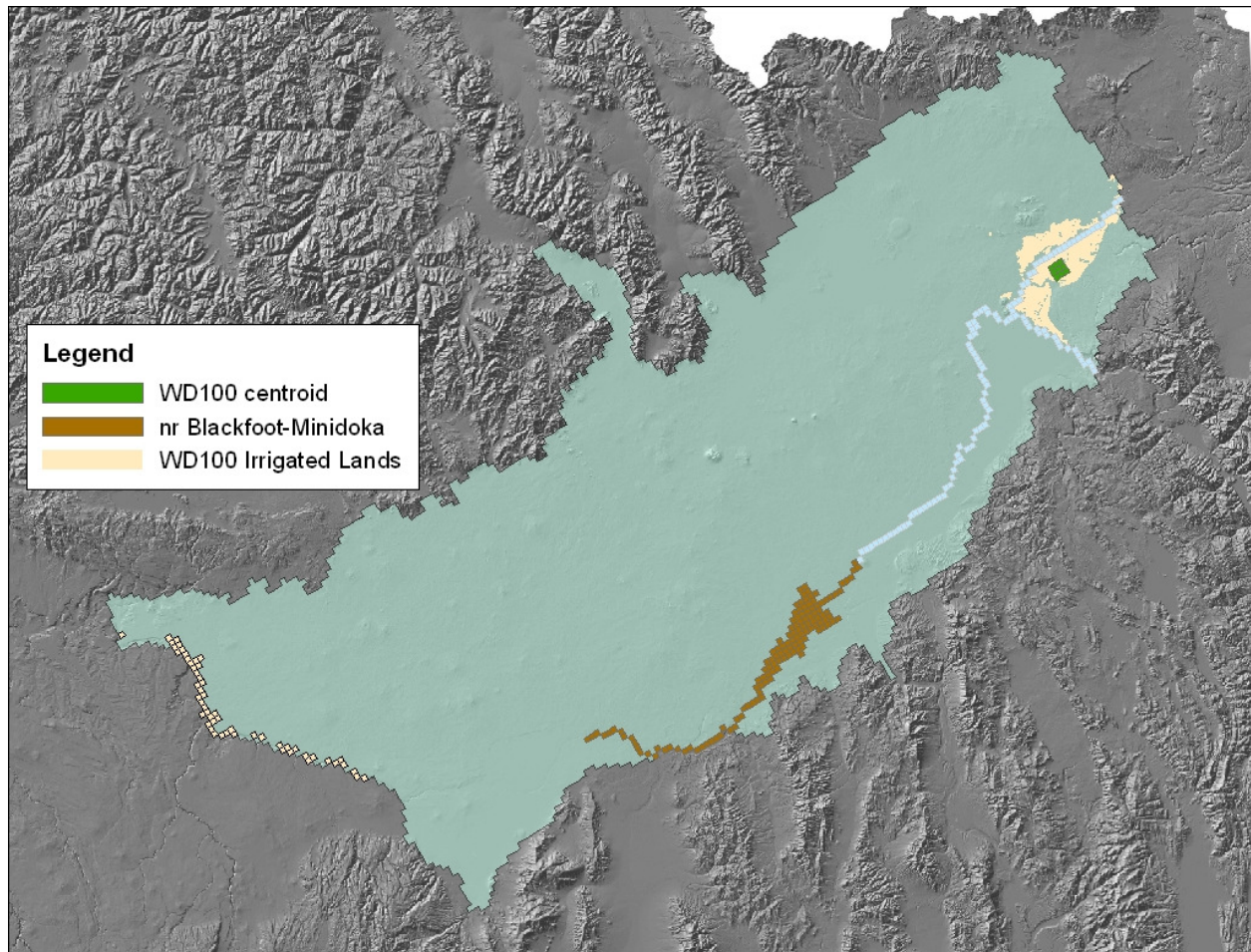


Impact of Water District 100 on Clear Lakes Spring using calibration run E120116A008.

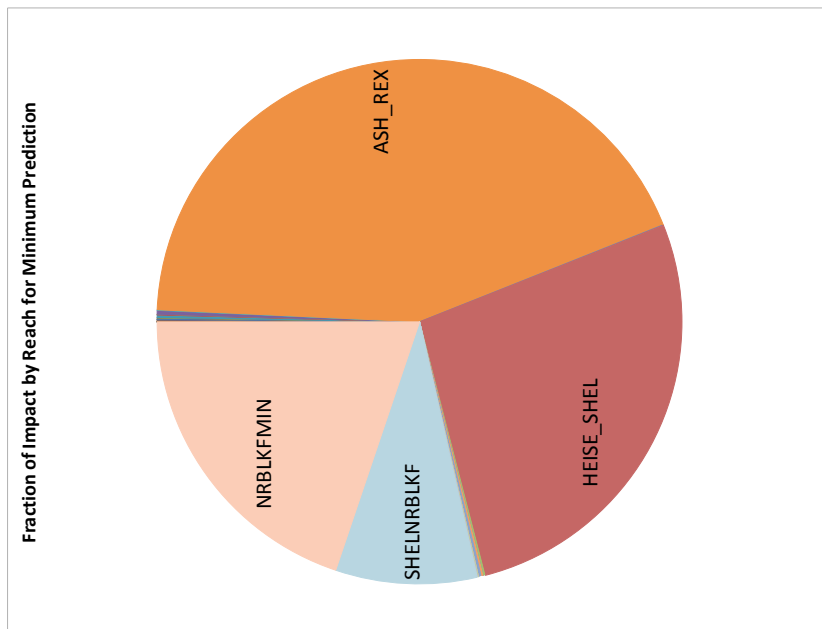
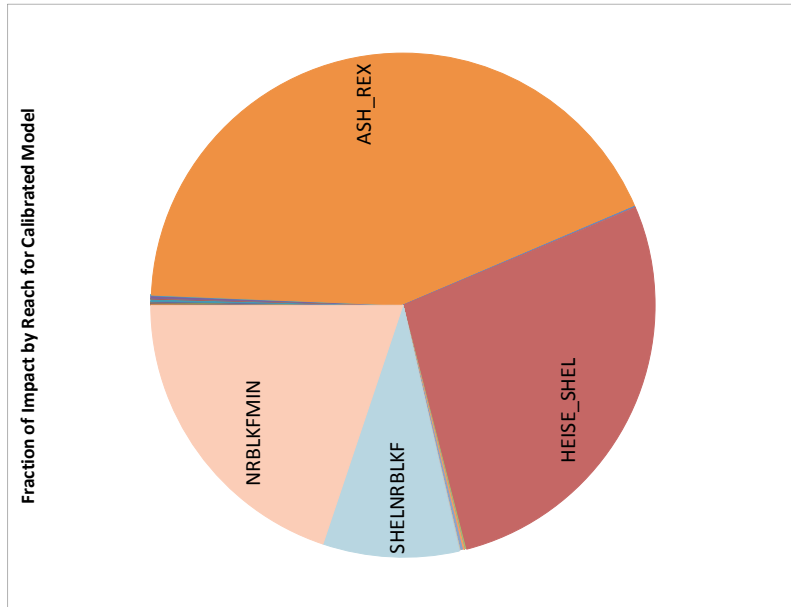




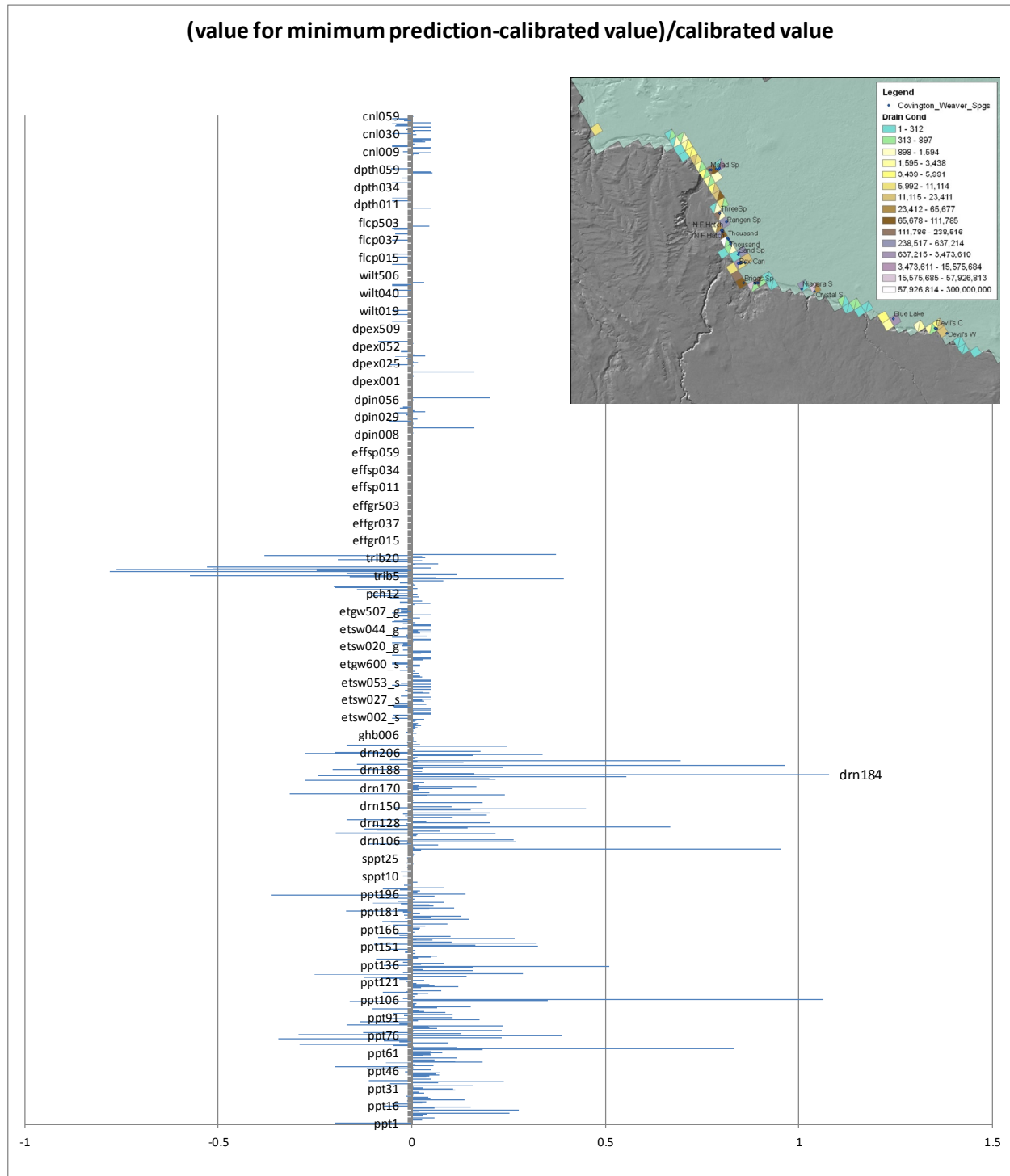
Impact of Water District 100 on near Blackfoot-Minidoka using calibration run E120116A008.



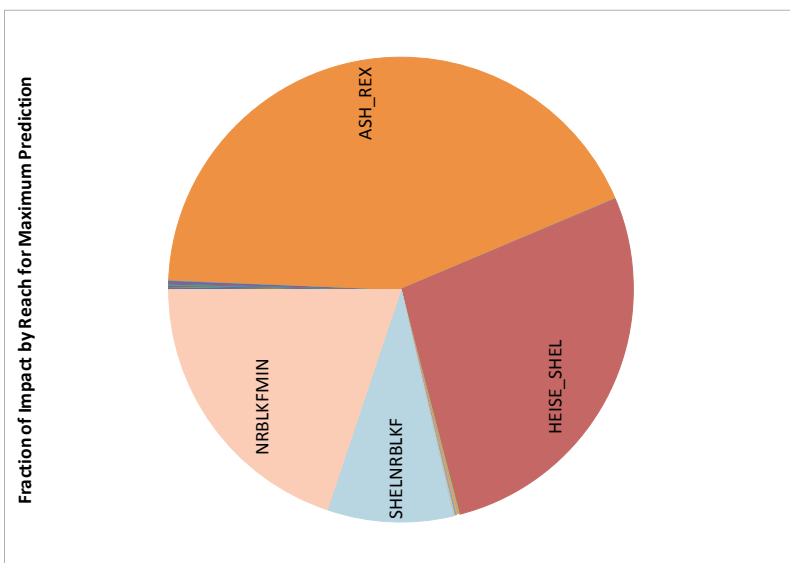
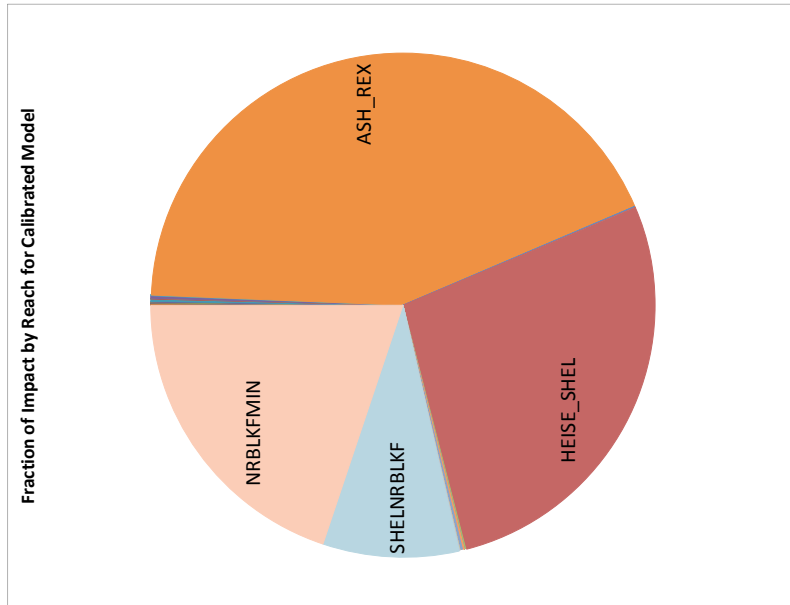
Impact of Water District 100 on near Blackfoot-Minidoka using calibration run E120116A008.



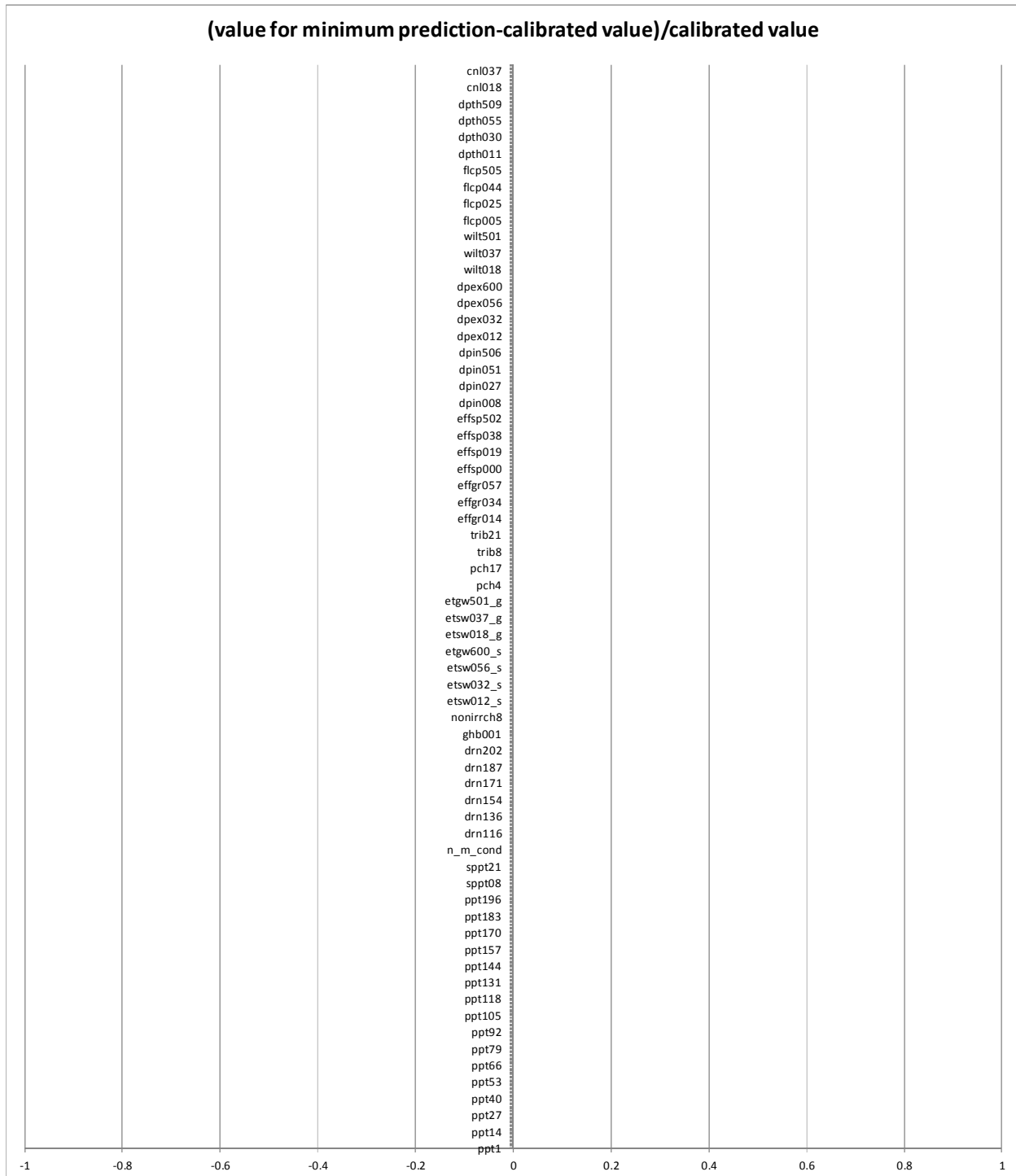
Impact of Water District 100 on near Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 100 on near Blackfoot-Minidoka using calibration run E120116A008.

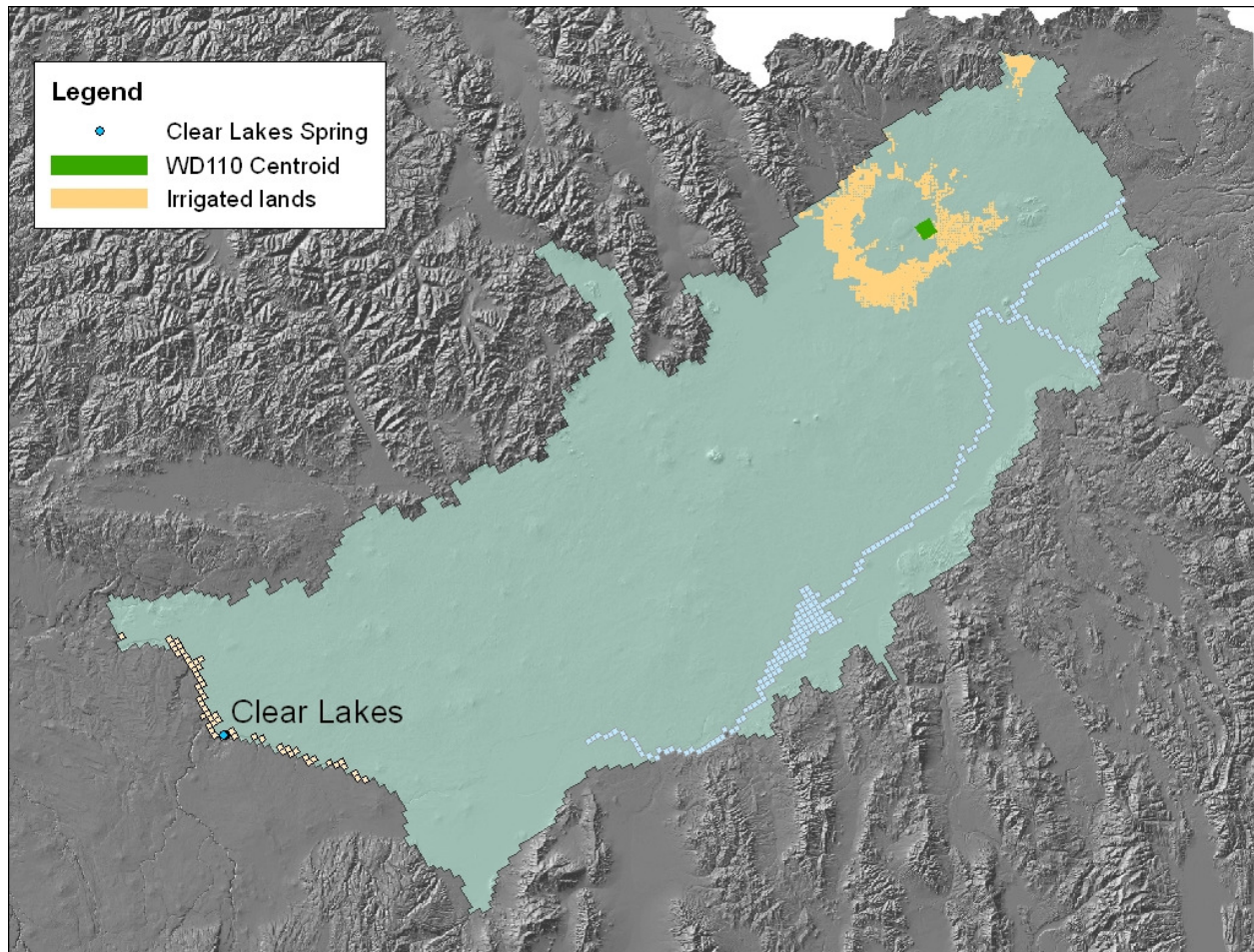


Impact of Water District 100 on near Blackfoot-Minidoka using calibration run E120116A008.



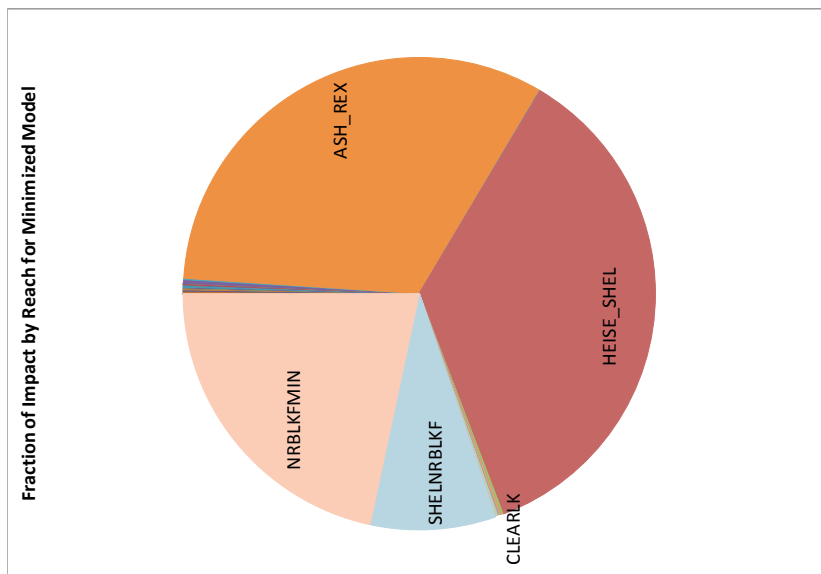
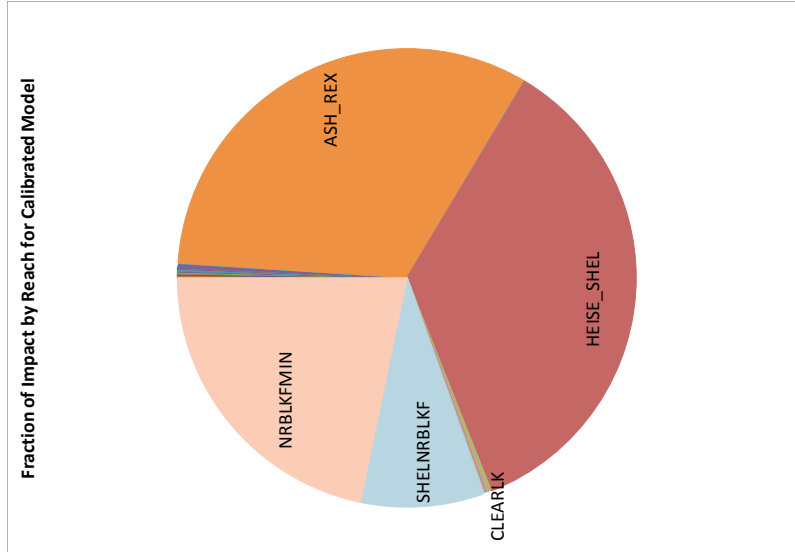


Impact of Water District 110 on Clear Lakes Spring using calibration run E110712A001.

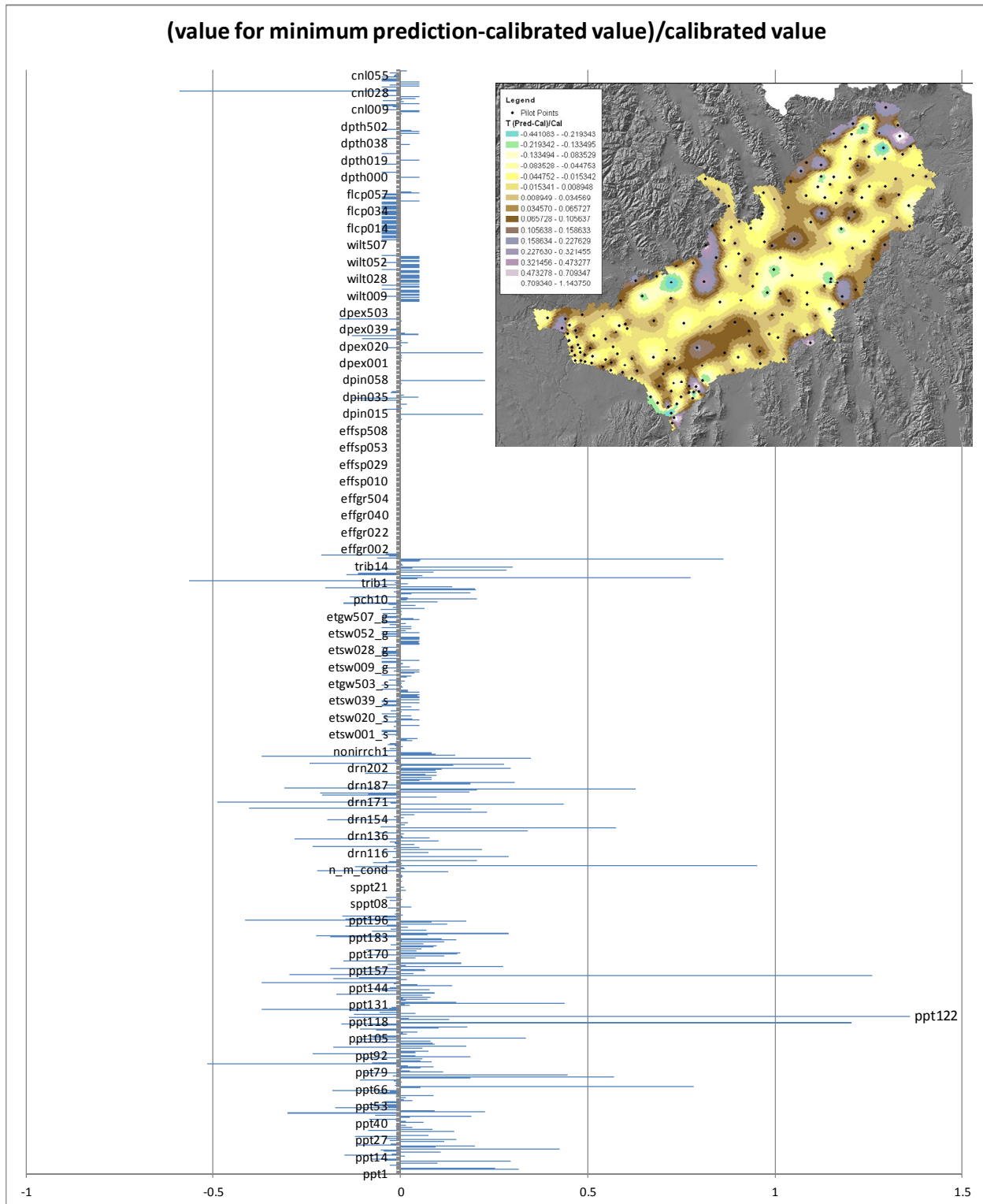




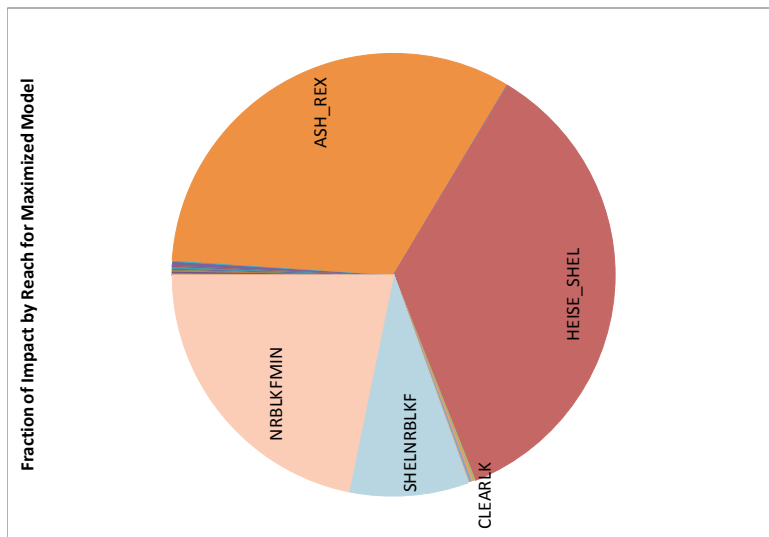
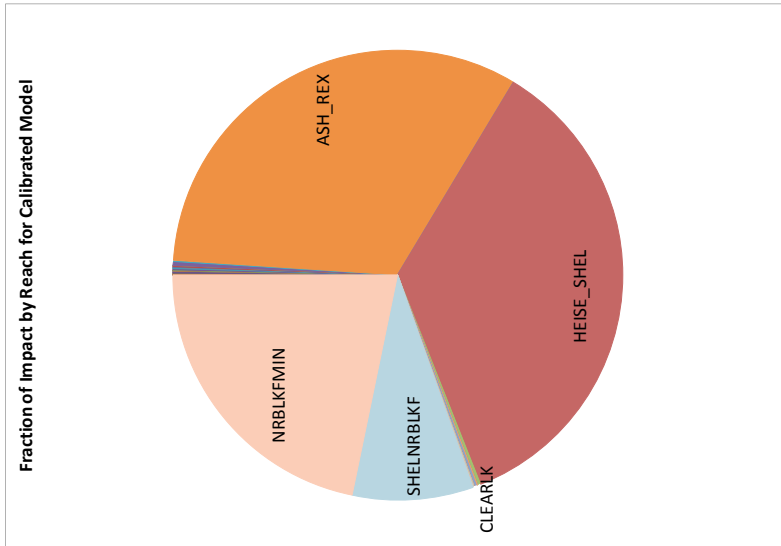
Impact of Water District 110 on Clear Lakes Spring using calibration run E110712A001.



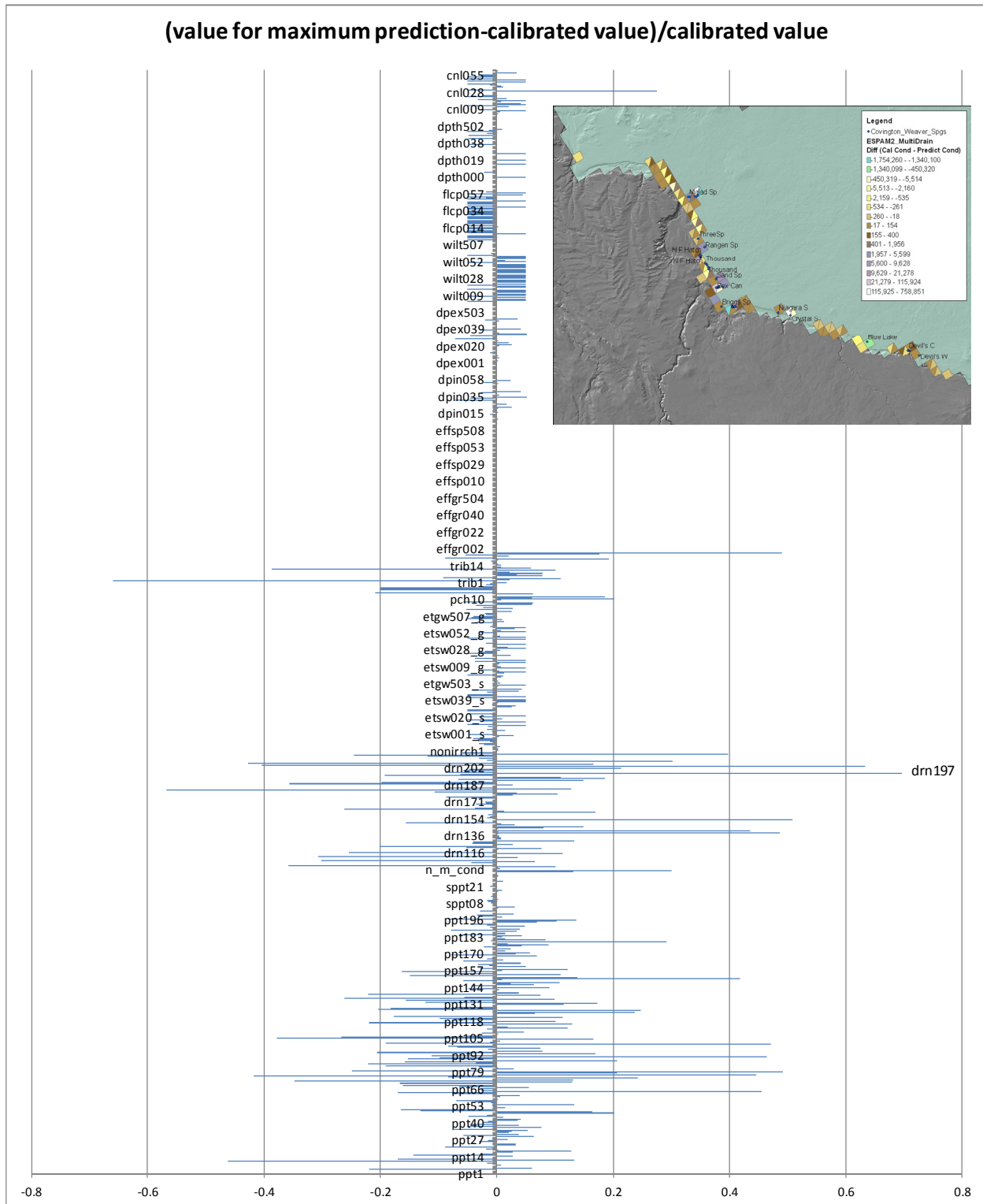
Impact of Water District 110 on Clear Lakes Spring using calibration run E110712A001.



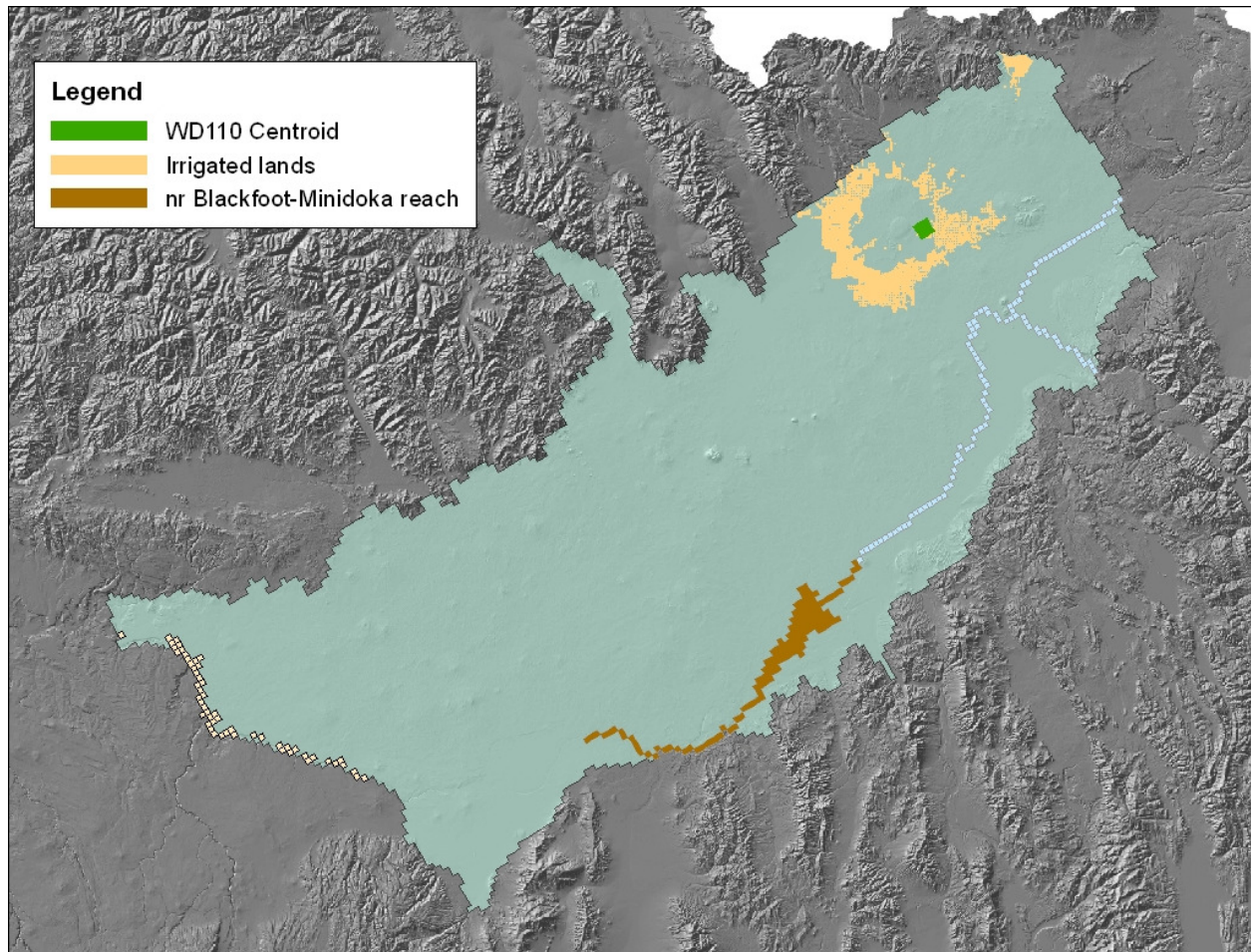
Impact of Water District 110 on Clear Lakes Spring using calibration run E110712A001.



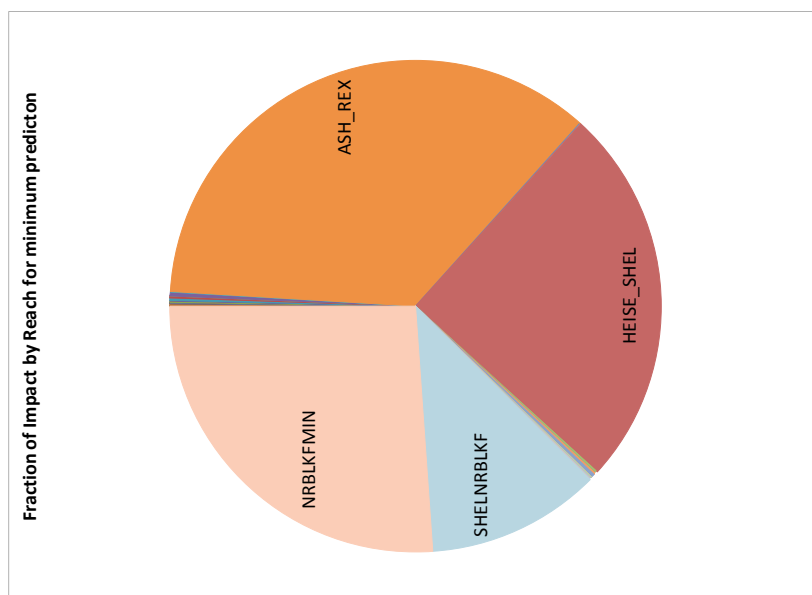
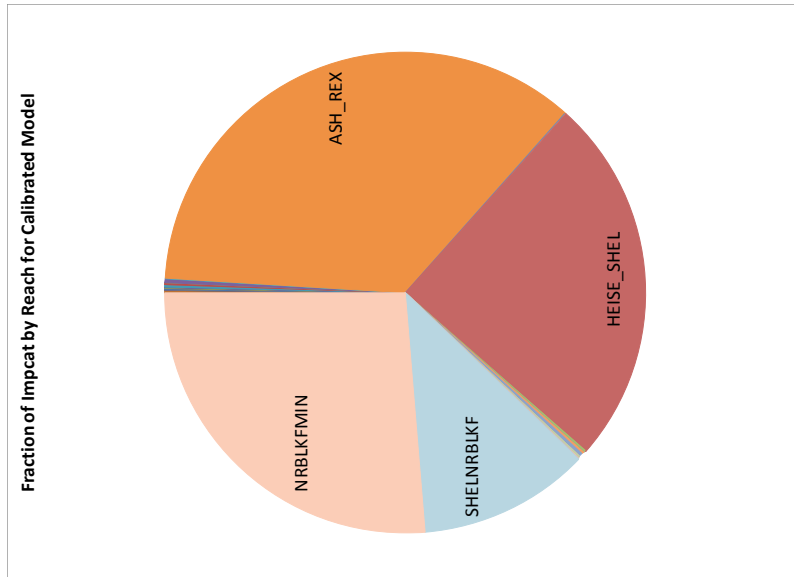
Impact of Water District 110 on Clear Lakes Spring using calibration run E110712A001.



Impact of Water District 110 on near Blackfoot-Minidoka using calibration run E120116A008.

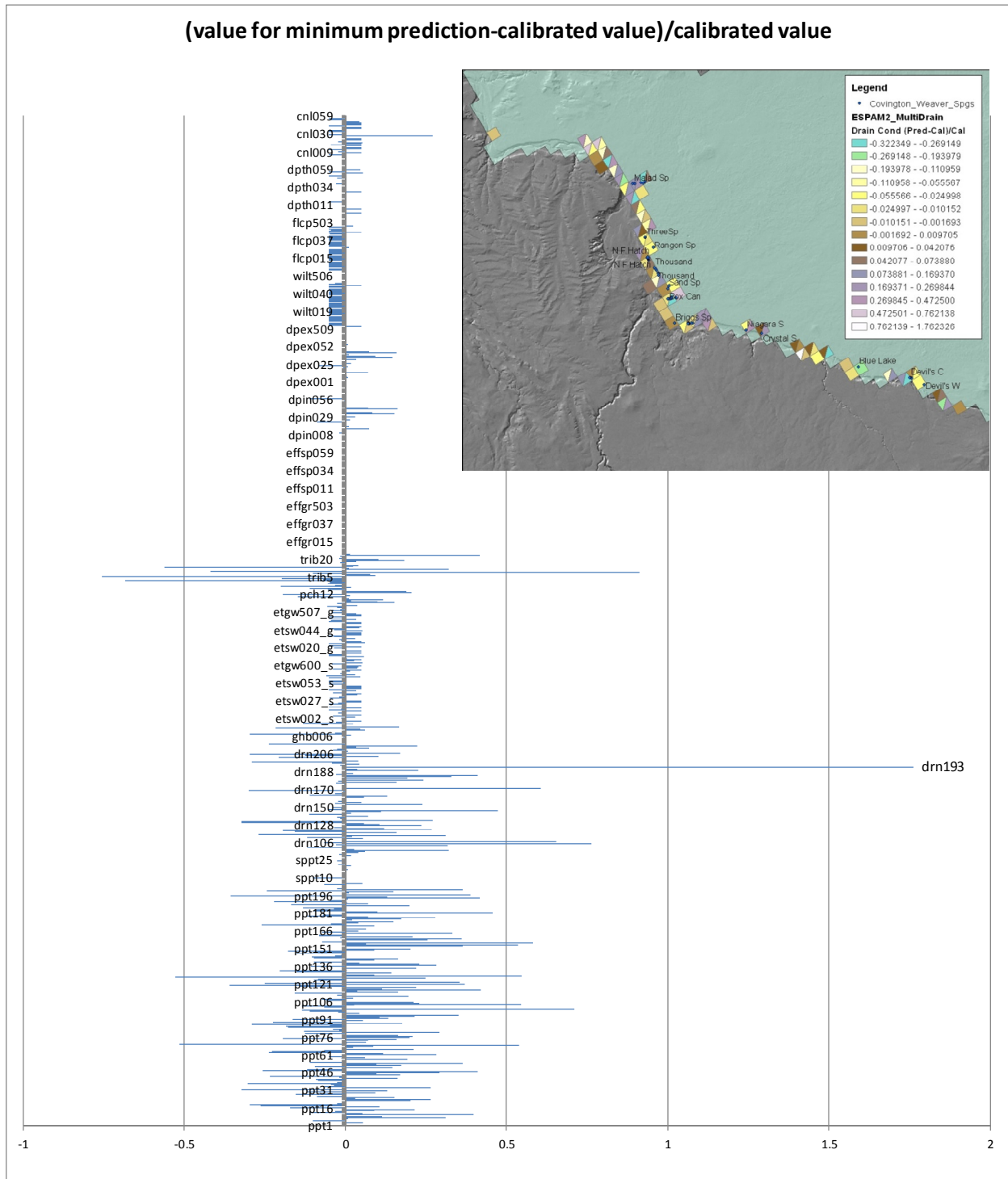


Impact of Water District 110 on near Blackfoot-Minidoka using calibration run E120116A008.

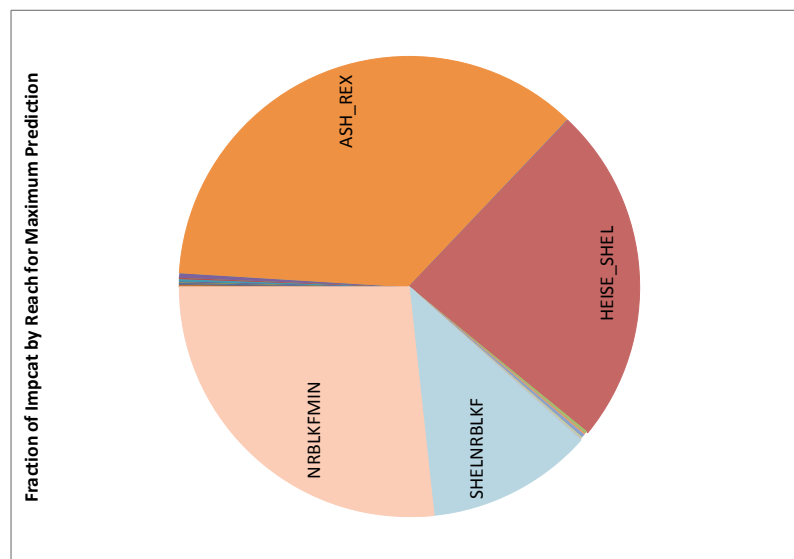
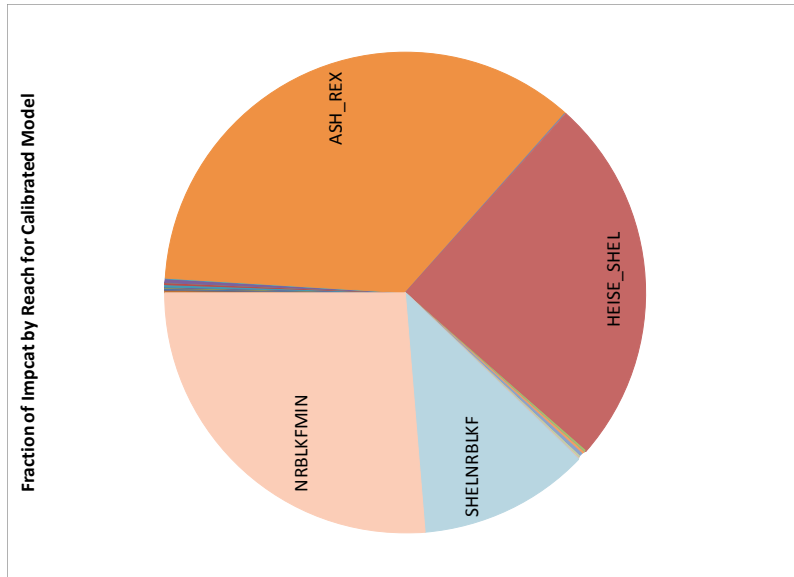




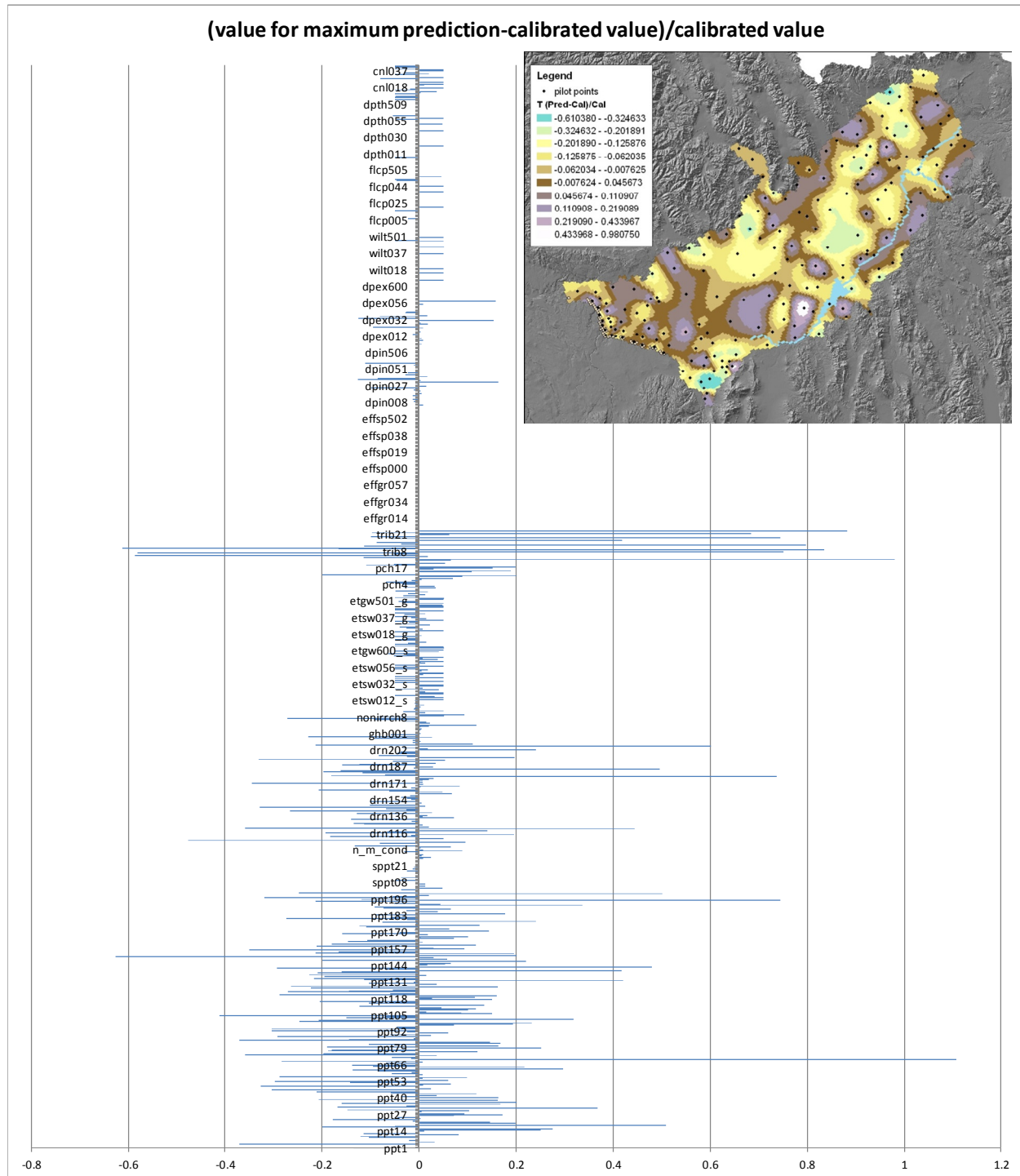
Impact of Water District 110 on near Blackfoot-Minidoka using calibration run E120116A008.



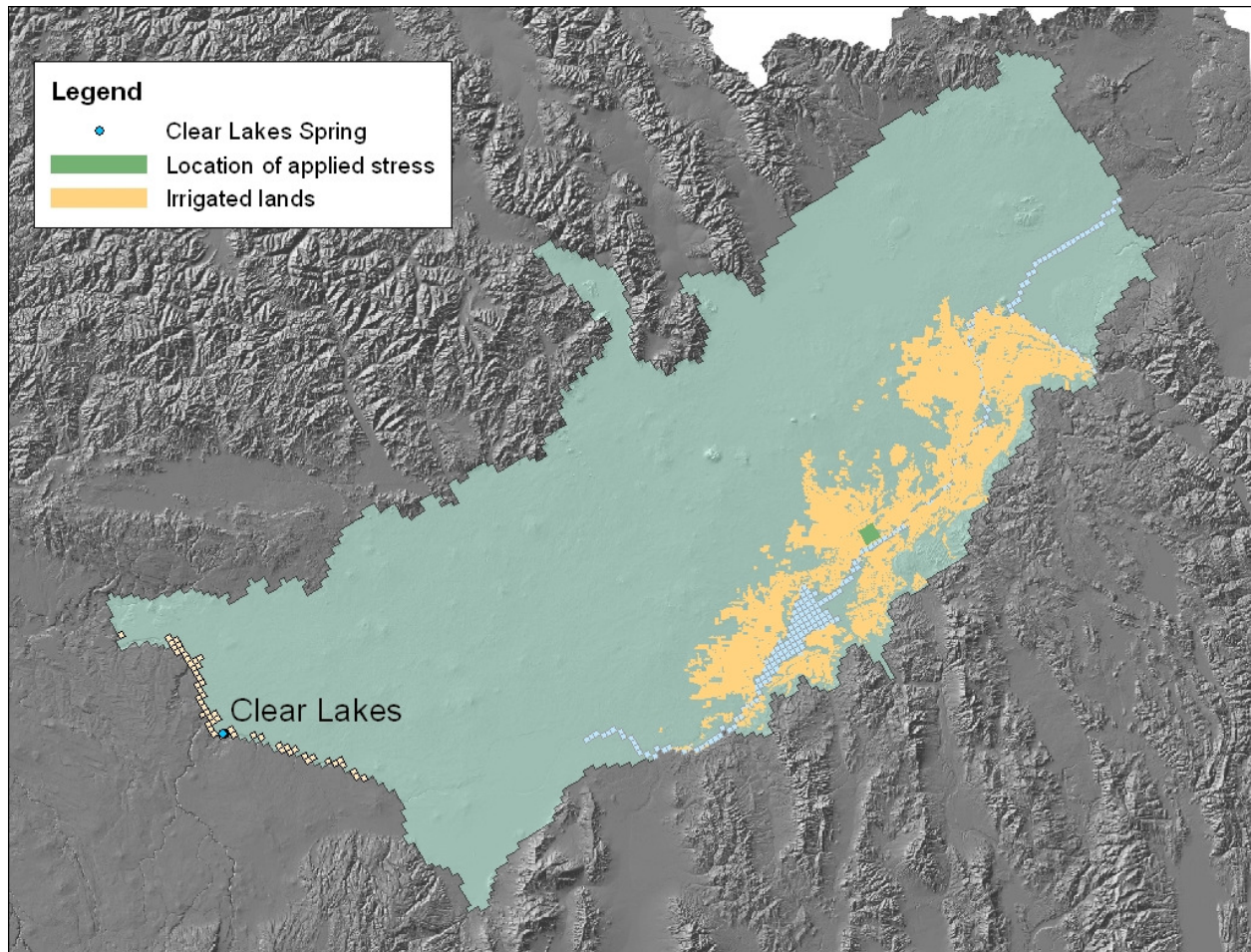
Impact of Water District 110 on near Blackfoot-Minidoka using calibration run E120116A008.



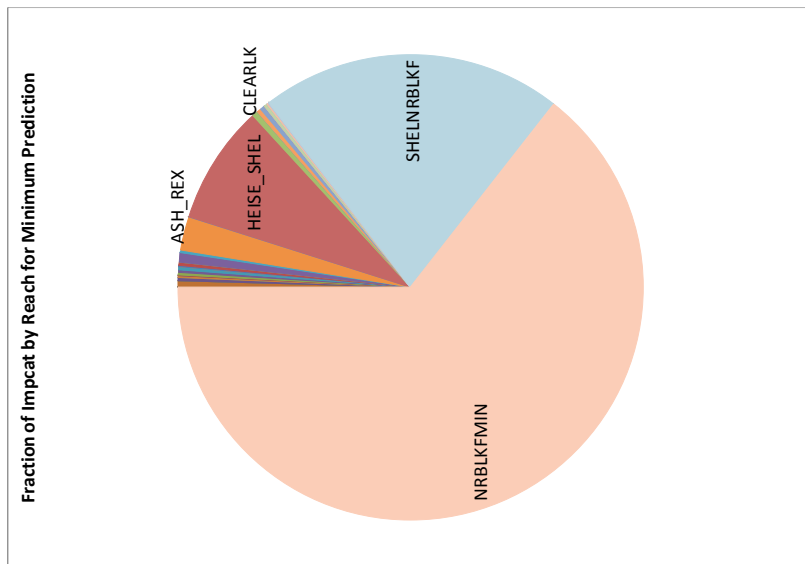
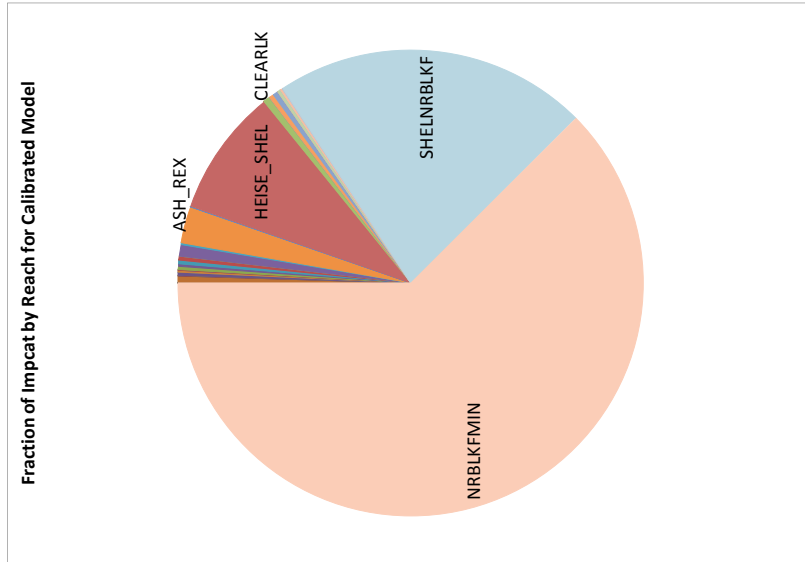
Impact of Water District 110 on near Blackfoot-Minidoka using calibration run E120116A008.



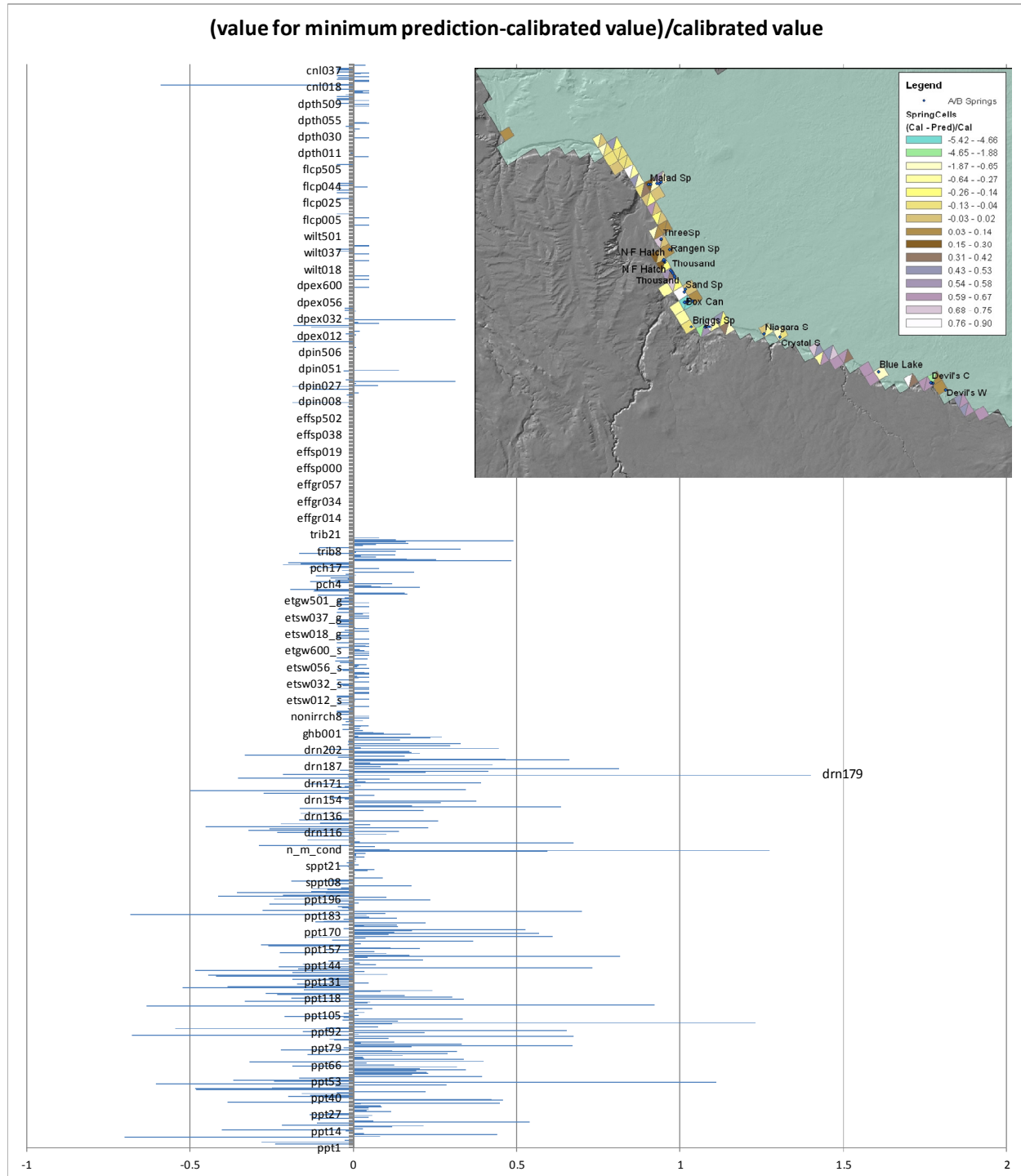
Impact of Water District 120 on Clear Lakes Spring using calibration run E110712A001.



Impact of Water District 120 on Clear Lakes Spring using calibration run E110712A001.

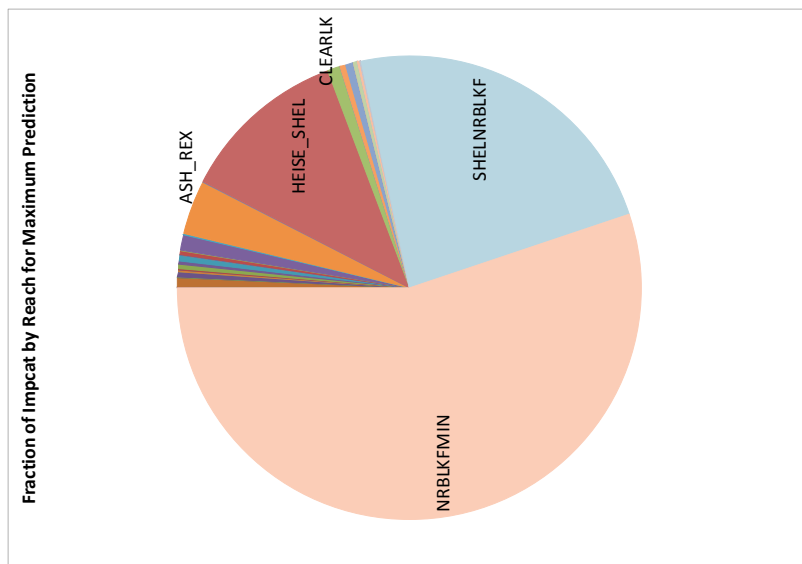
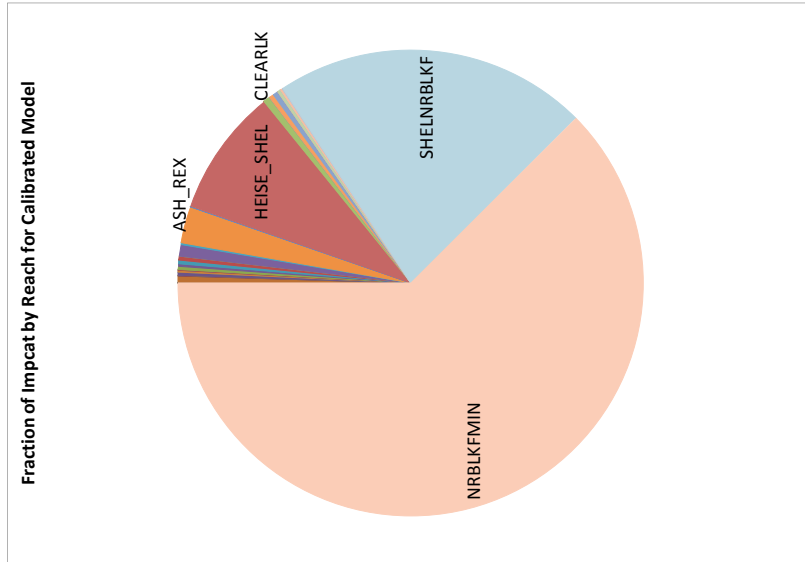


Impact of Water District 120 on Clear Lakes Spring using calibration run E110712A001.

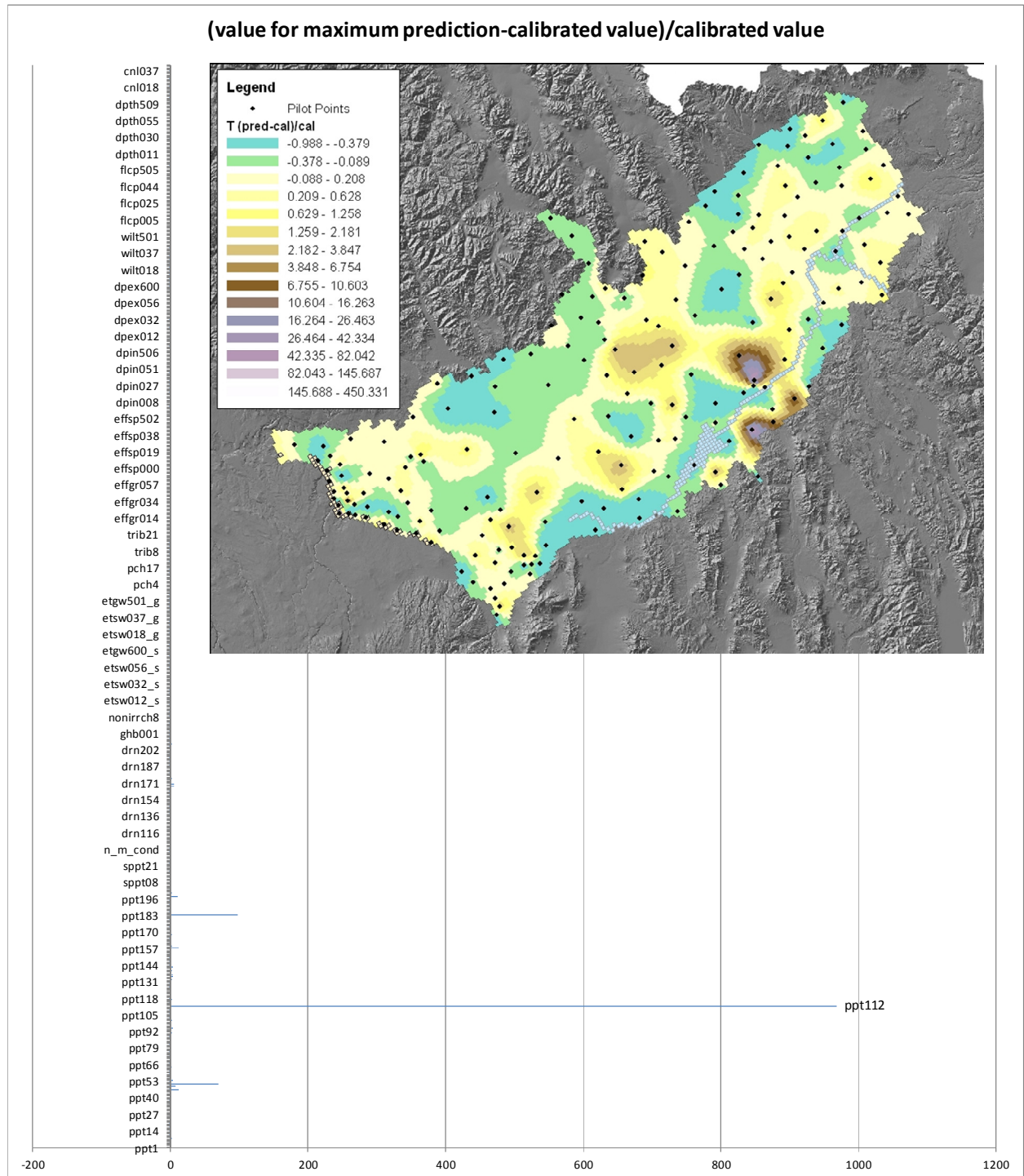




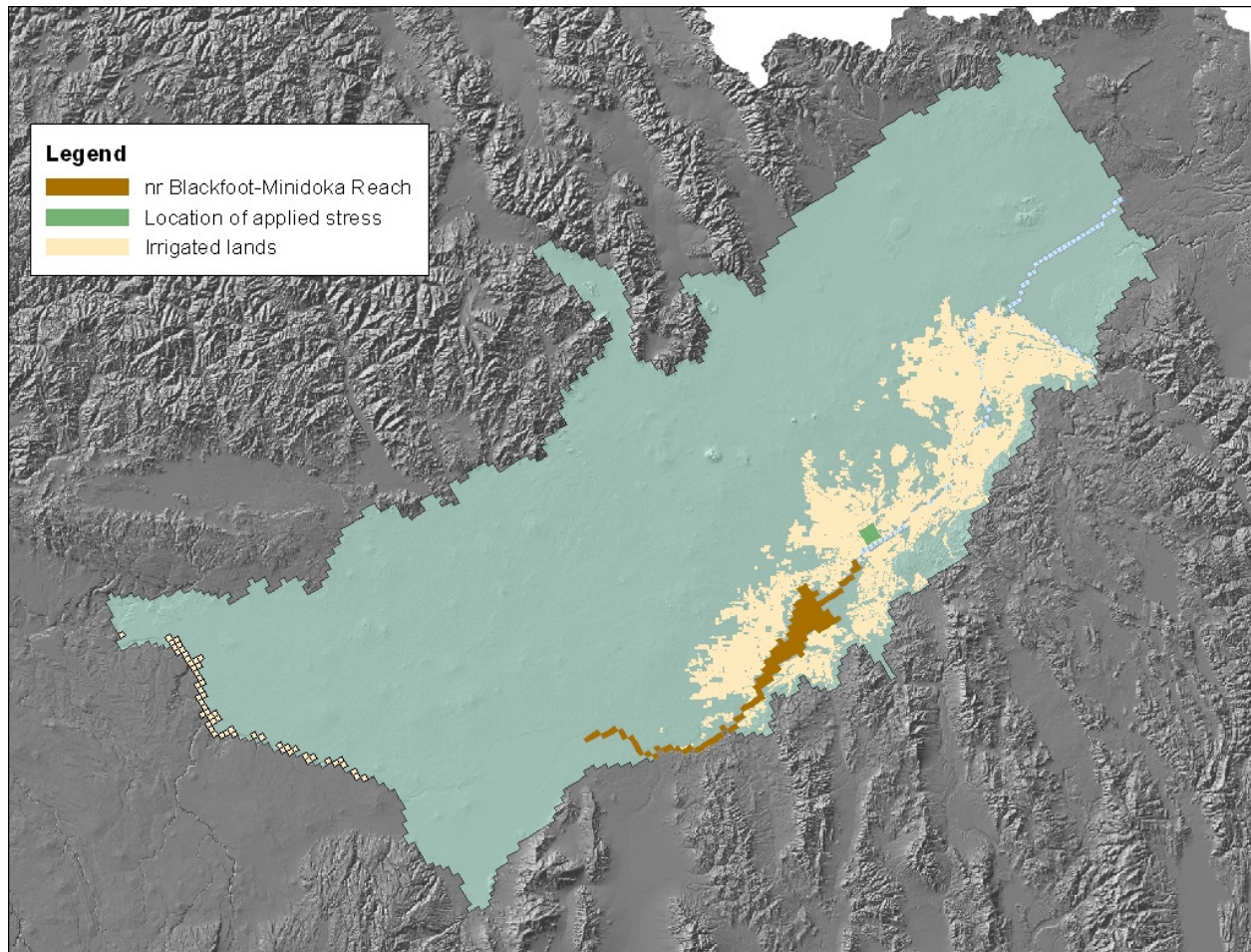
Impact of Water District 120 on Clear Lakes Spring using calibration run E110712A001.



Impact of Water District 120 on Clear Lakes Spring using calibration run E110712A001.

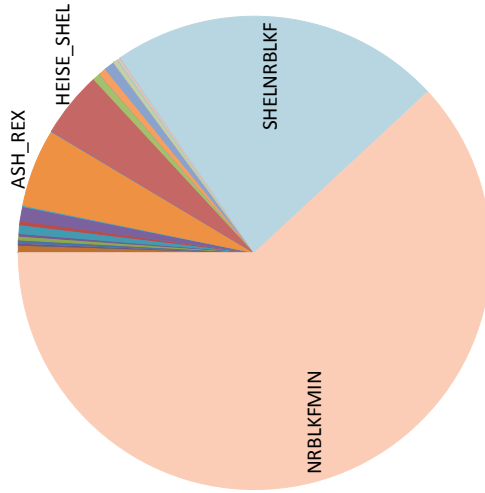


Impact of Water District 120 on near Blackfoot-Minidoka using calibration run E120116A008.

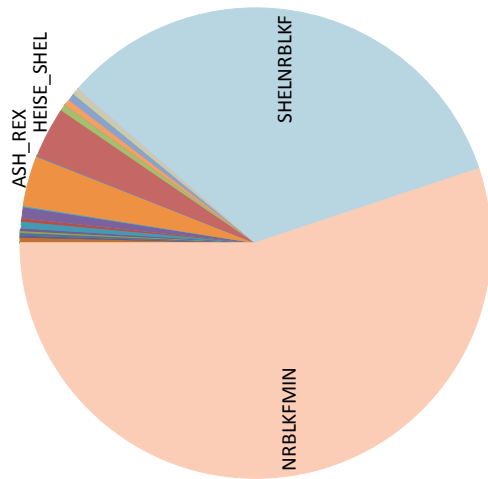


Impact of Water District 120 on near Blackfoot-Minidoka using calibration run E120116A008.

Fraction of Impact by Reach for Calibrated Model

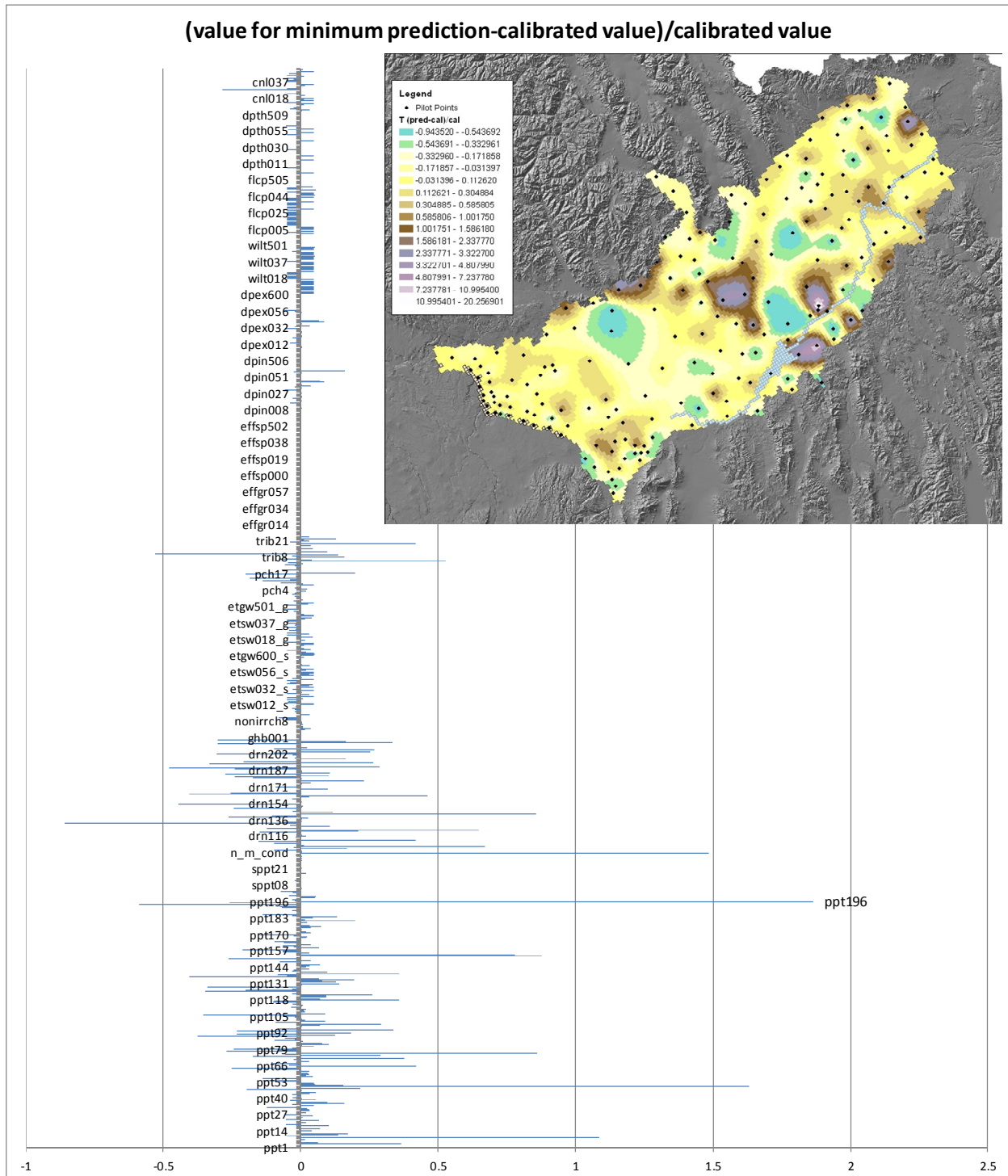


Fraction of Impact by Reach for Minimum Prediction



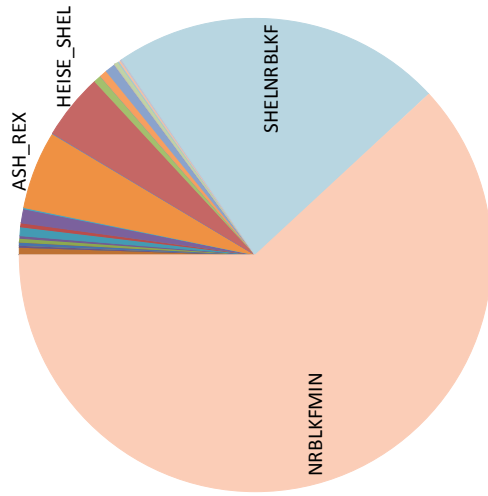


Impact of Water District 120 on near Blackfoot-Minidoka using calibration run E120116A008.

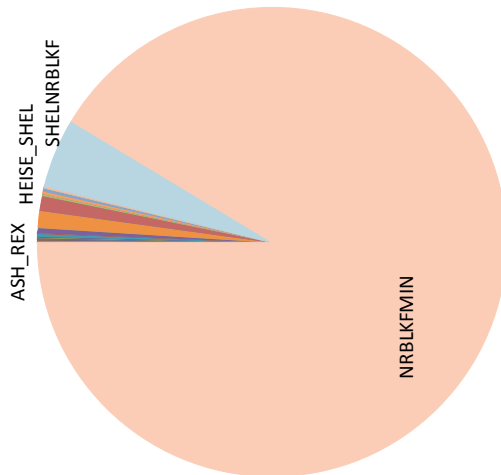


Impact of Water District 120 on near Blackfoot-Minidoka using calibration run E120116A008.

Fraction of Impact by Reach for Calibrated Model

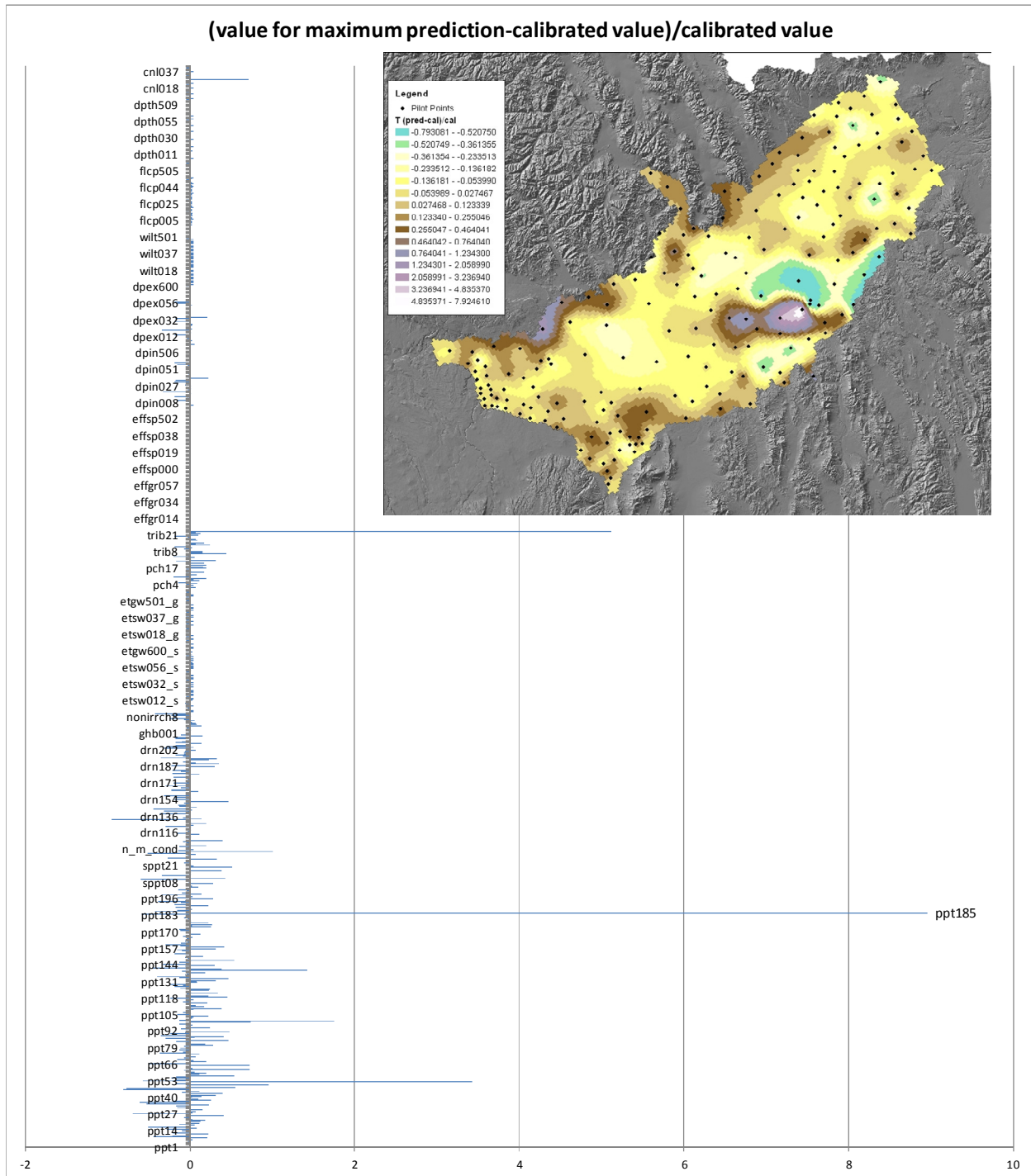


Fraction of Impact by Reach for Maximum Prediction

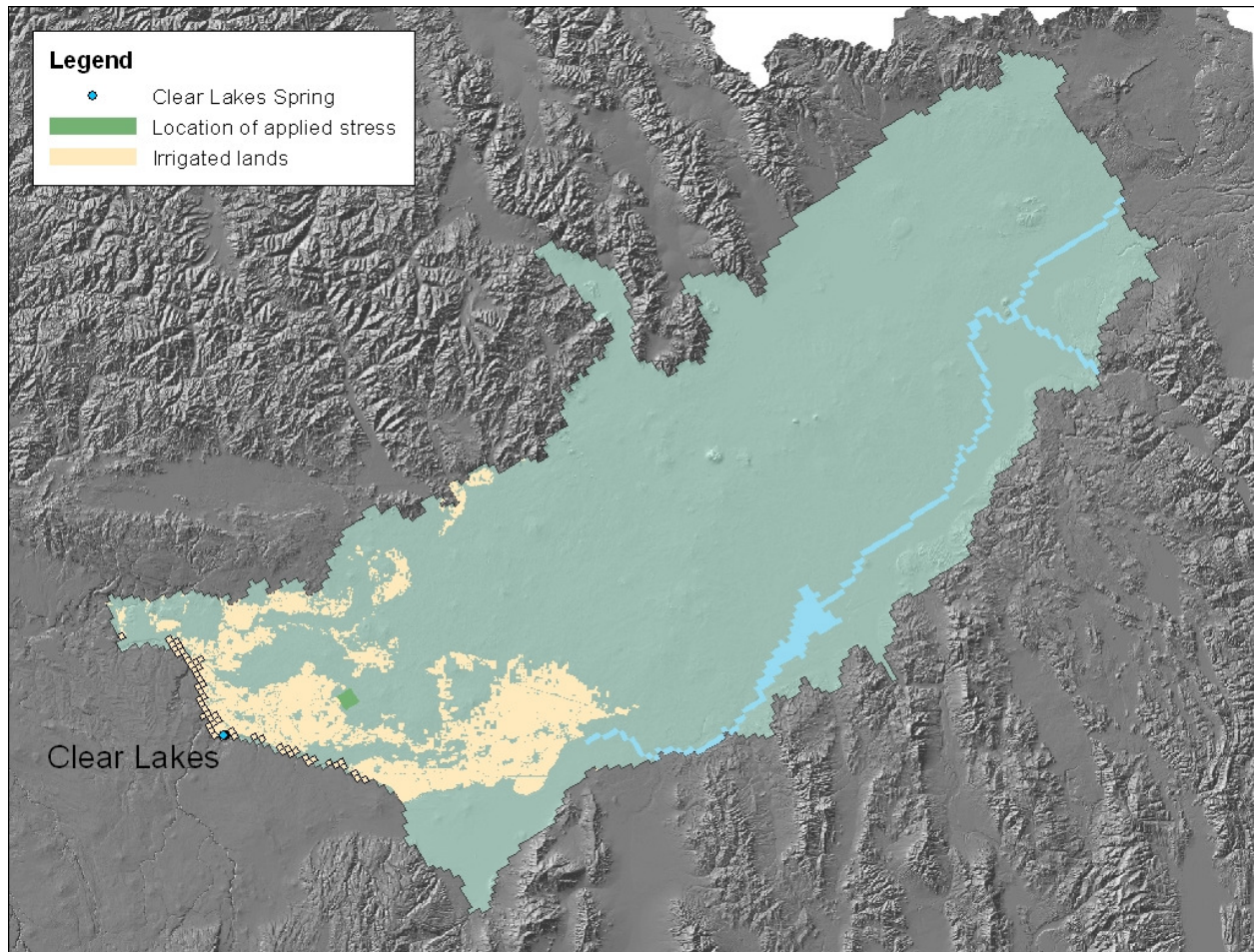




Impact of Water District 120 on near Blackfoot-Minidoka using calibration run E120116A008.

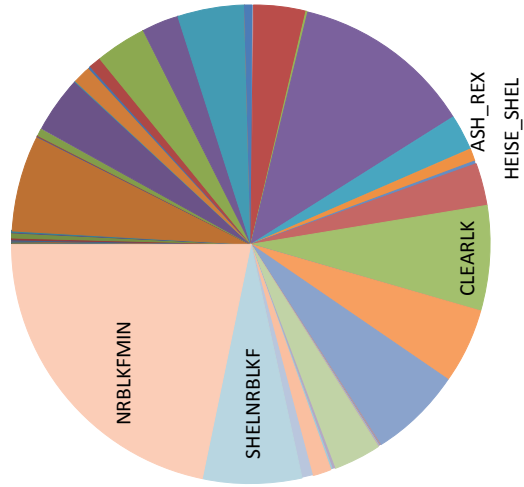


Impact of Water District 130 on Clear Lakes Spring using calibration run E110712A001.

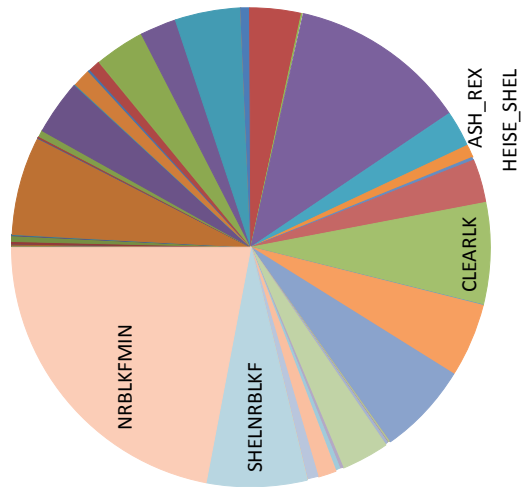


Impact of Water District 130 on Clear Lakes Spring using calibration run E110712A001.

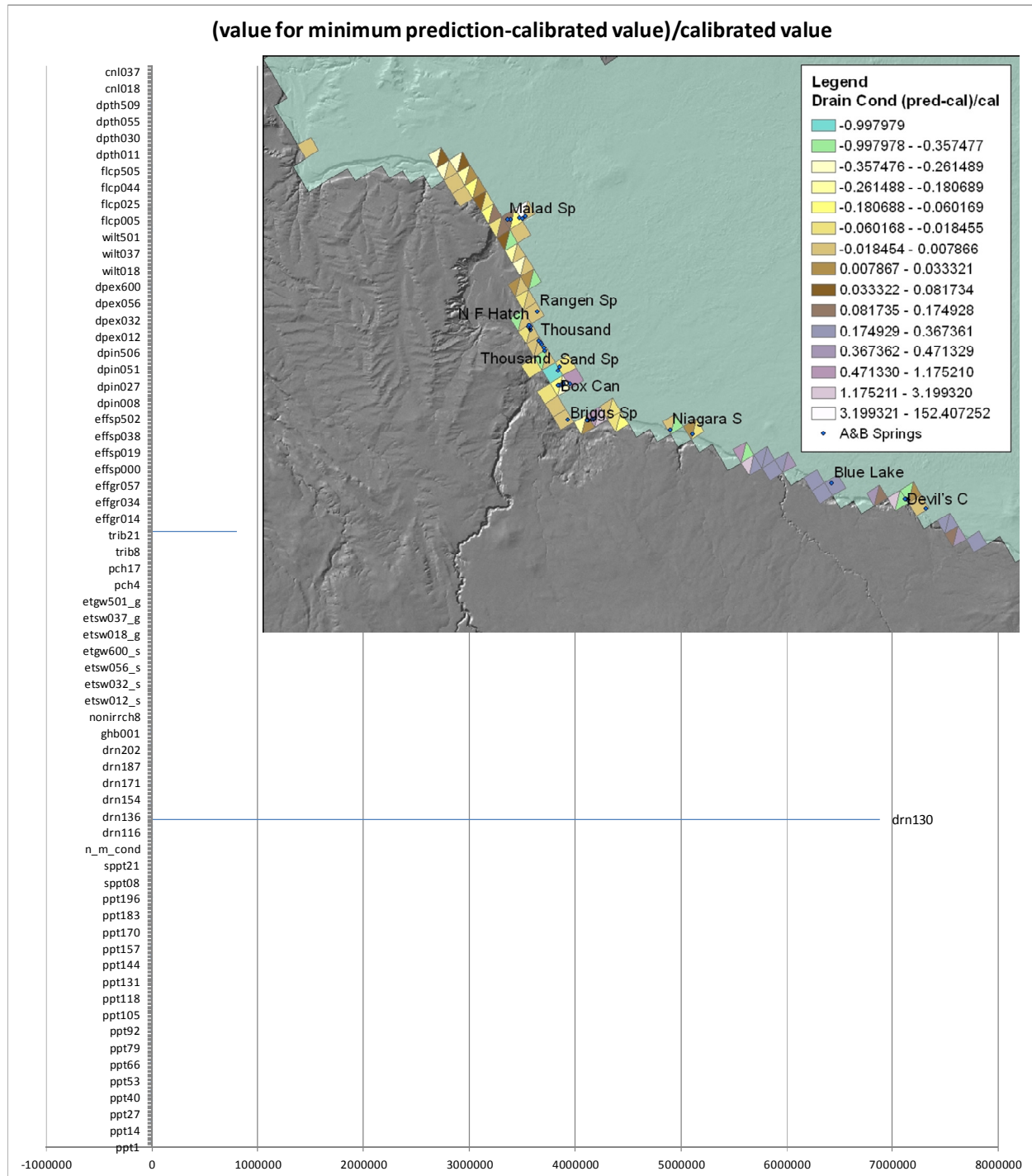
Fraction of Impact by Reach for Calibrated Model



Fraction of Impact by Reach for Minimum Prediction

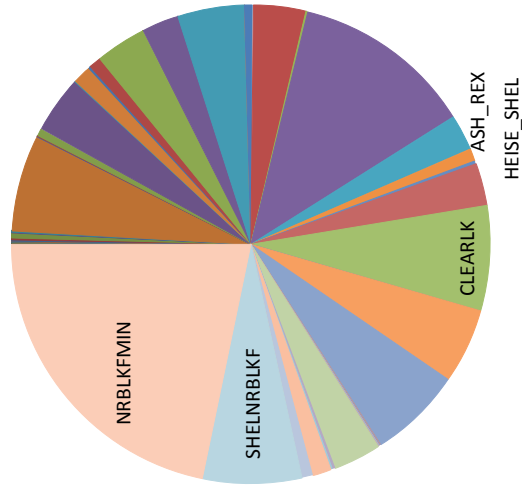


Impact of Water District 130 on Clear Lakes Spring using calibration run E110712A001.

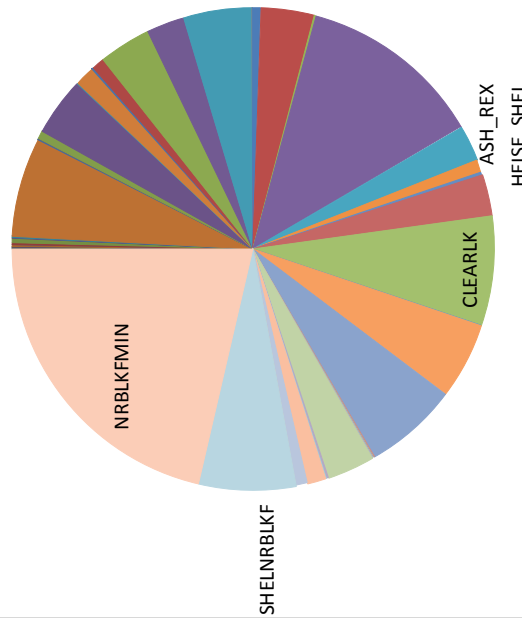


Impact of Water District 130 on Clear Lakes Spring using calibration run E110712A001.

Fraction of Impact by Reach for Calibrated Model

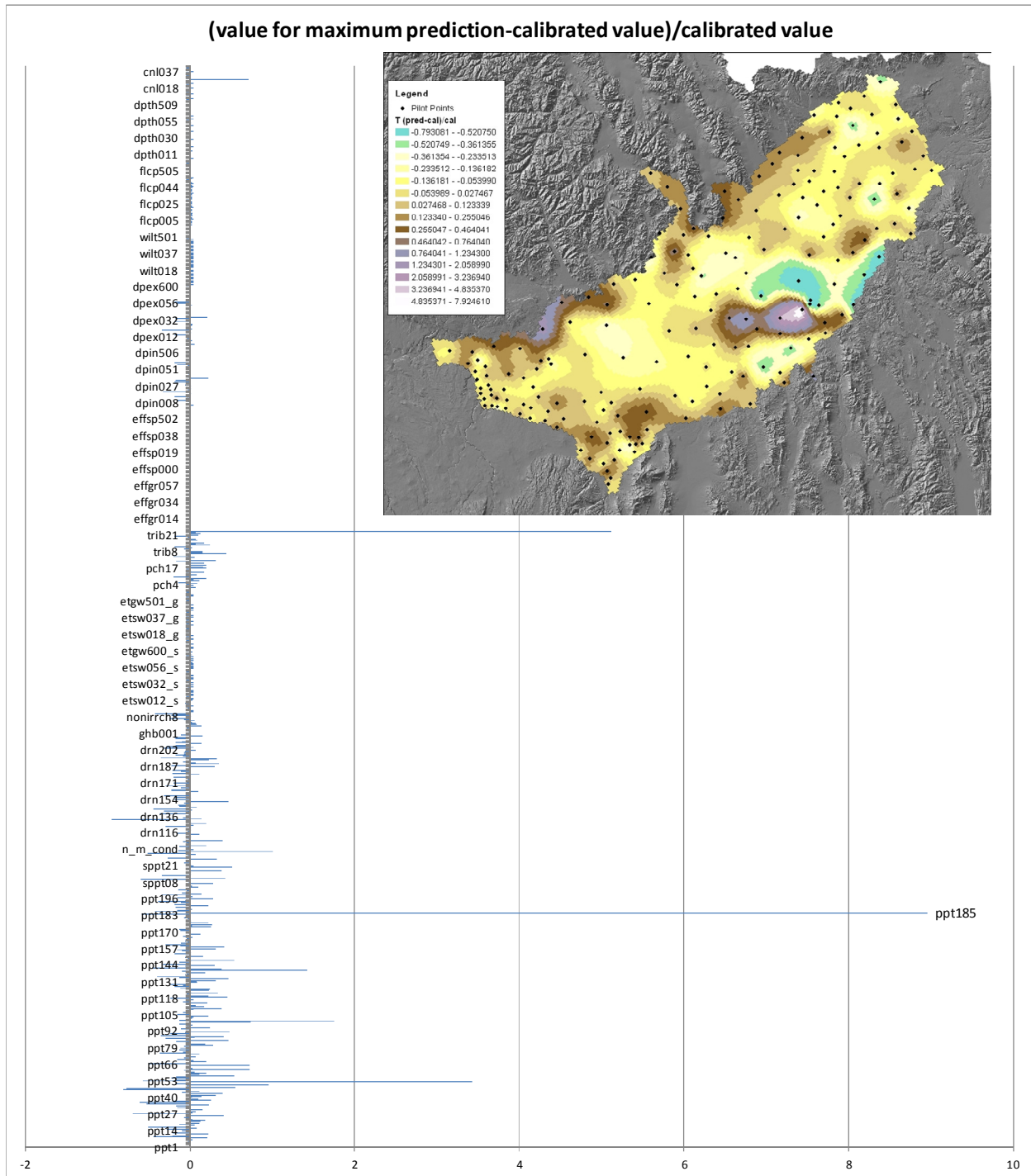


Fraction of Impact by Reach for Maximum Prediction



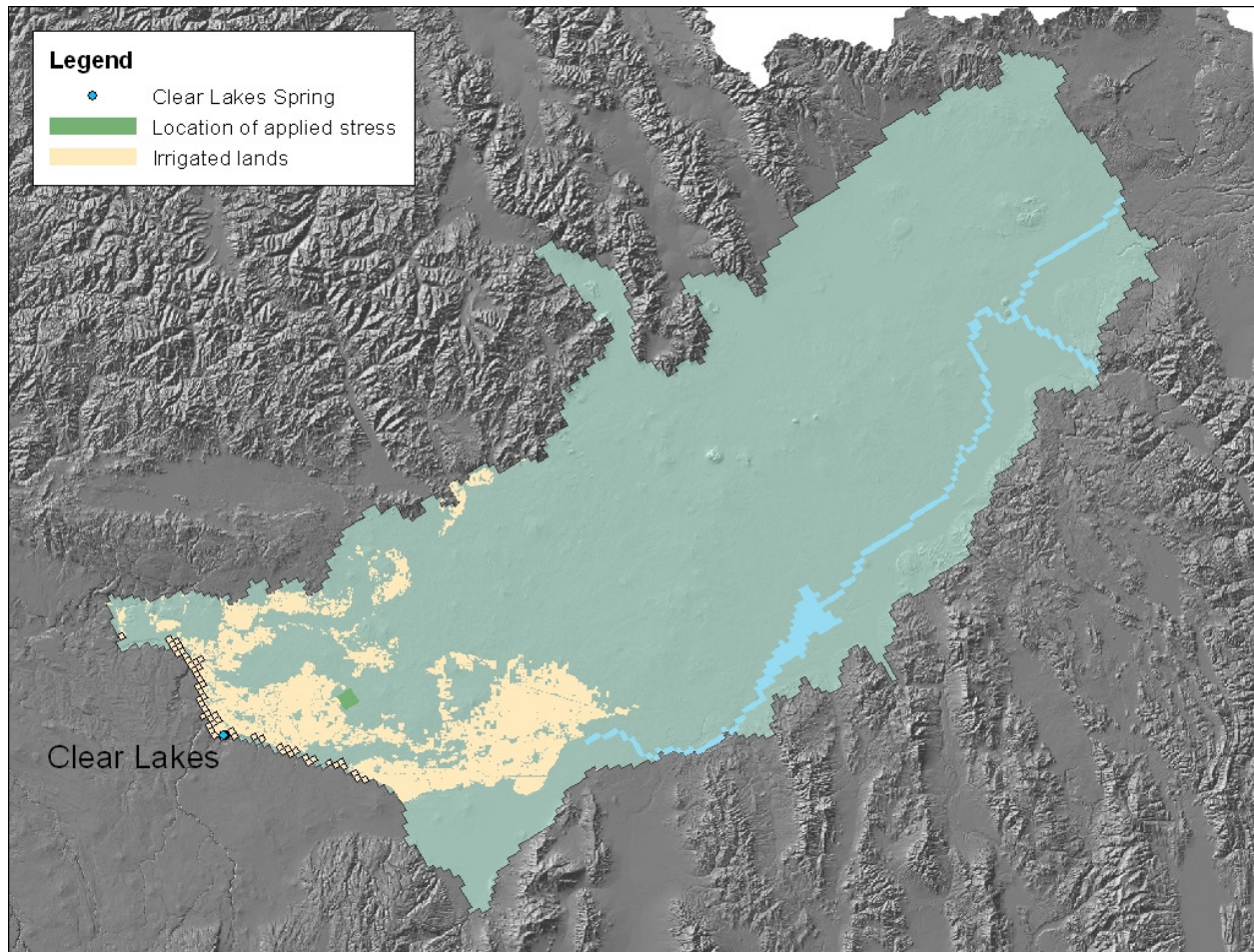


Impact of Water District 130 on Clear Lakes Spring using calibration run E110712A001.

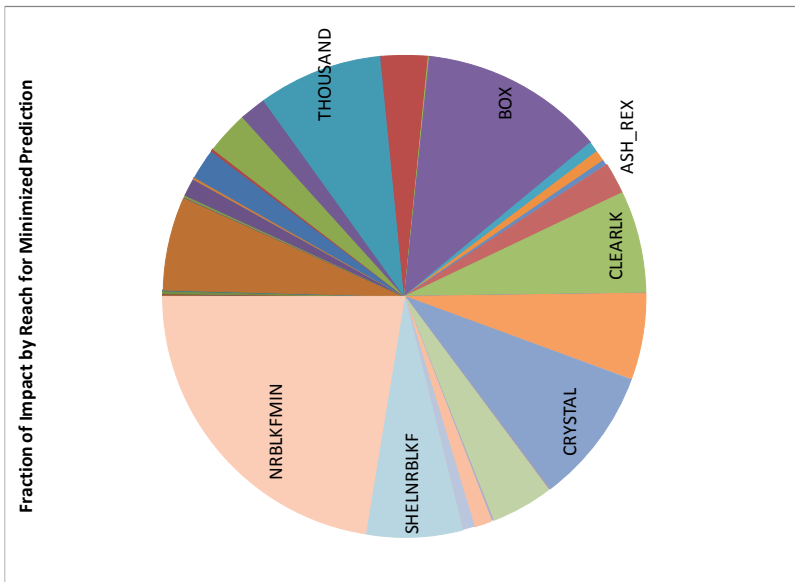
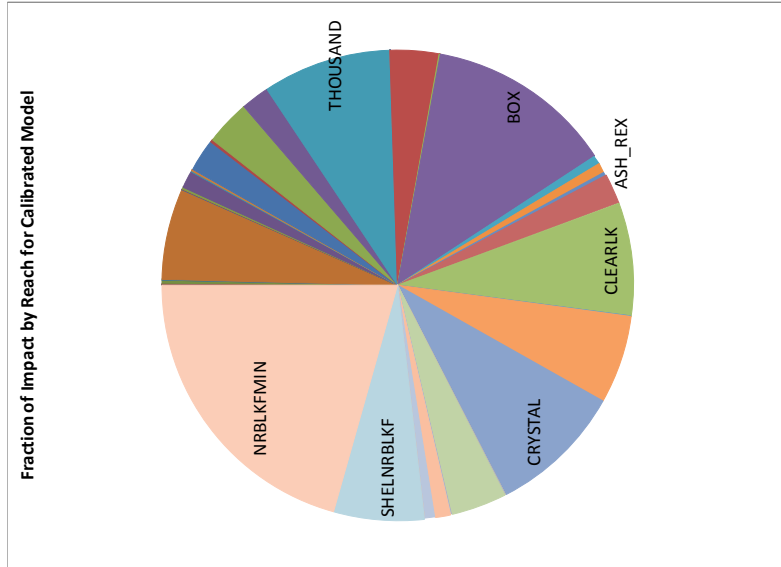




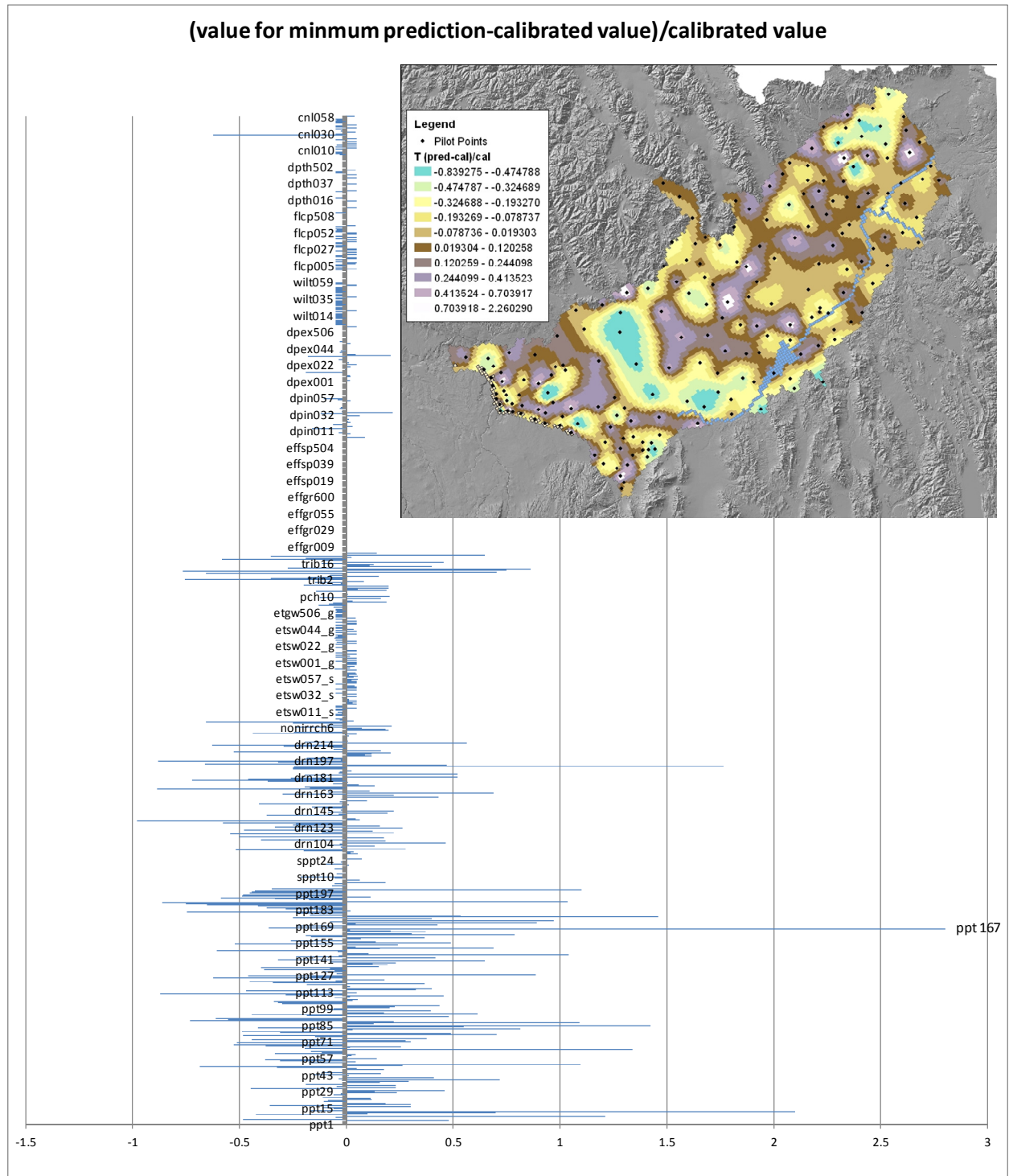
Impact of Water District 130 on Clear Lakes Spring using calibration run E121025A001.



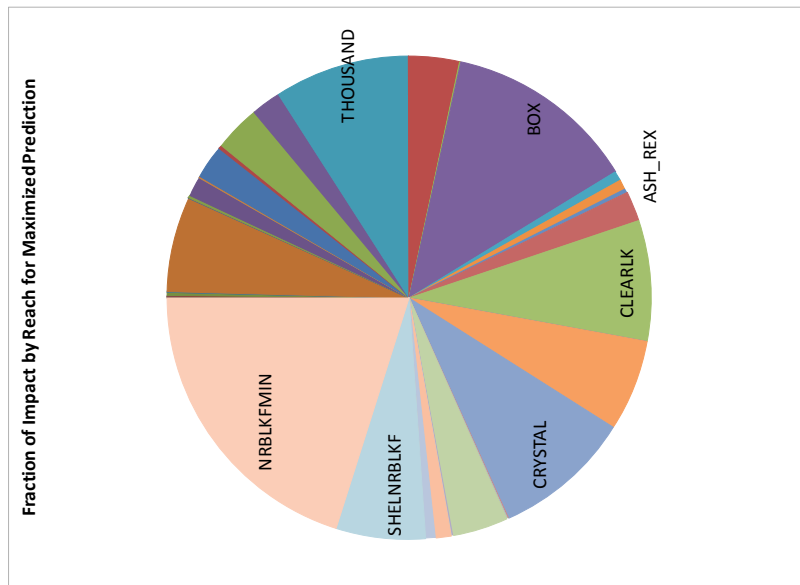
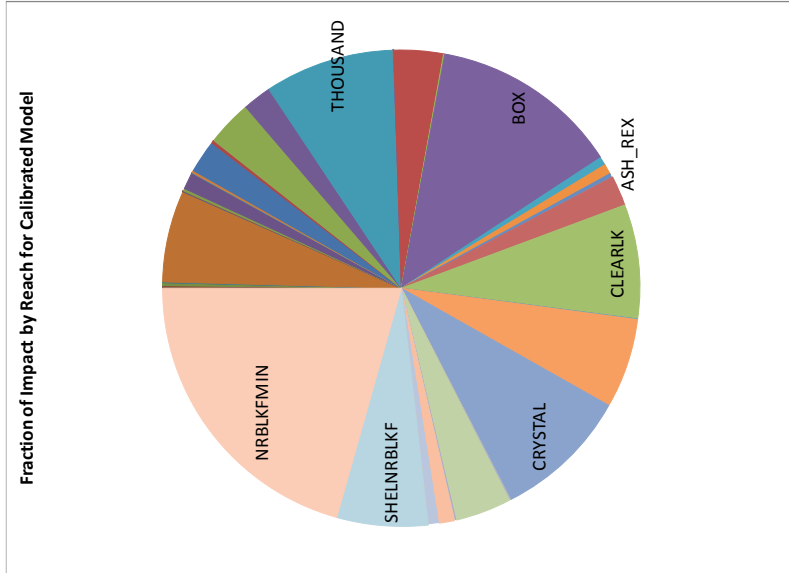
Impact of Water District 130 on Clear Lakes Spring using calibration run E121025A001.



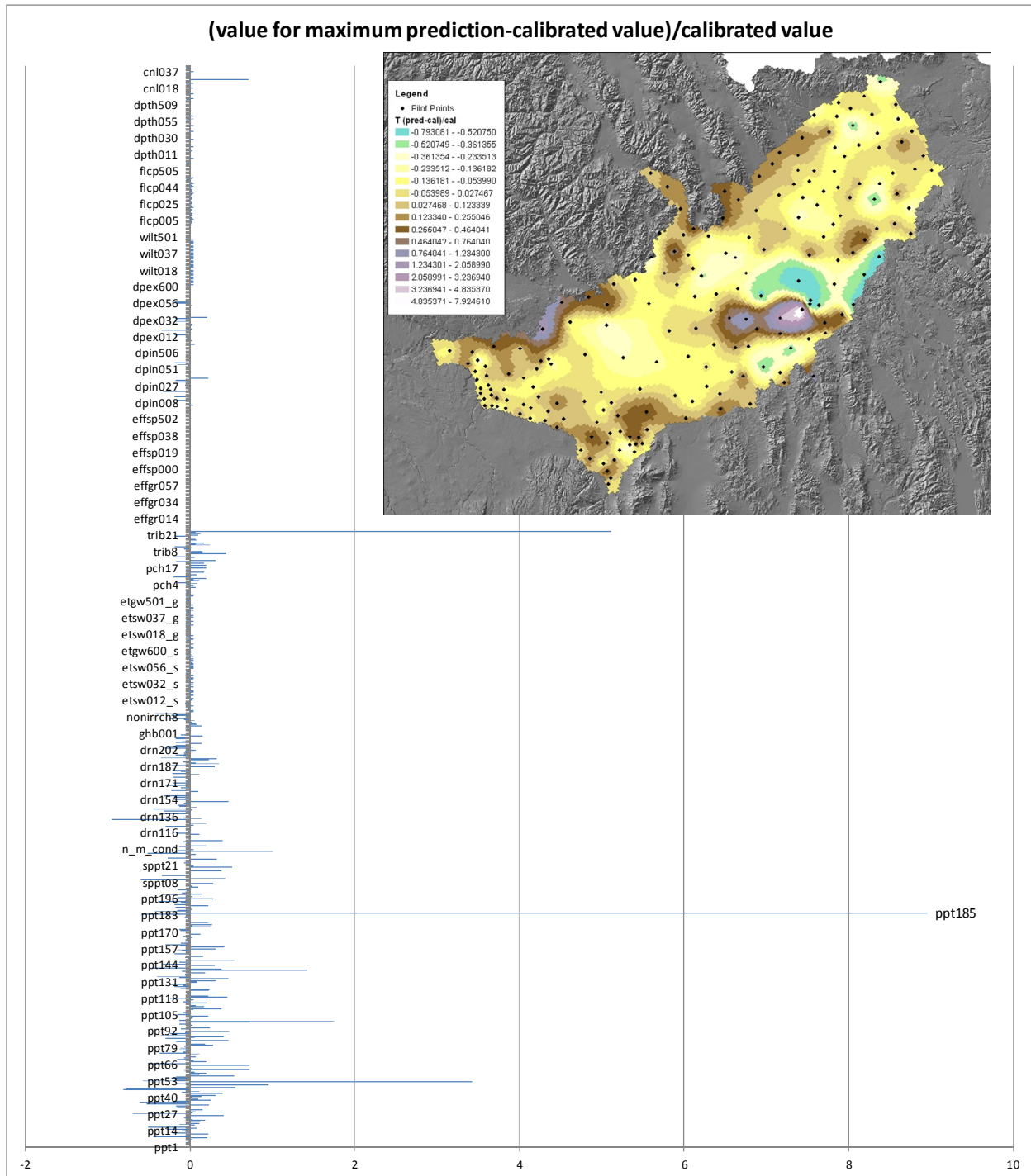
Impact of Water District 130 on Clear Lakes Spring using calibration run E121025A001.



Impact of Water District 130 on Clear Lakes Spring using calibration run E121025A001.

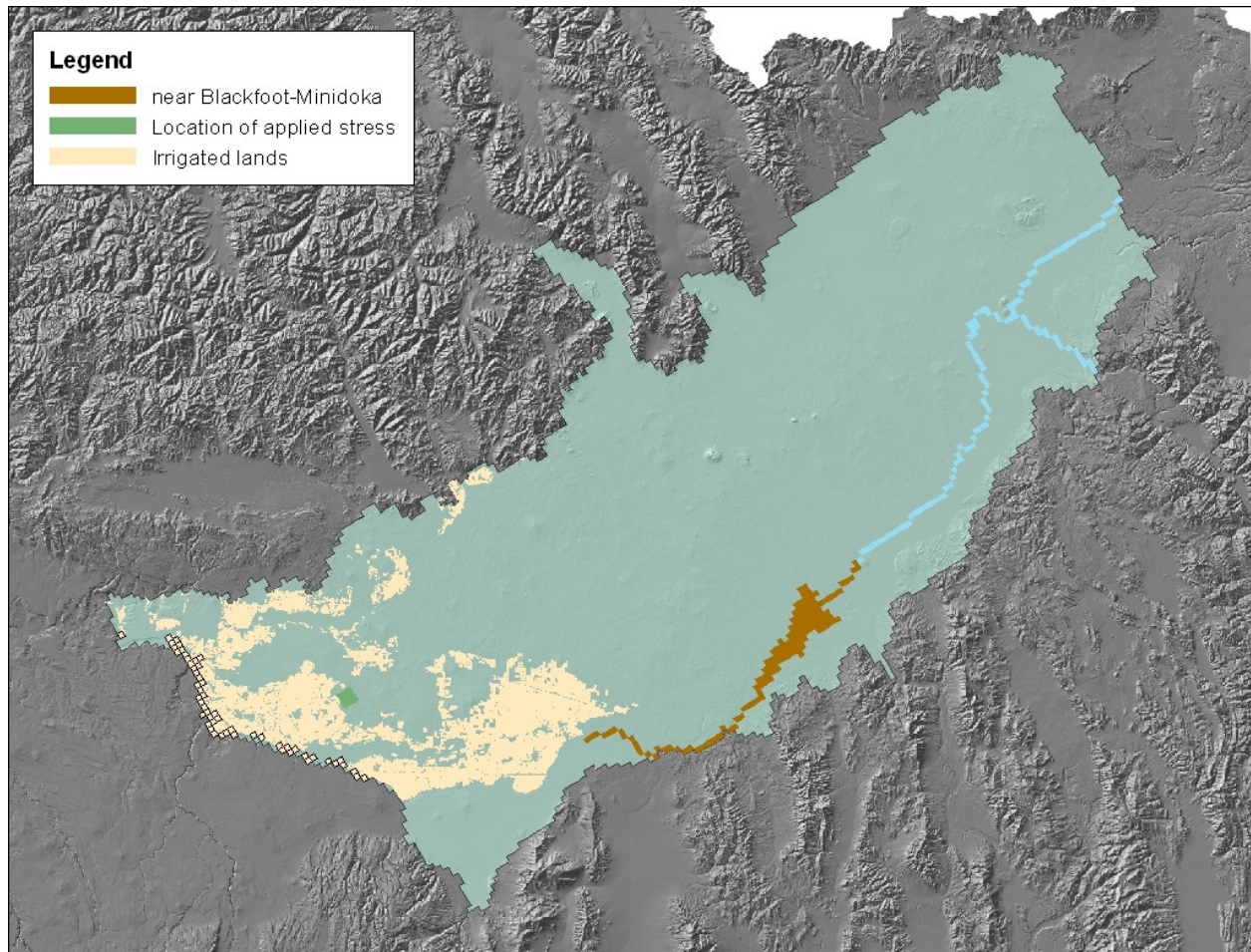


Impact of Water District 130 on Clear Lakes Spring using calibration run E121025A001.





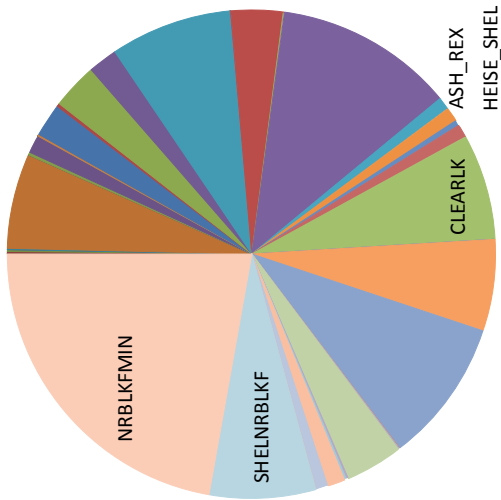
Impact of Water District 130 on near Blackfoot-Minidoka using calibration run E120116A008.



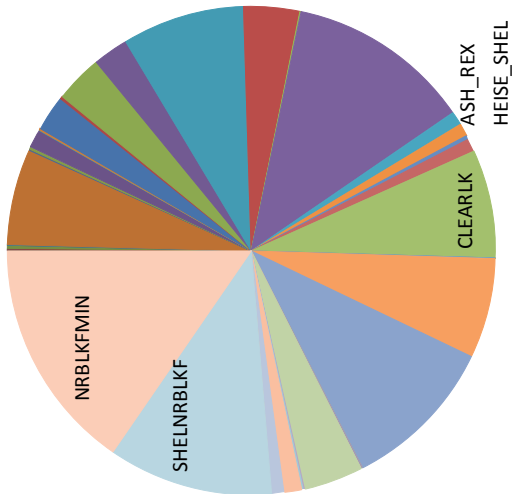


Impact of Water District 130 on near Blackfoot-Minidoka using calibration run E120116A008.

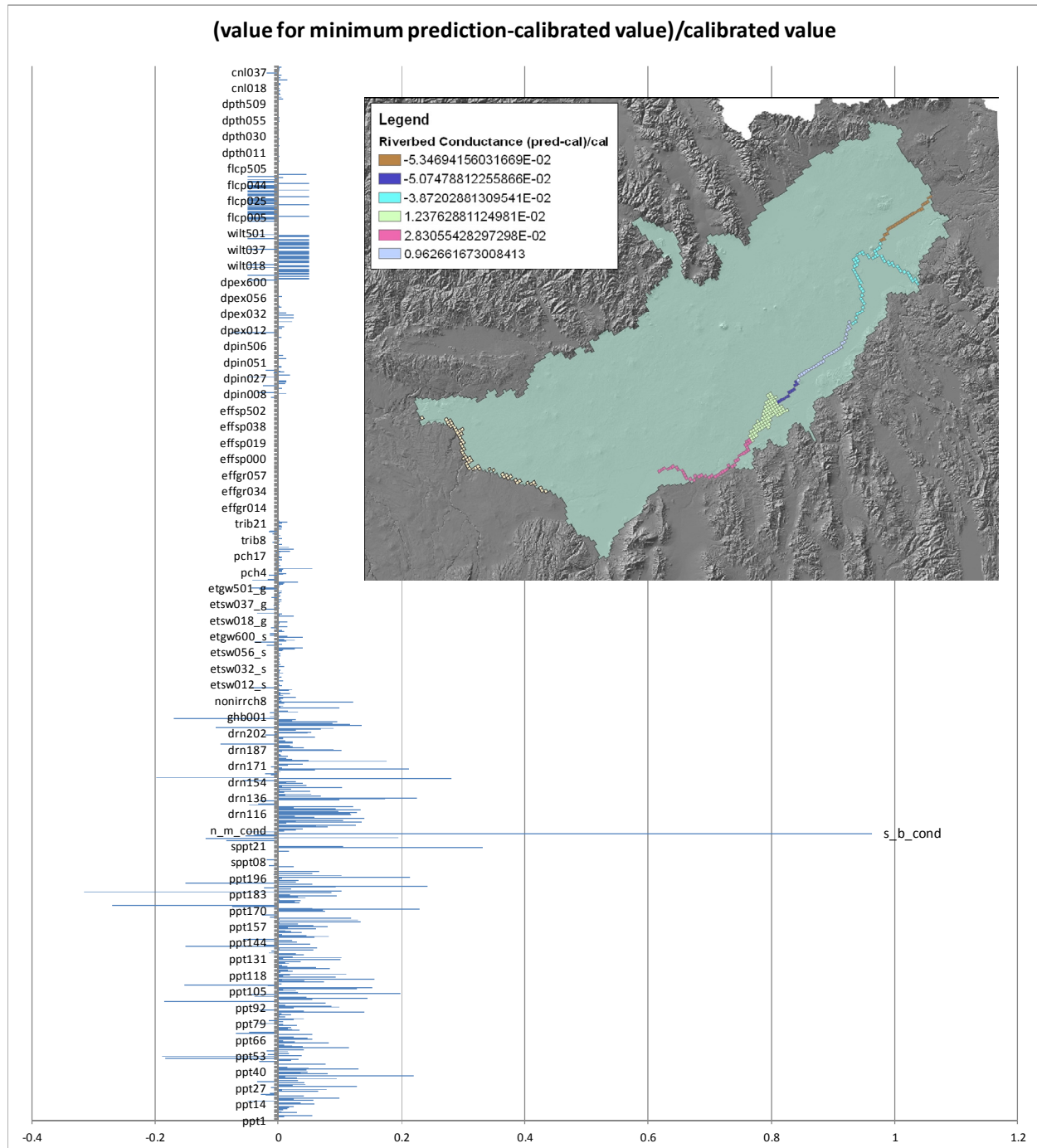
Fraction of Impact by Reach for Calibrated Model



Fraction of Impact by Reach for Minimum Prediction

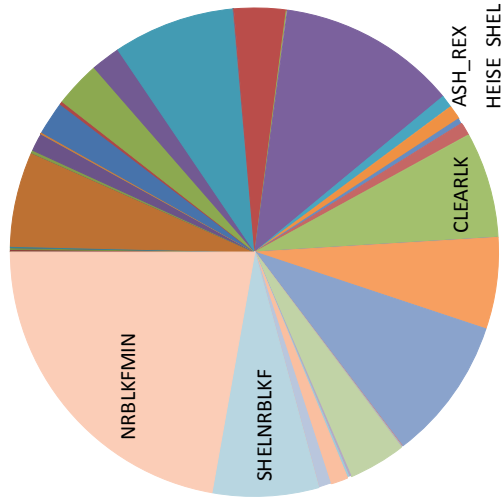


Impact of Water District 130 on near Blackfoot-Minidoka using calibration run E120116A008.

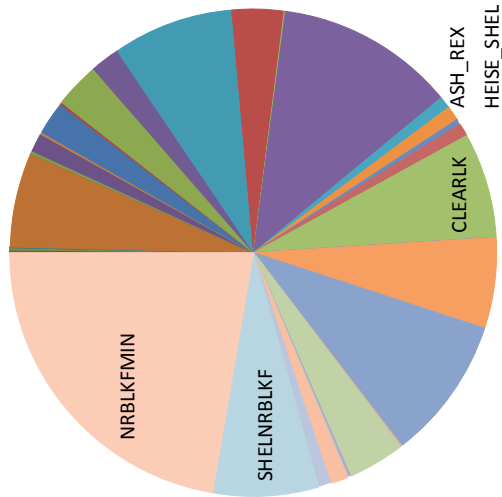


Impact of Water District 130 on near Blackfoot-Minidoka using calibration run E120116A008.

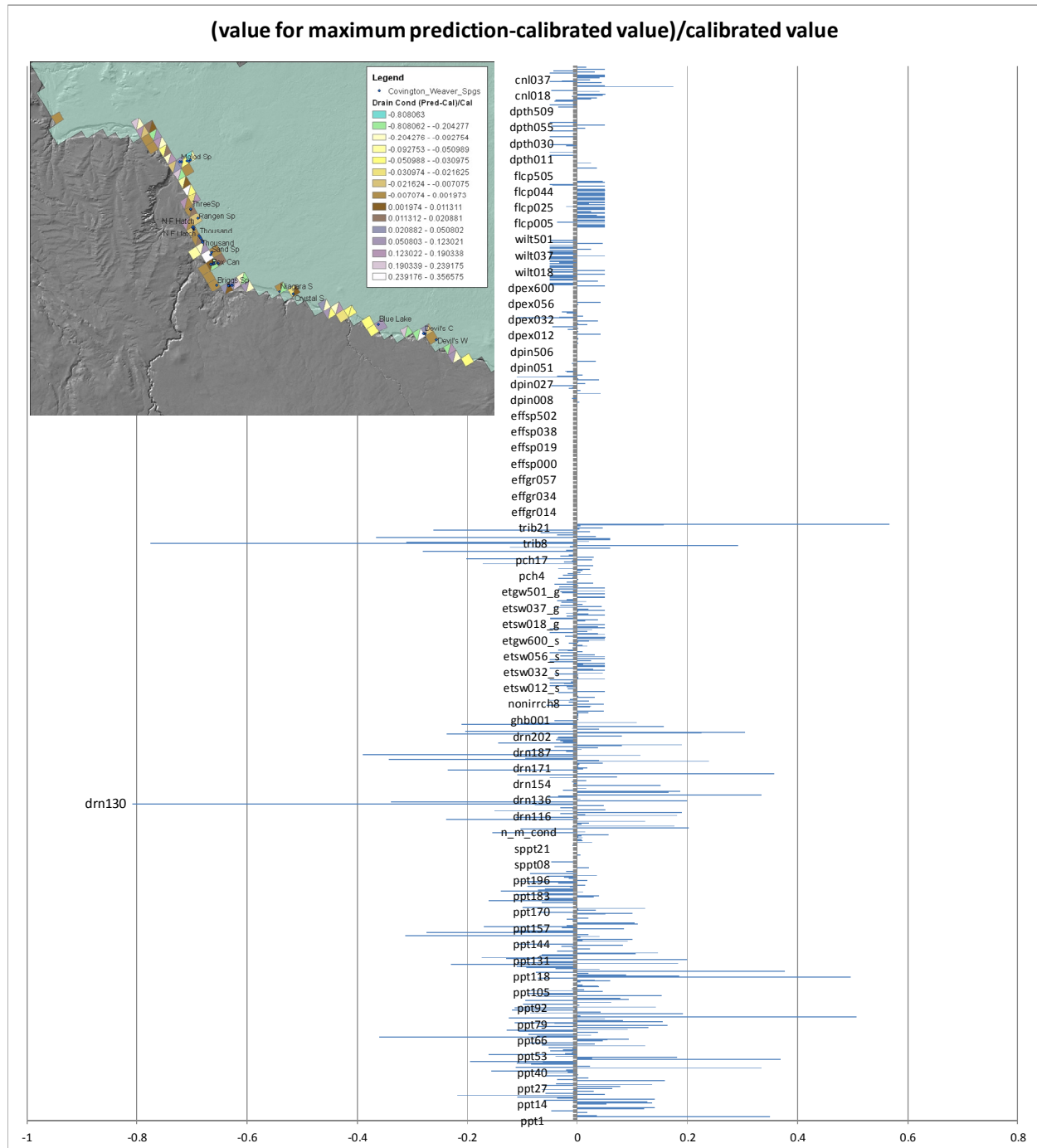
Fraction of Impact by Reach for Calibrated Model



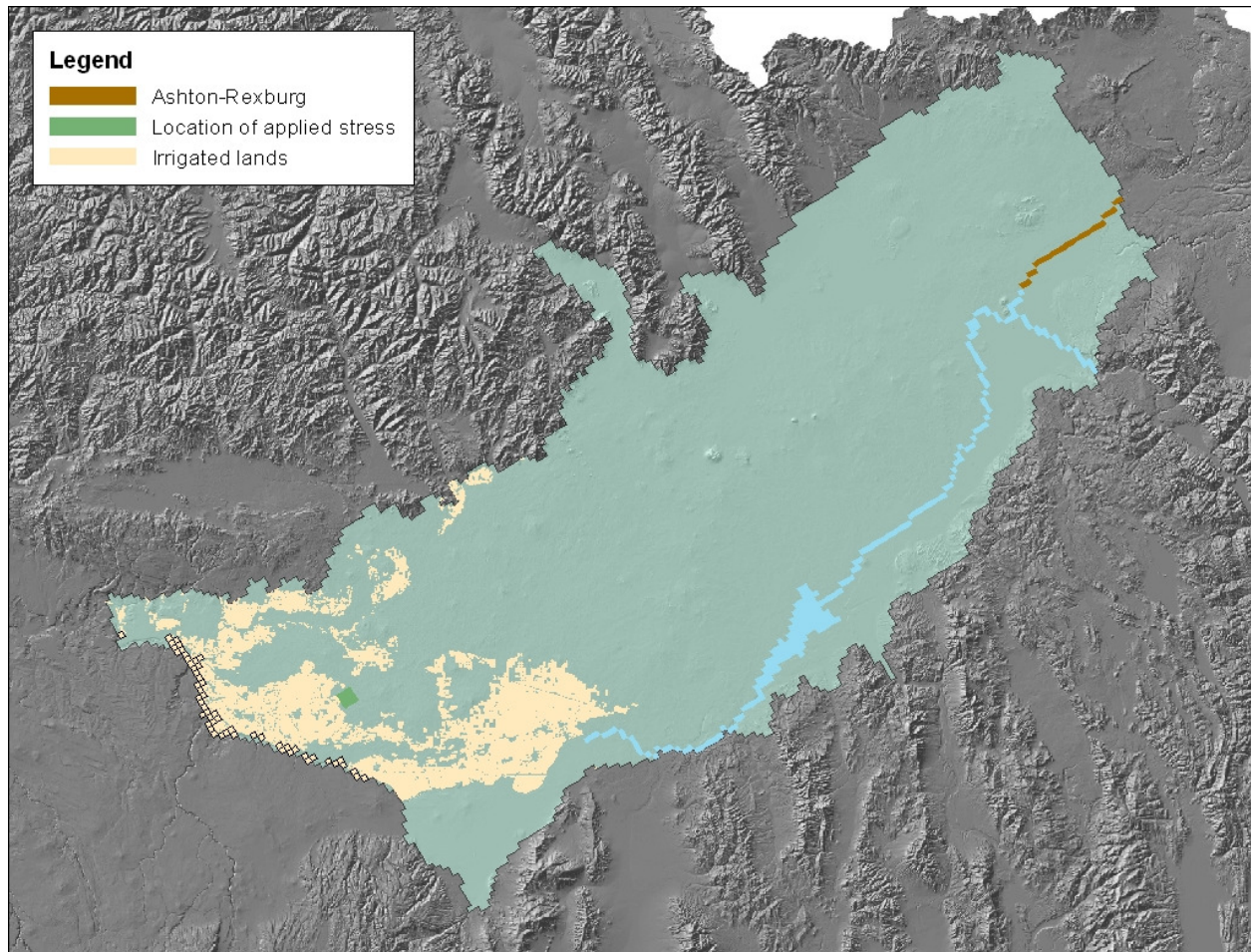
Fraction of Impact by Reach for Maximum Prediction



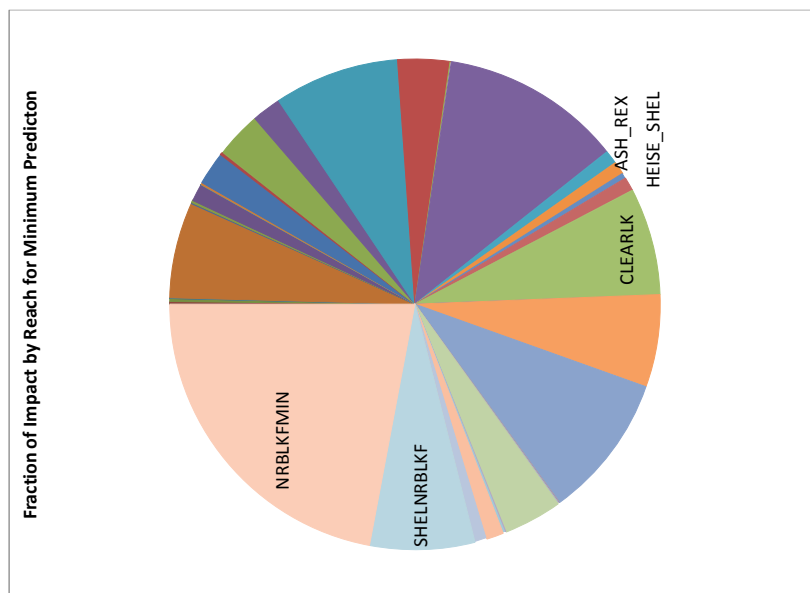
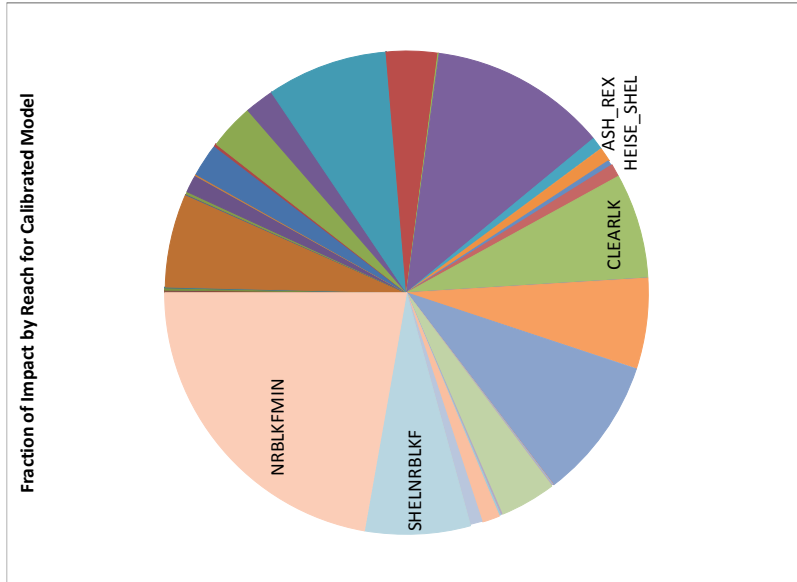
Impact of Water District 130 on near Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 130 on Ashton-Rexburg using calibration run E120116A008.

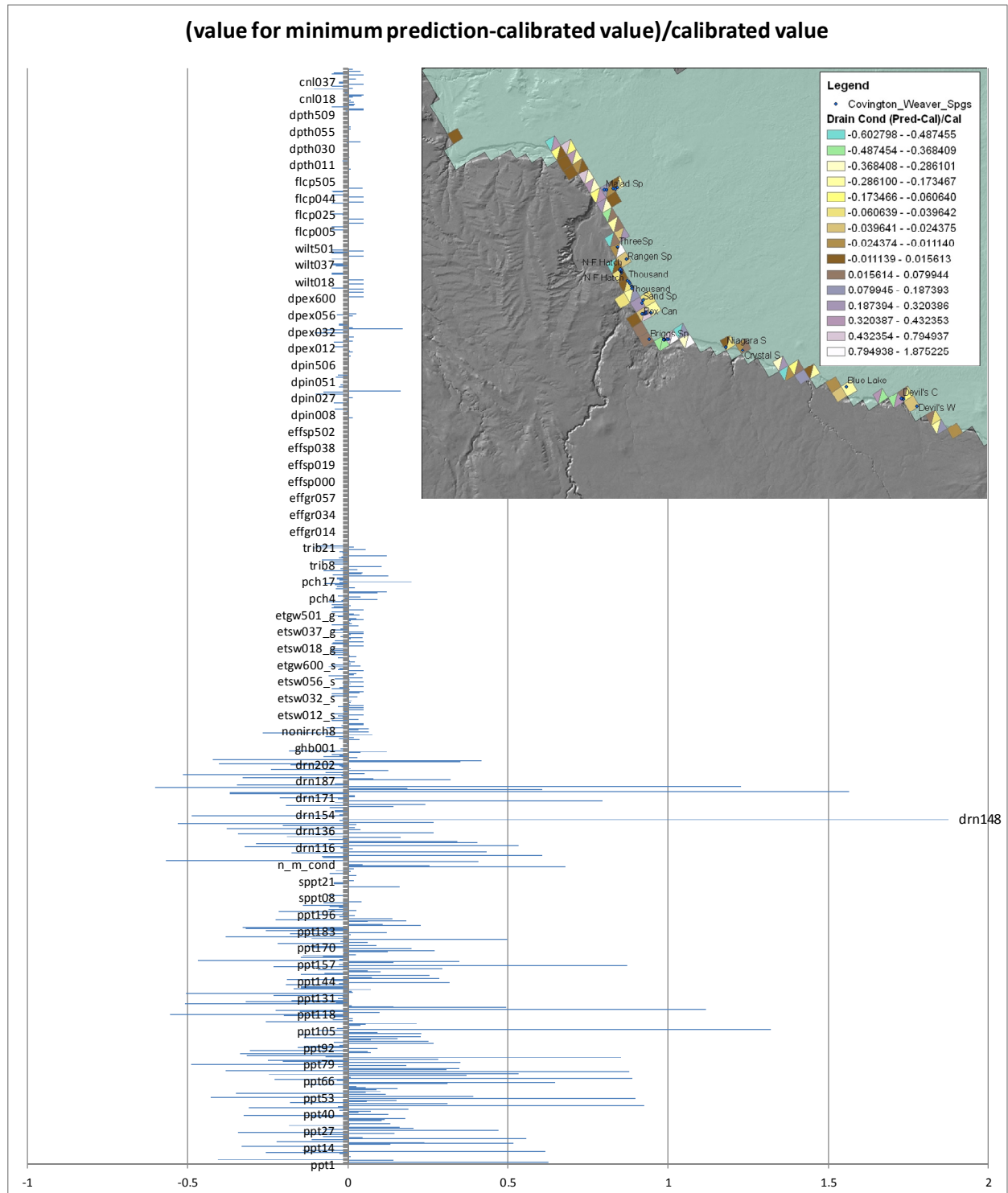


Impact of Water District 130 on Ashton-Rexburg using calibration run E120116A008.

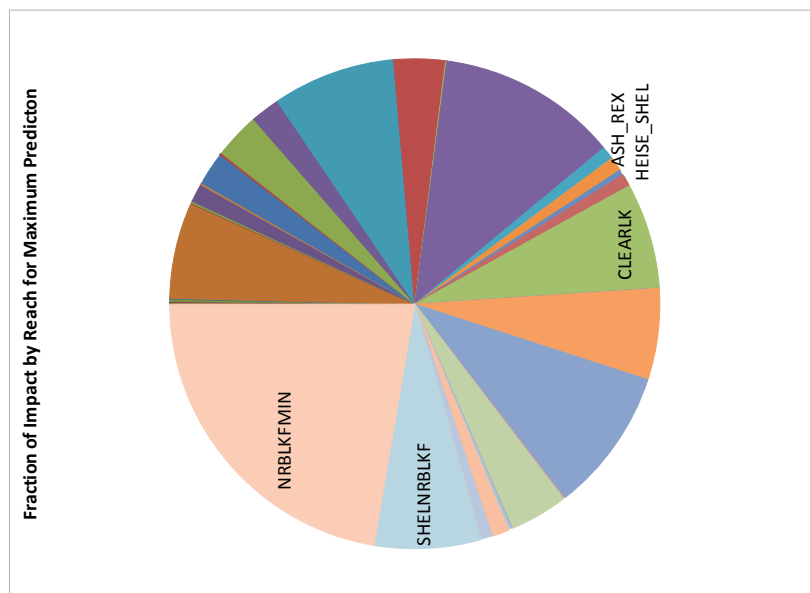
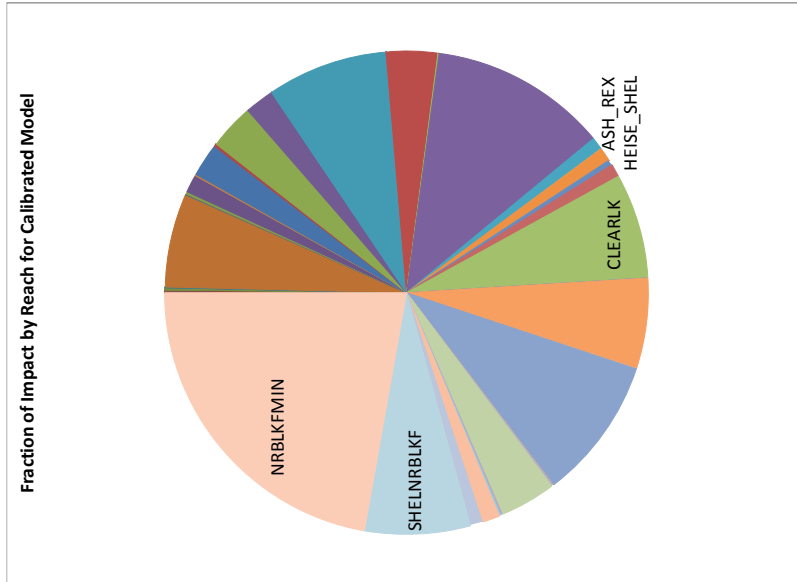




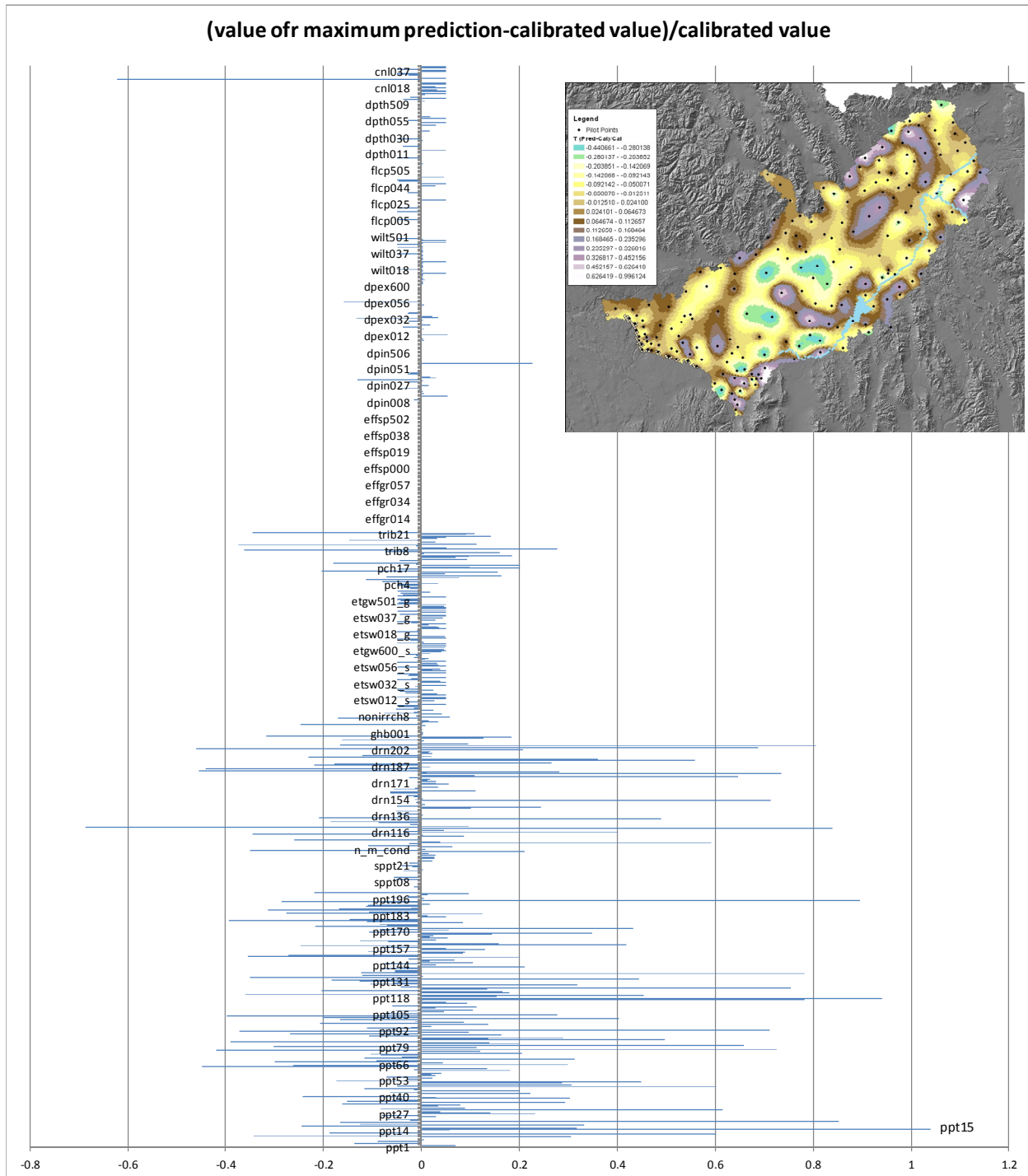
Impact of Water District 130 on Ashton-Rexburg using calibration run E120116A008.



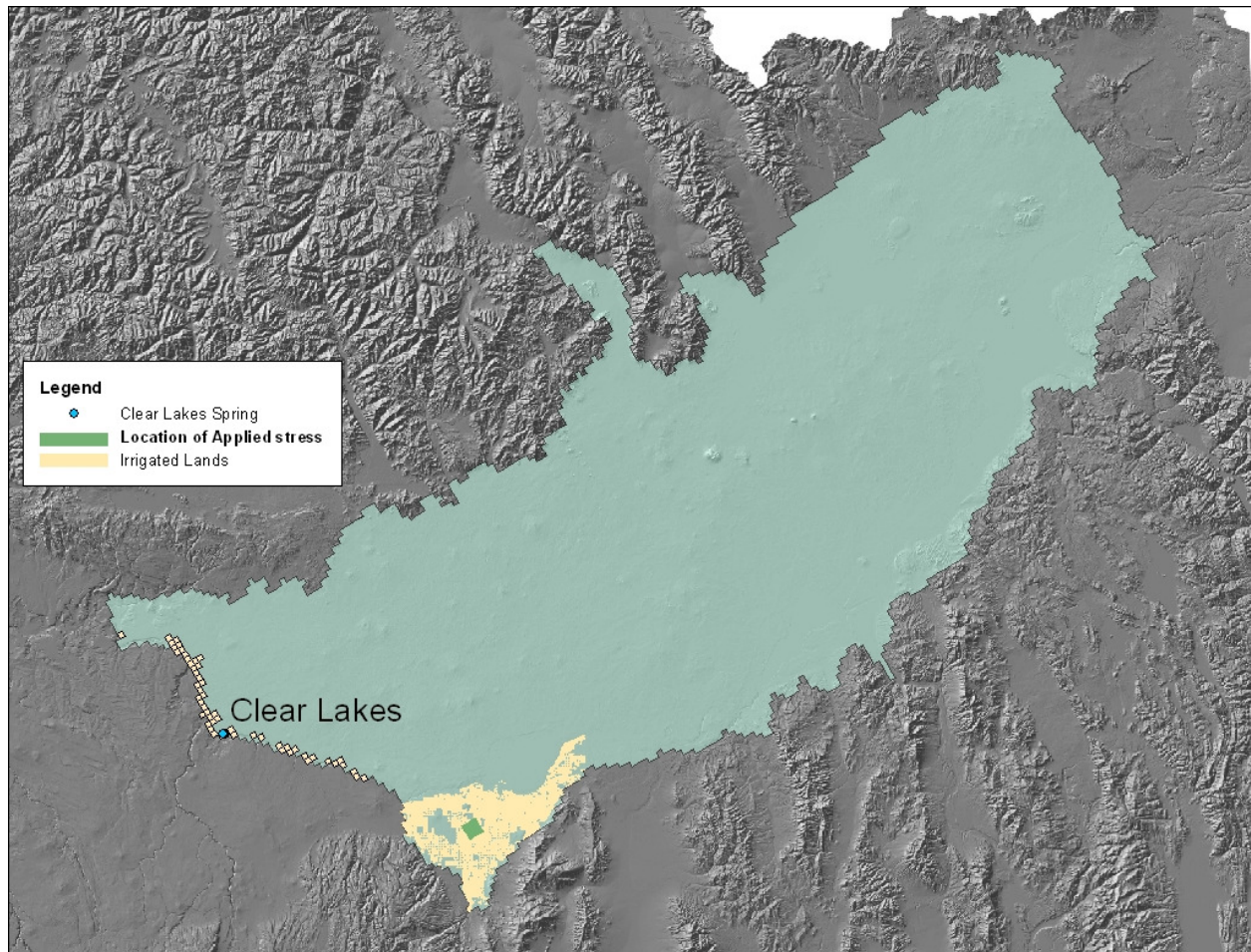
Impact of Water District 130 on Ashton-Rexburg using calibration run E120116A008.



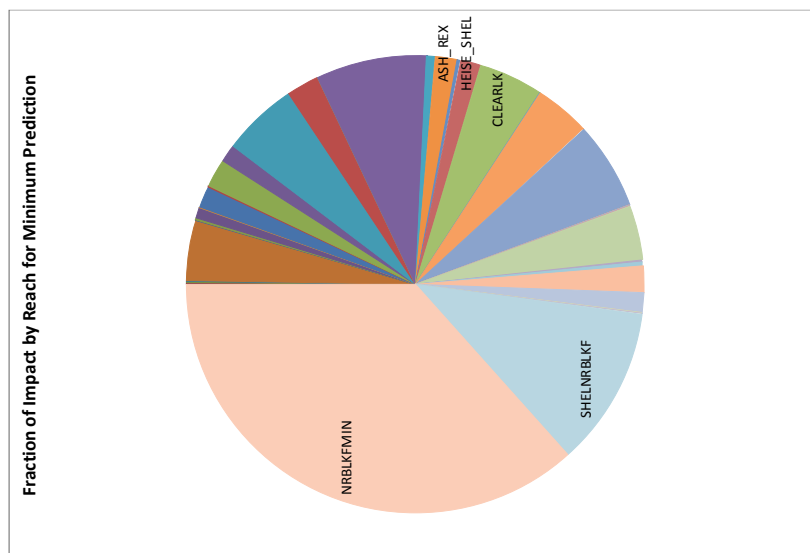
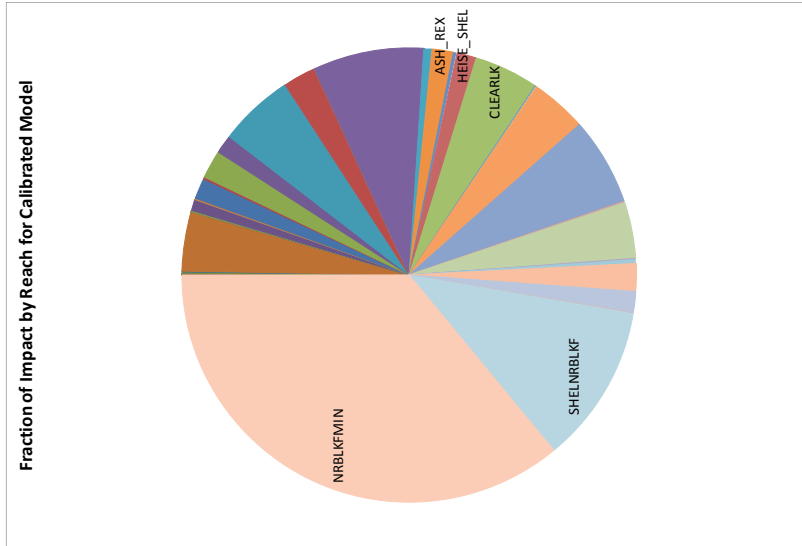
Impact of Water District 130 on Ashton-Rexburg using calibration run E120116A008.



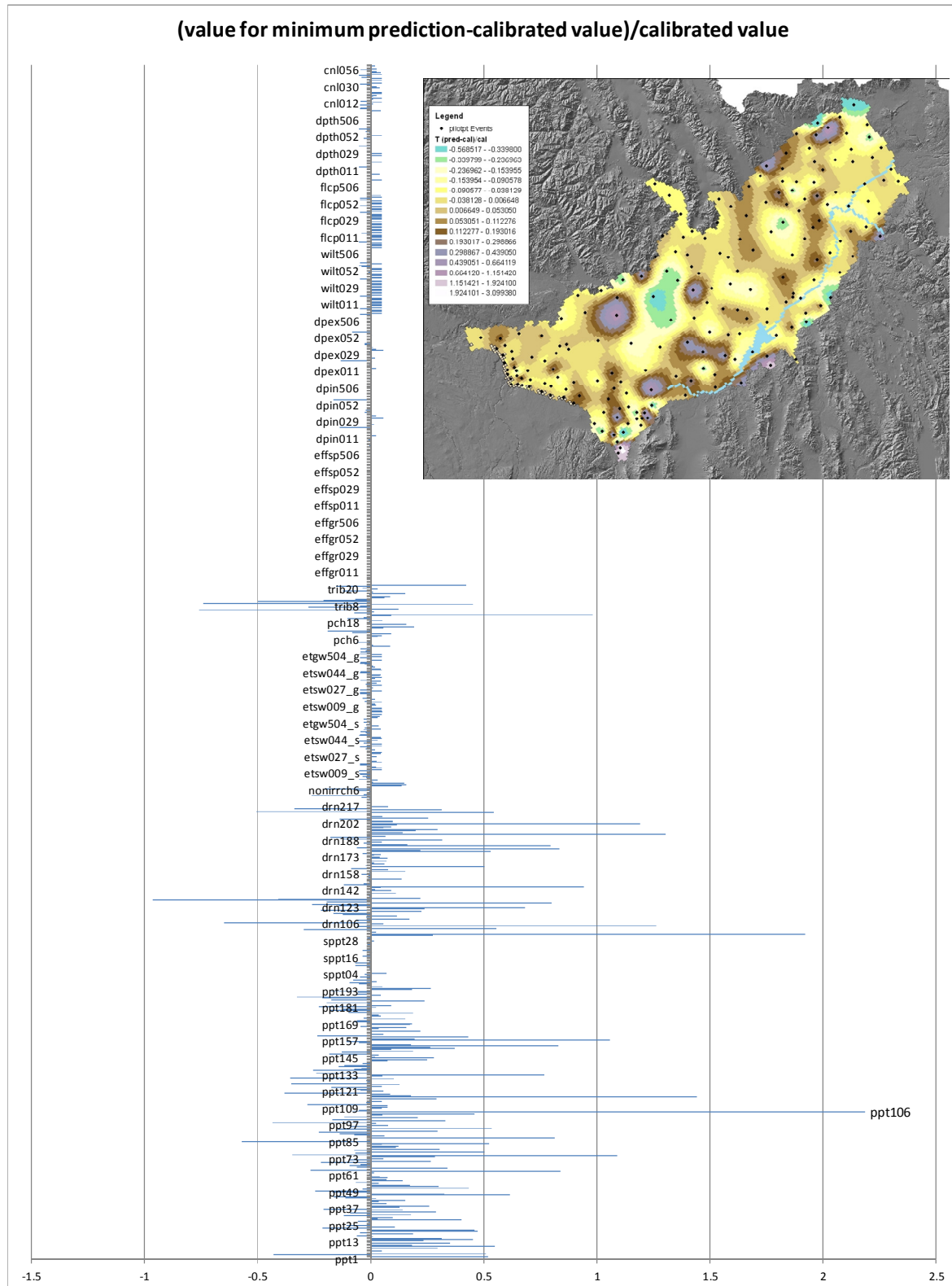
Impact of Water District 140 on Clear Lakes Spring using calibration run E120116A008.



Impact of Water District 140 on Clear Lakes Spring using calibration run E120116A008.

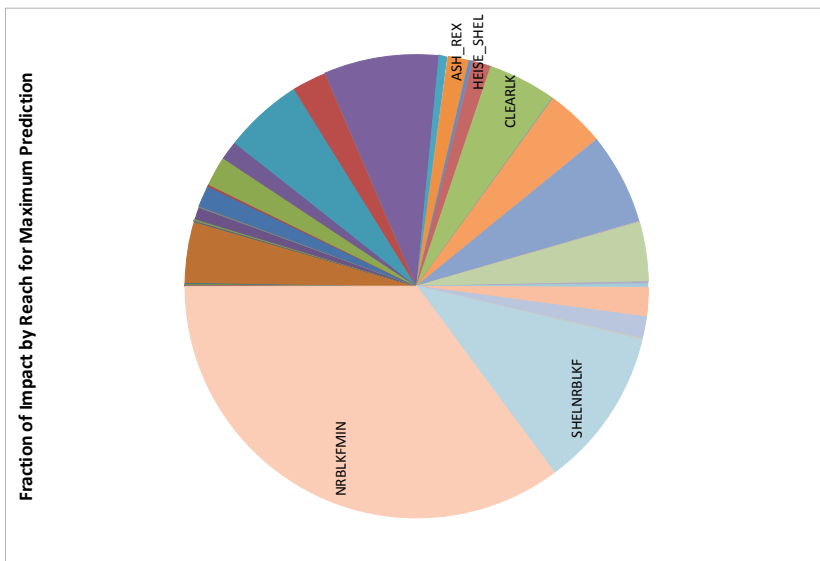
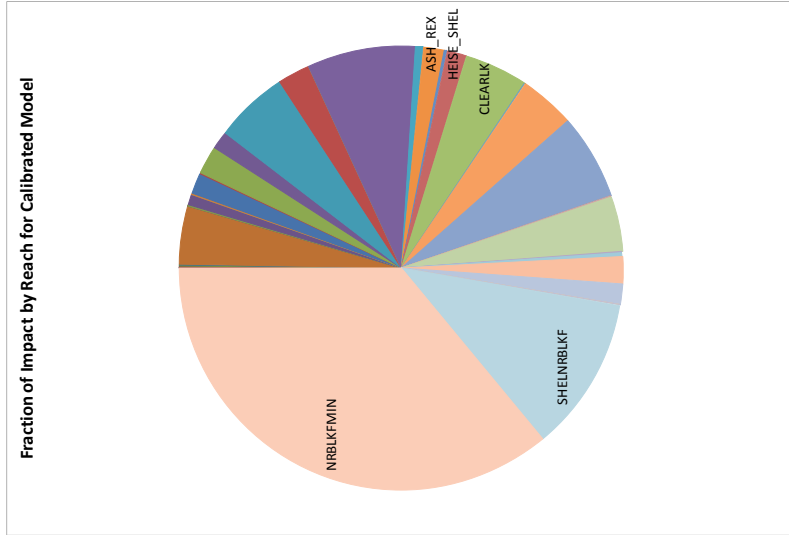


Impact of Water District 140 on Clear Lakes Spring using calibration run E120116A008.

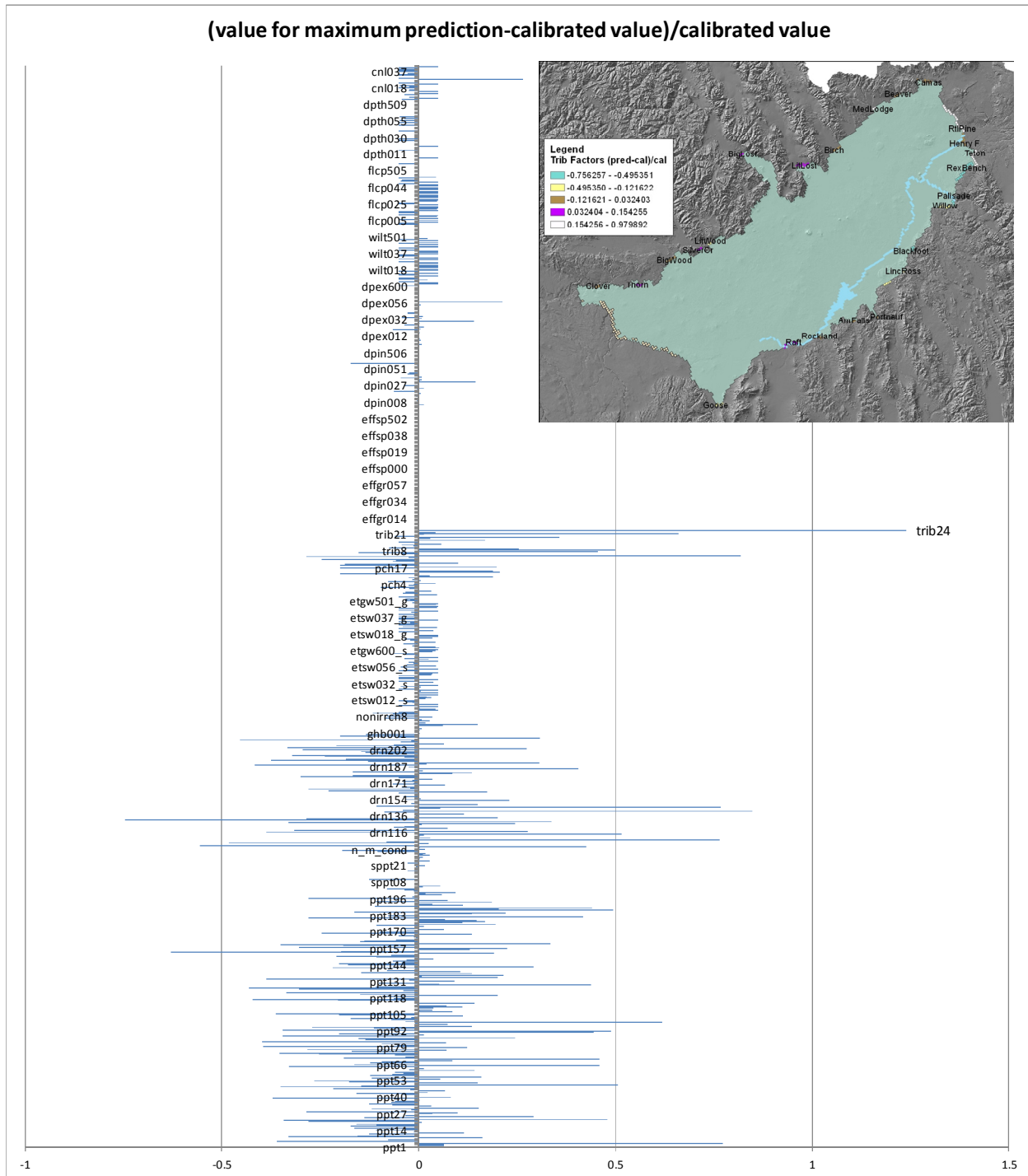




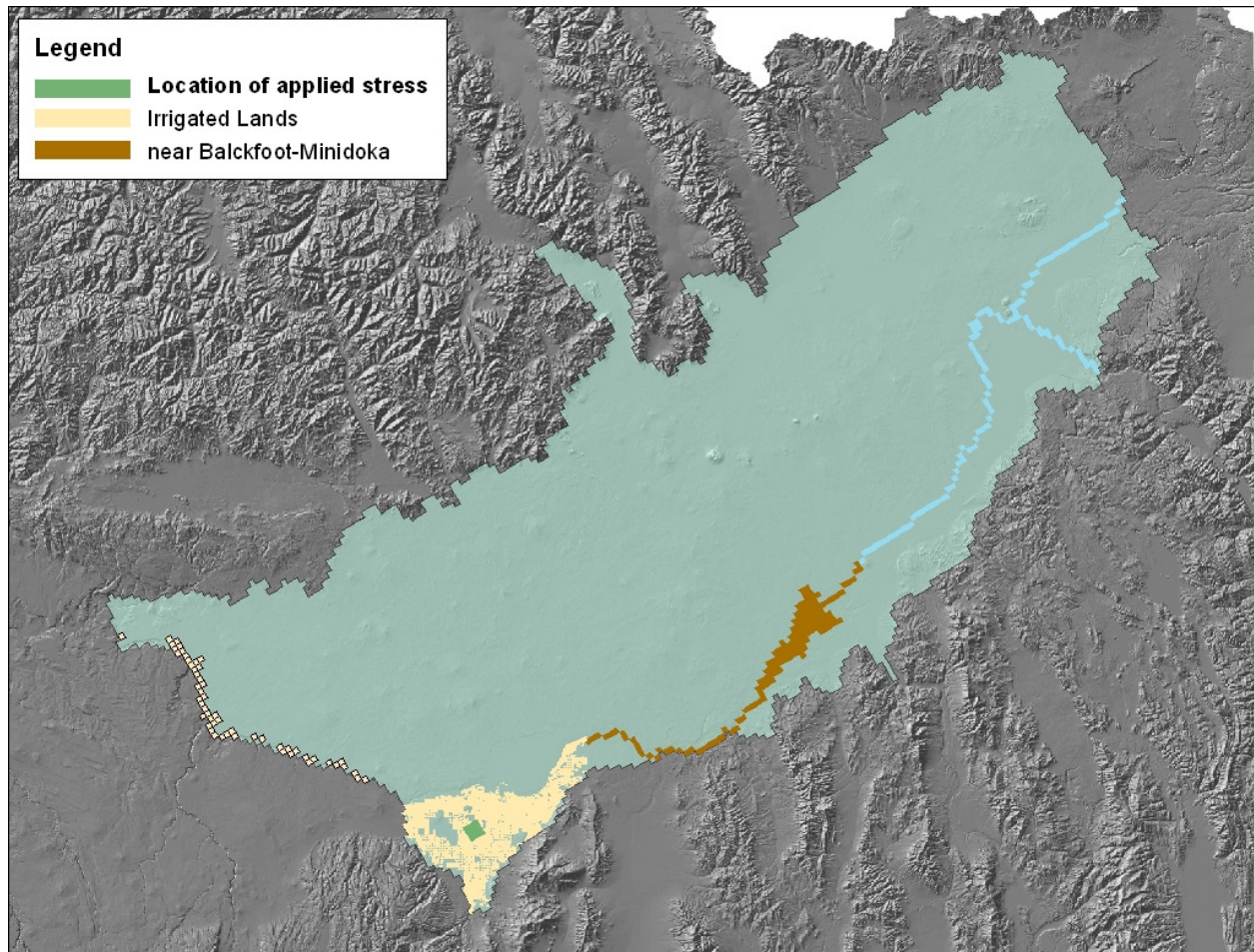
Impact of Water District 140 on Clear Lakes Spring using calibration run E120116A008.



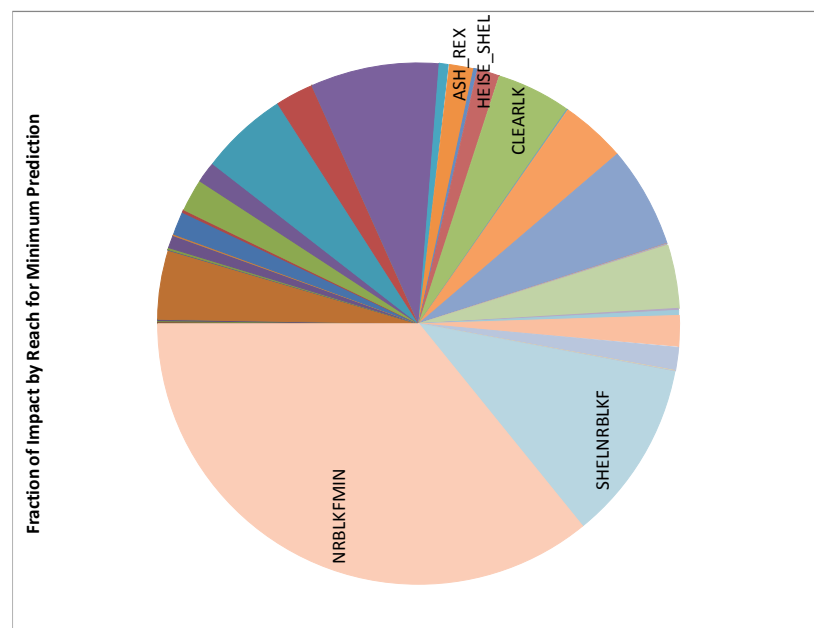
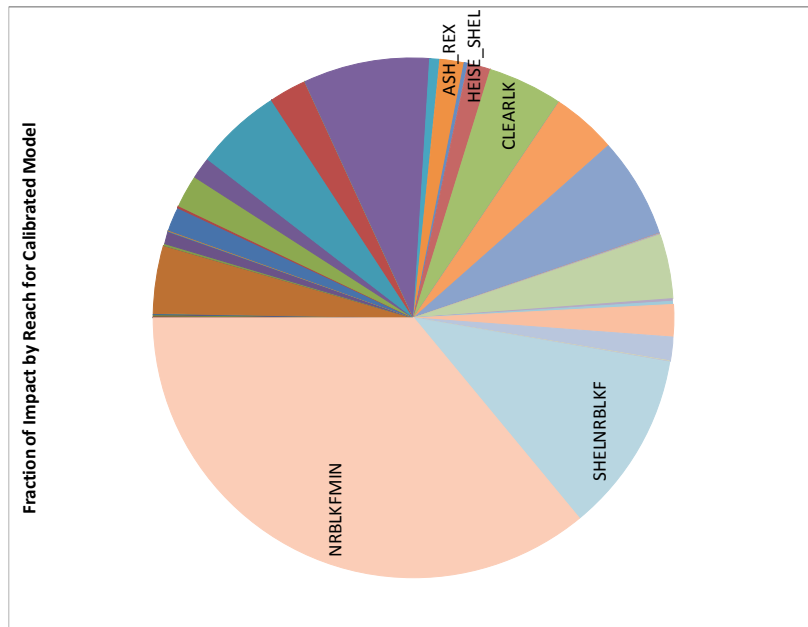
Impact of Water District 140 on Clear Lakes Spring using calibration run E120116A008.



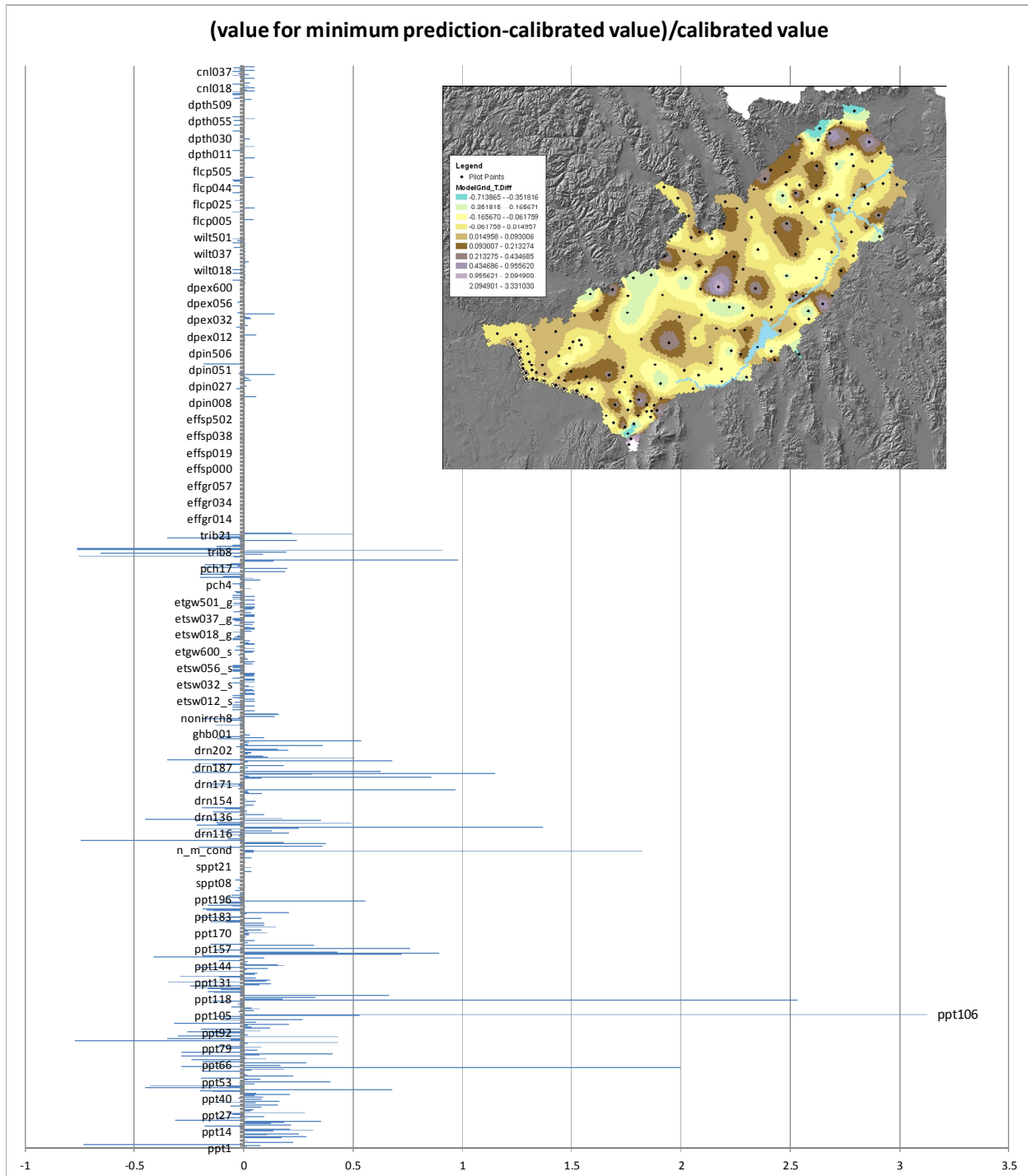
Impact of Water District 140 on near Blackfoot-Minidoka using calibration run E120116A008.



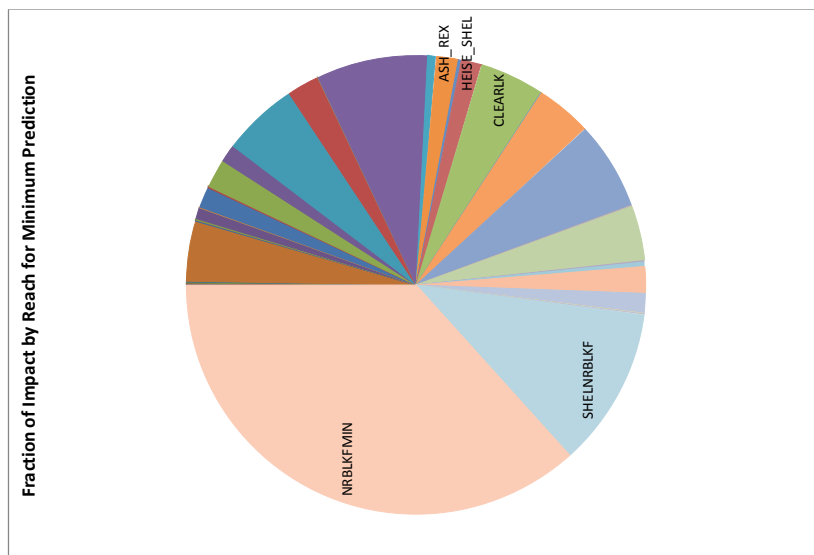
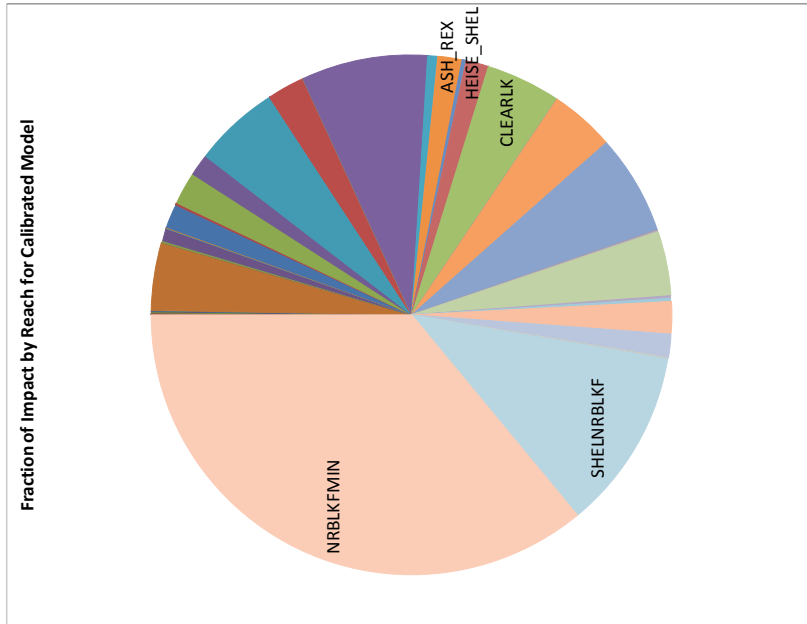
Impact of Water District 140 on near Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 140 on near Blackfoot-Minidoka using calibration run E120116A008.

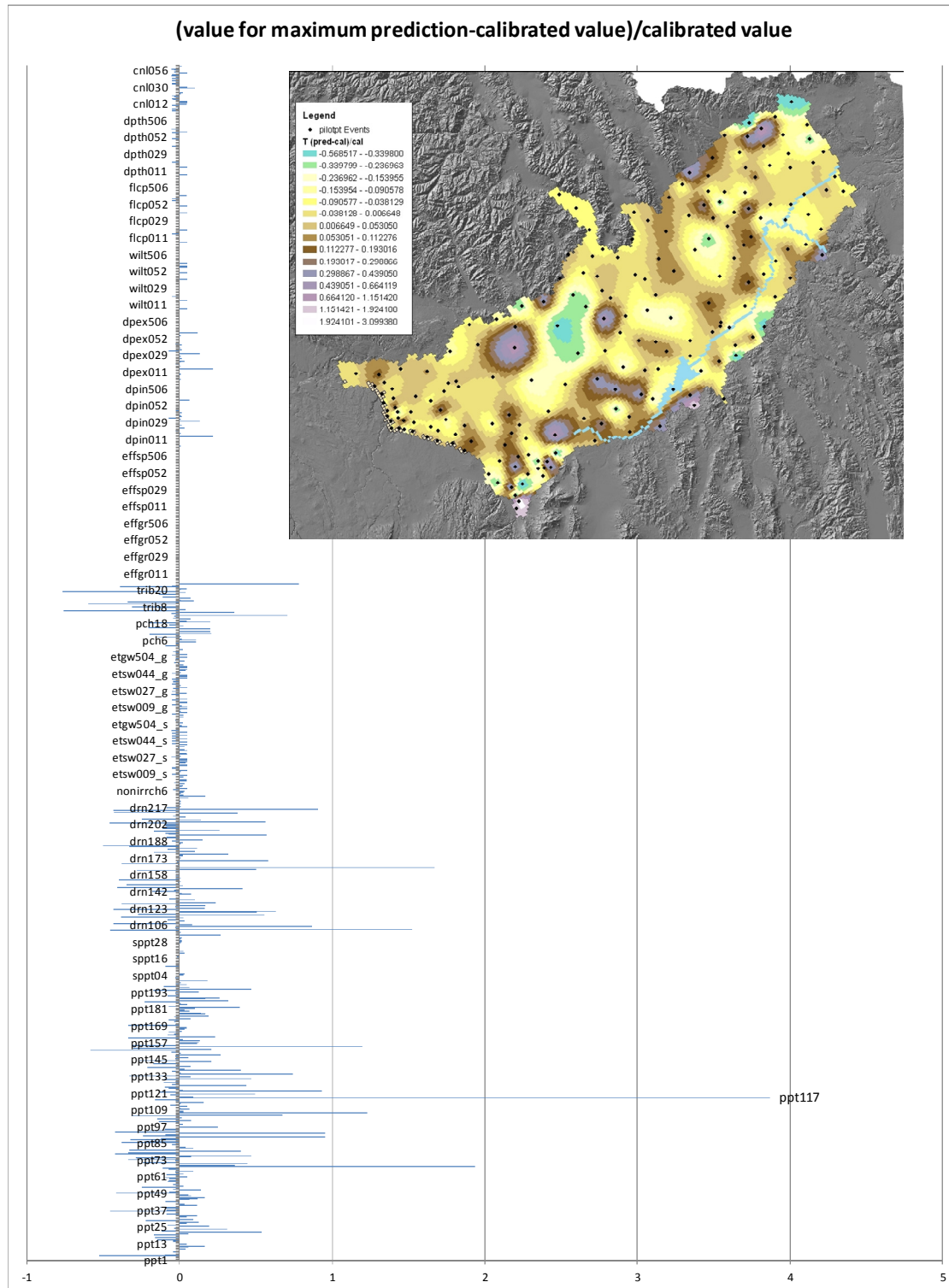


Impact of Water District 140 on near Blackfoot-Minidoka using calibration run E120116A008.



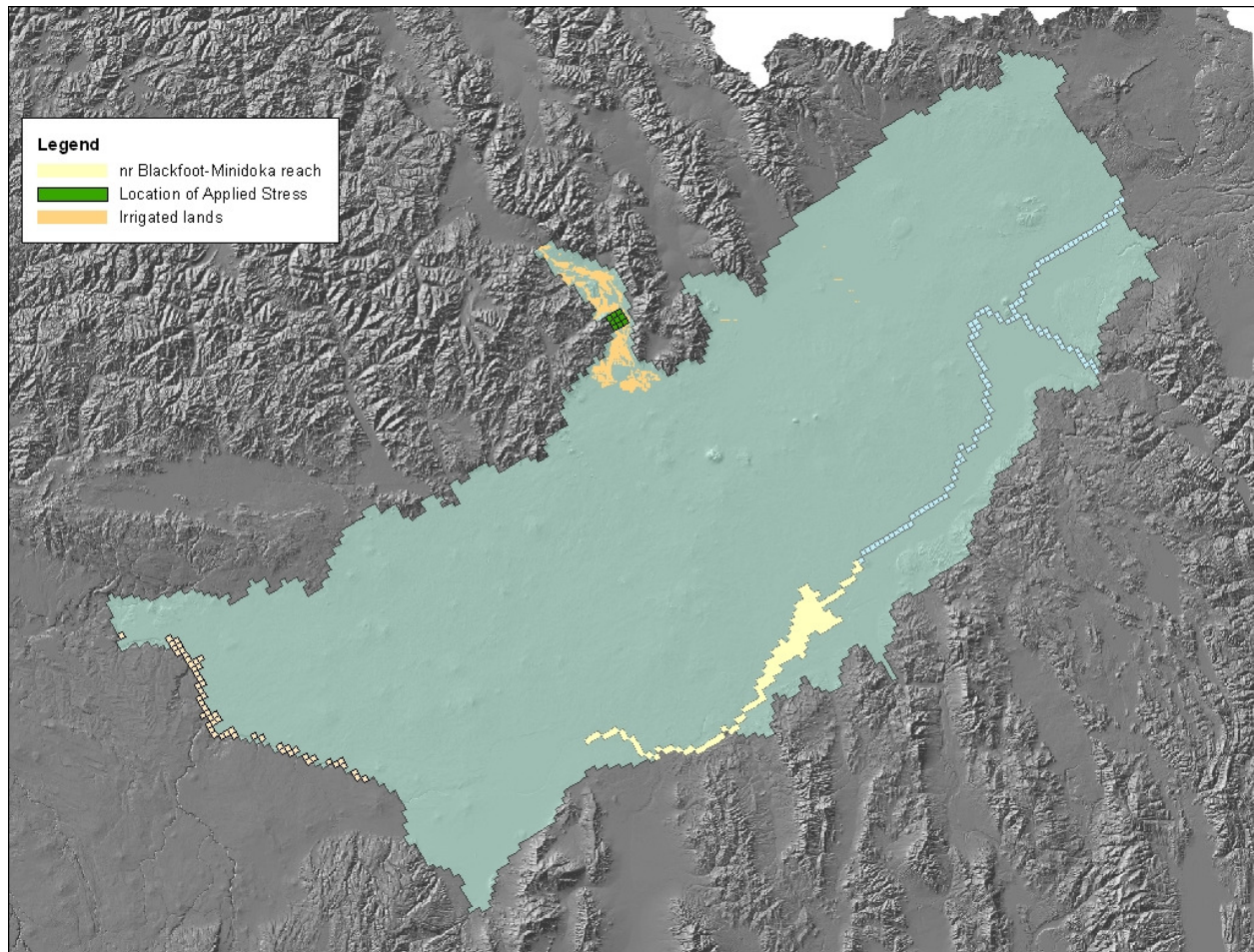


Impact of Water District 140 on near Blackfoot-Minidoka using calibration run E120116A008.

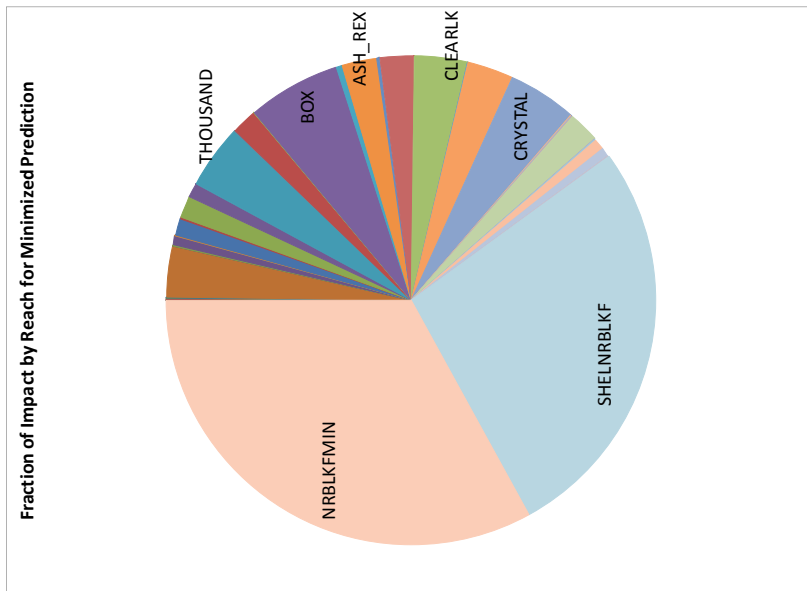
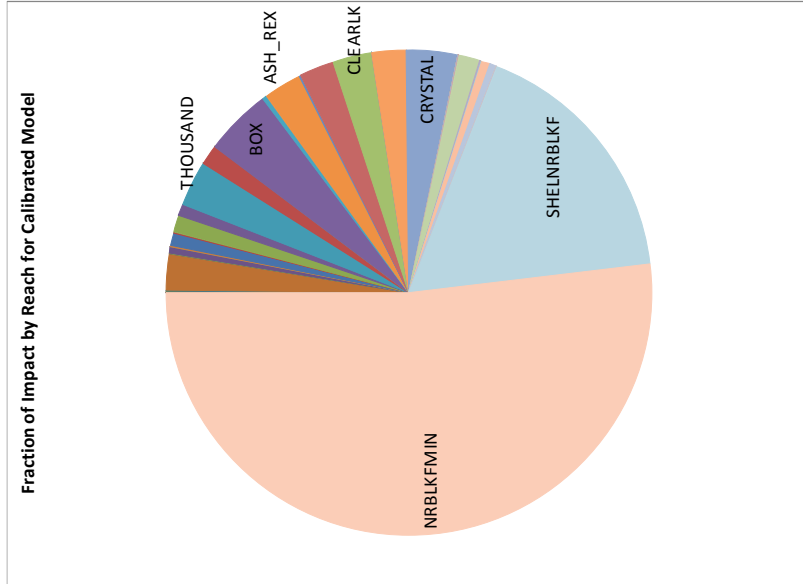


## **Appendix B; Filtered/Unfiltered Test Charts**

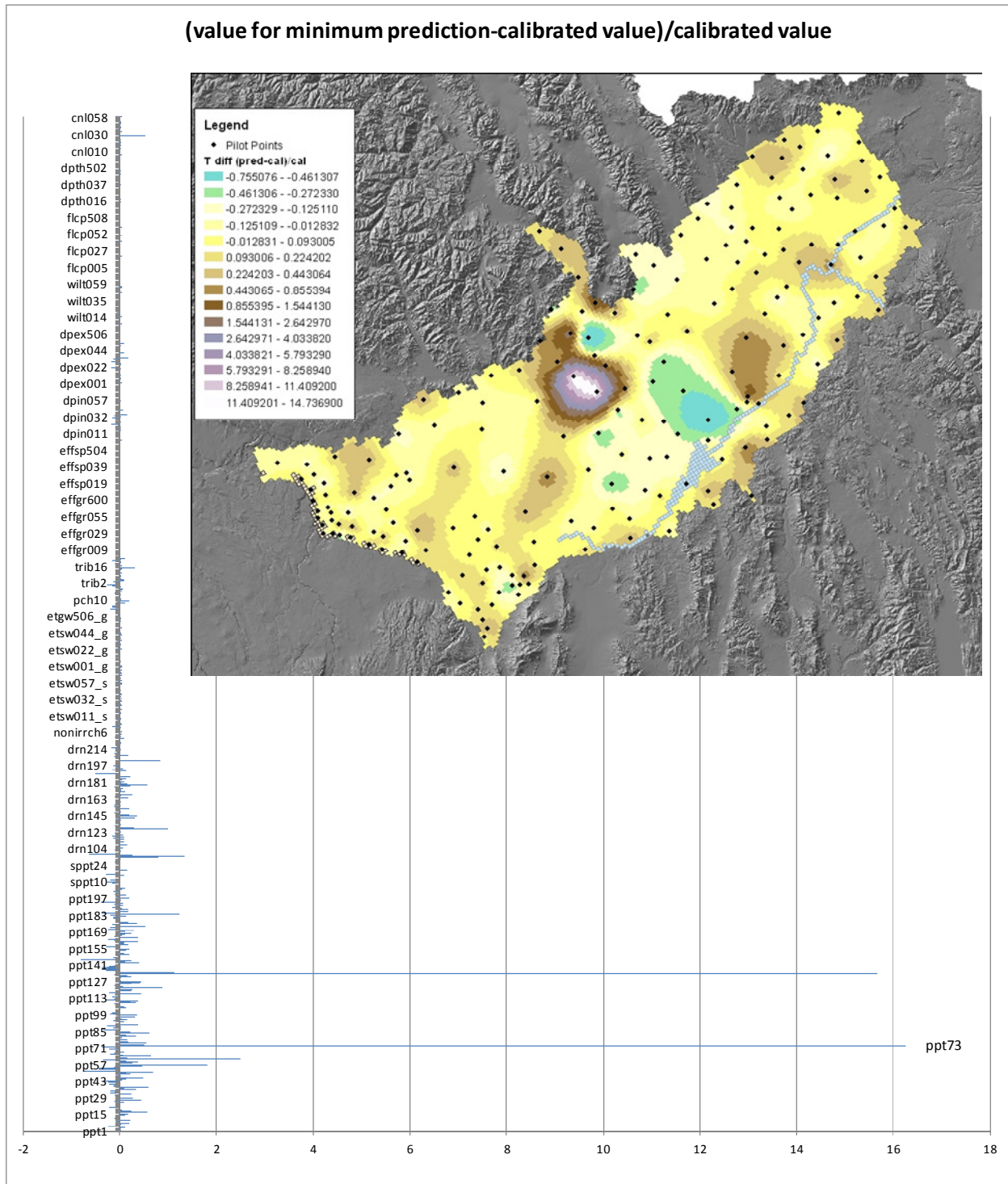
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.

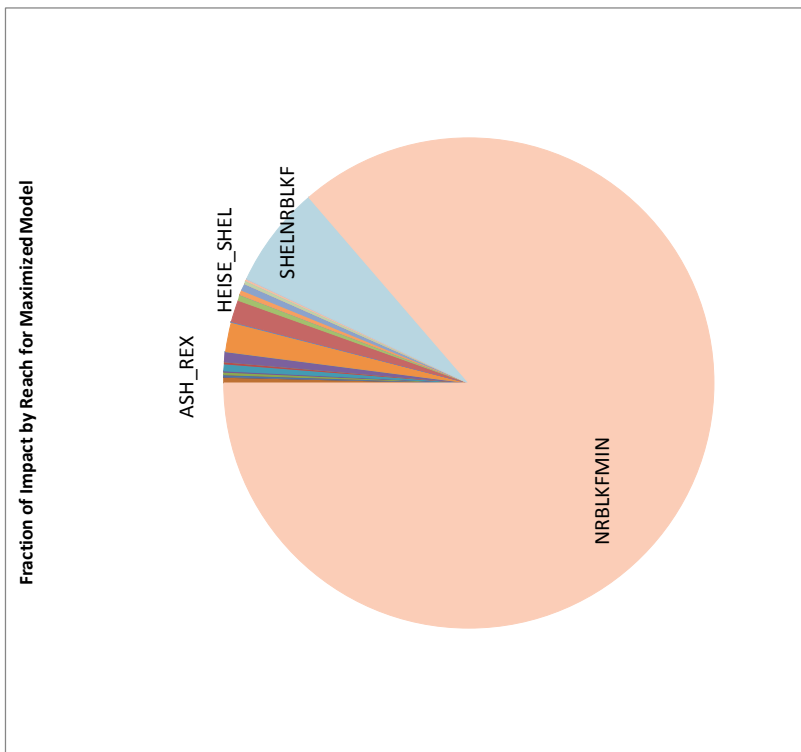
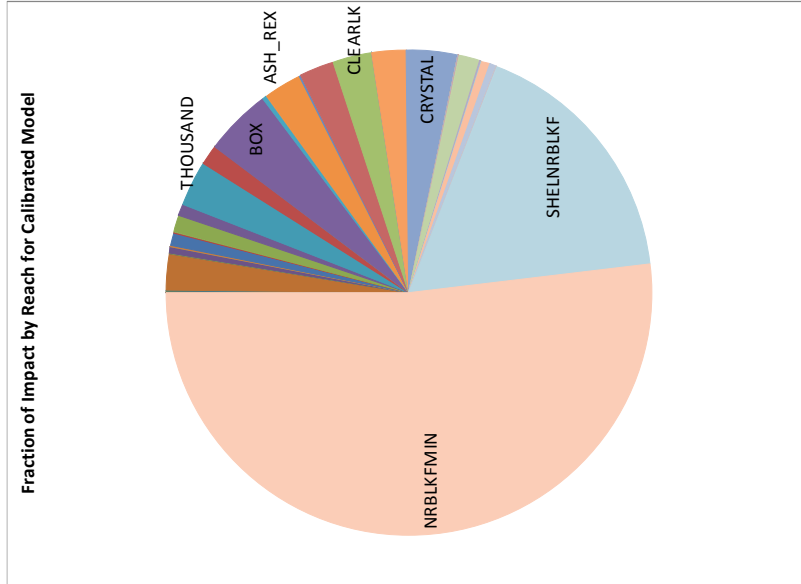


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



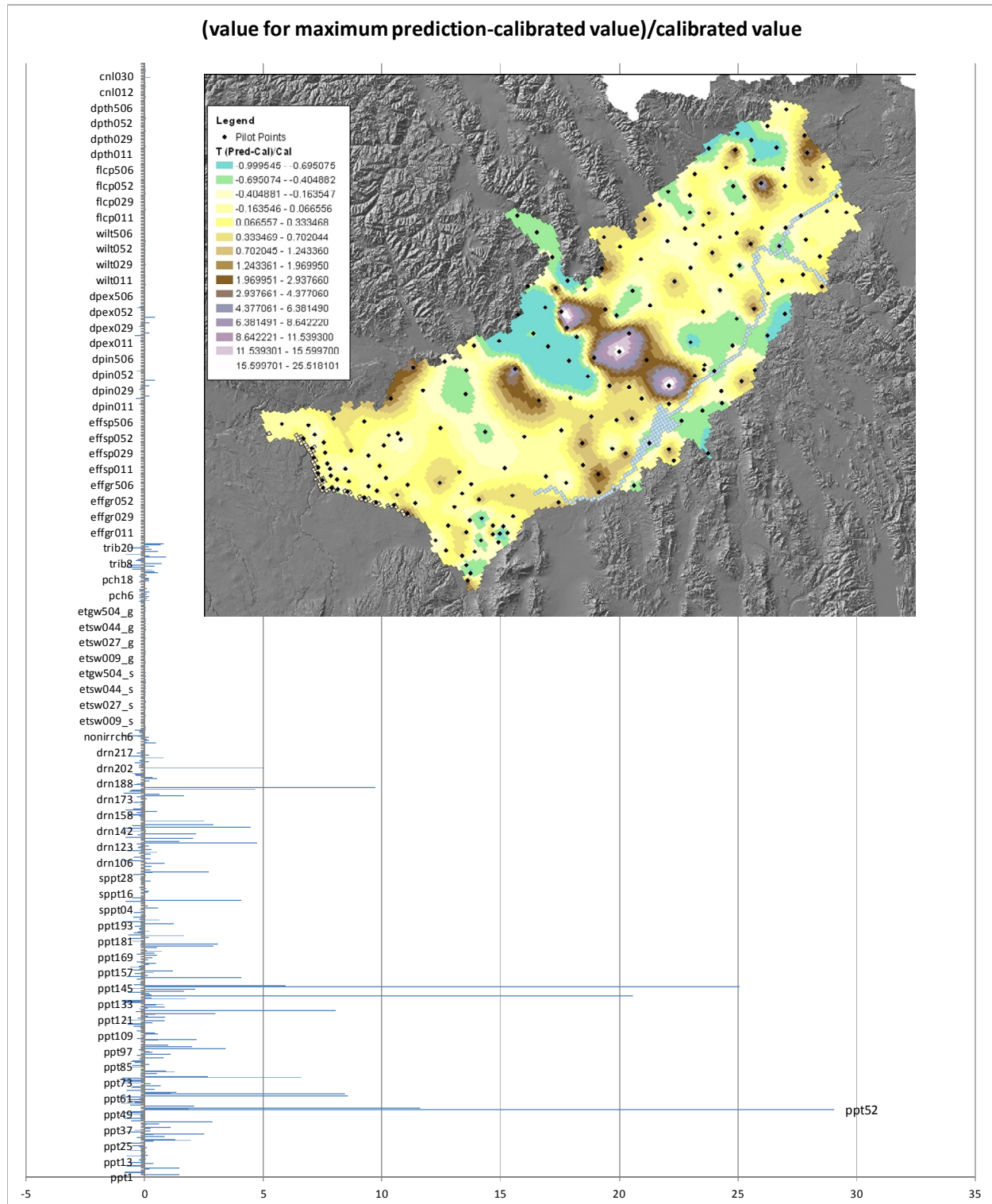


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.

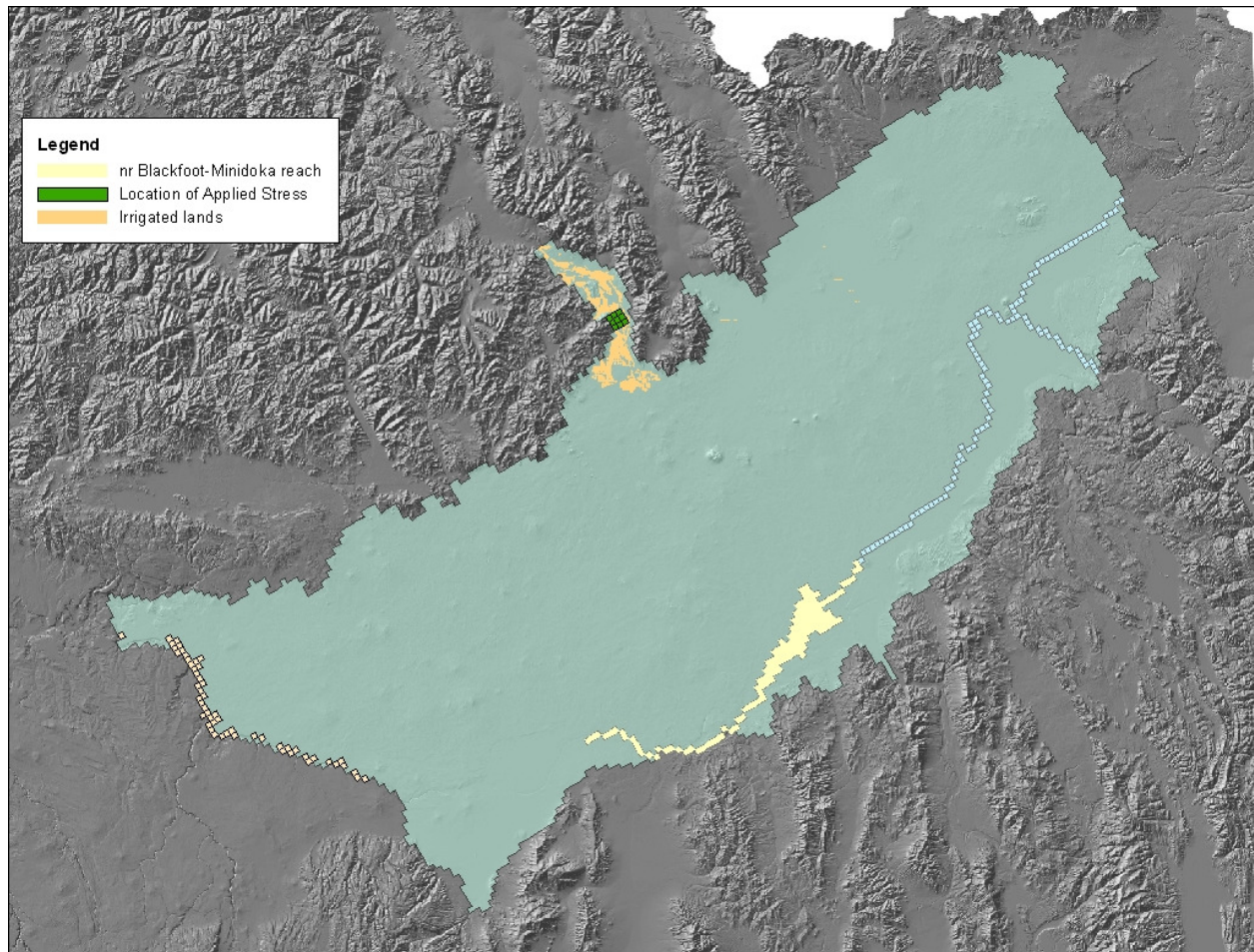




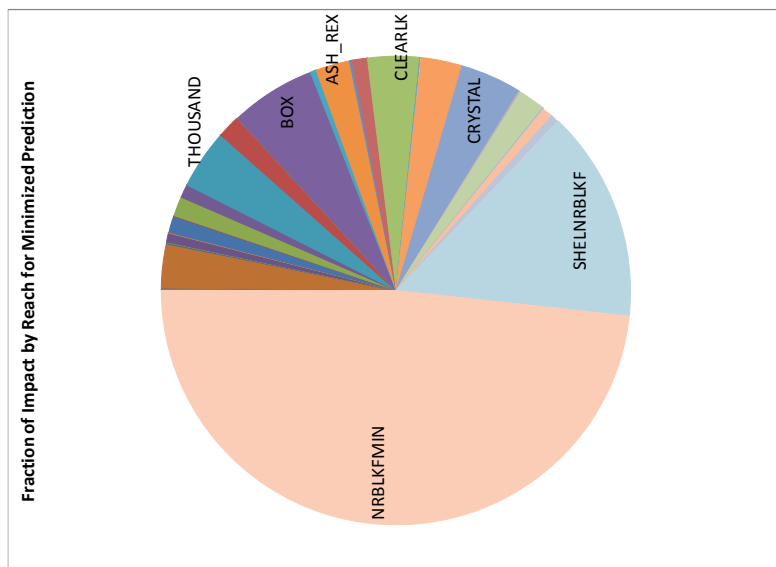
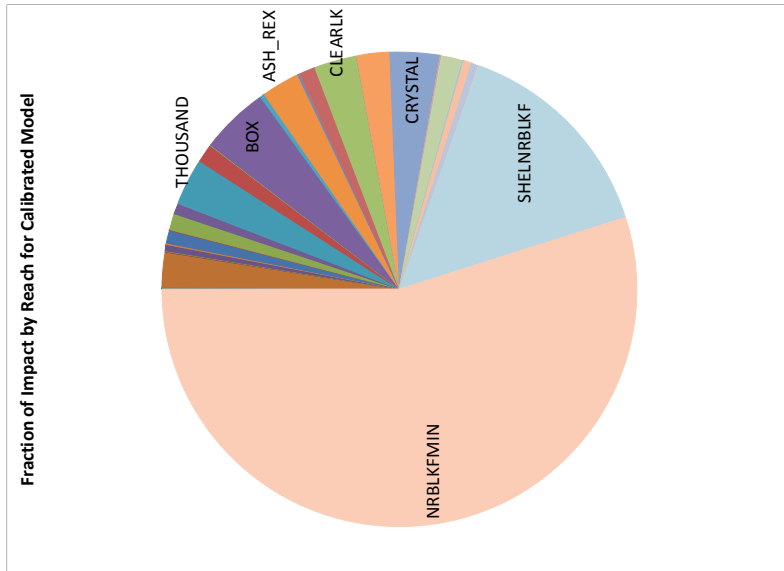
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116A008.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116Afilt.

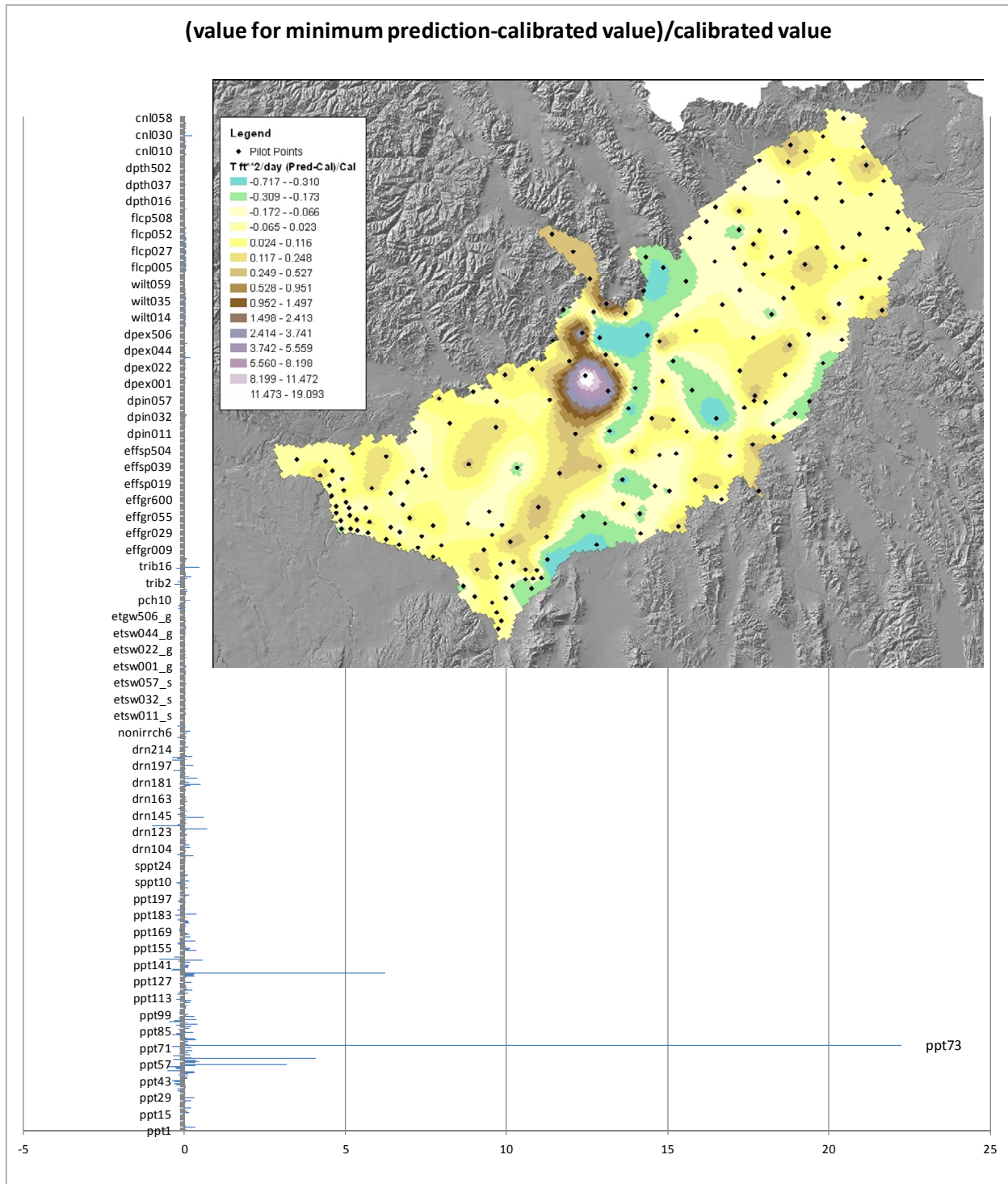


Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116Afilt.

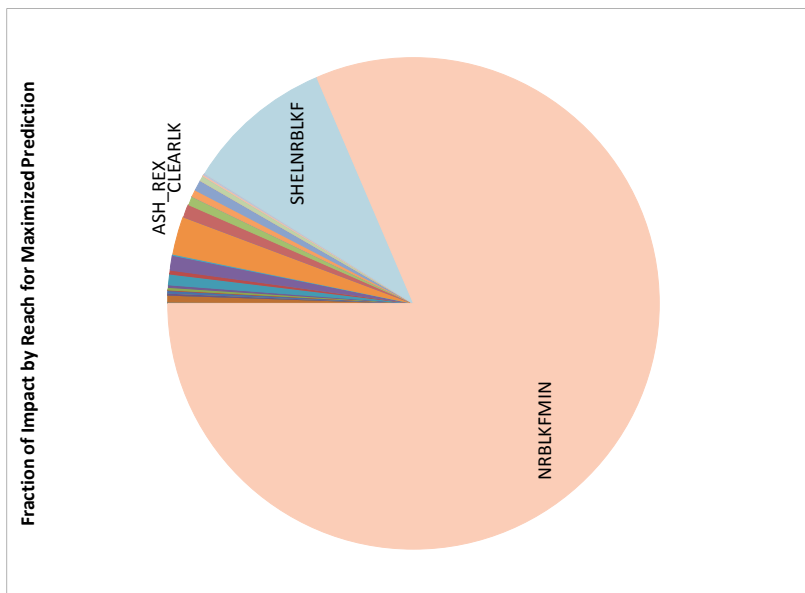
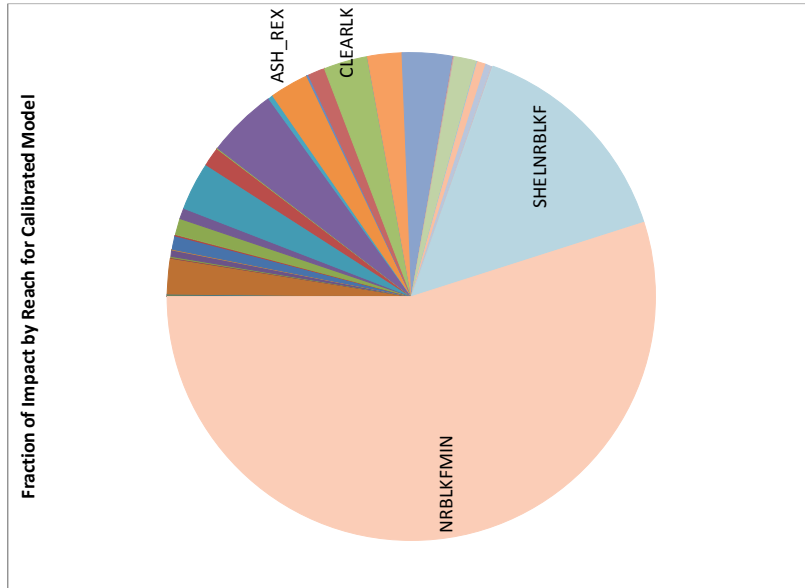




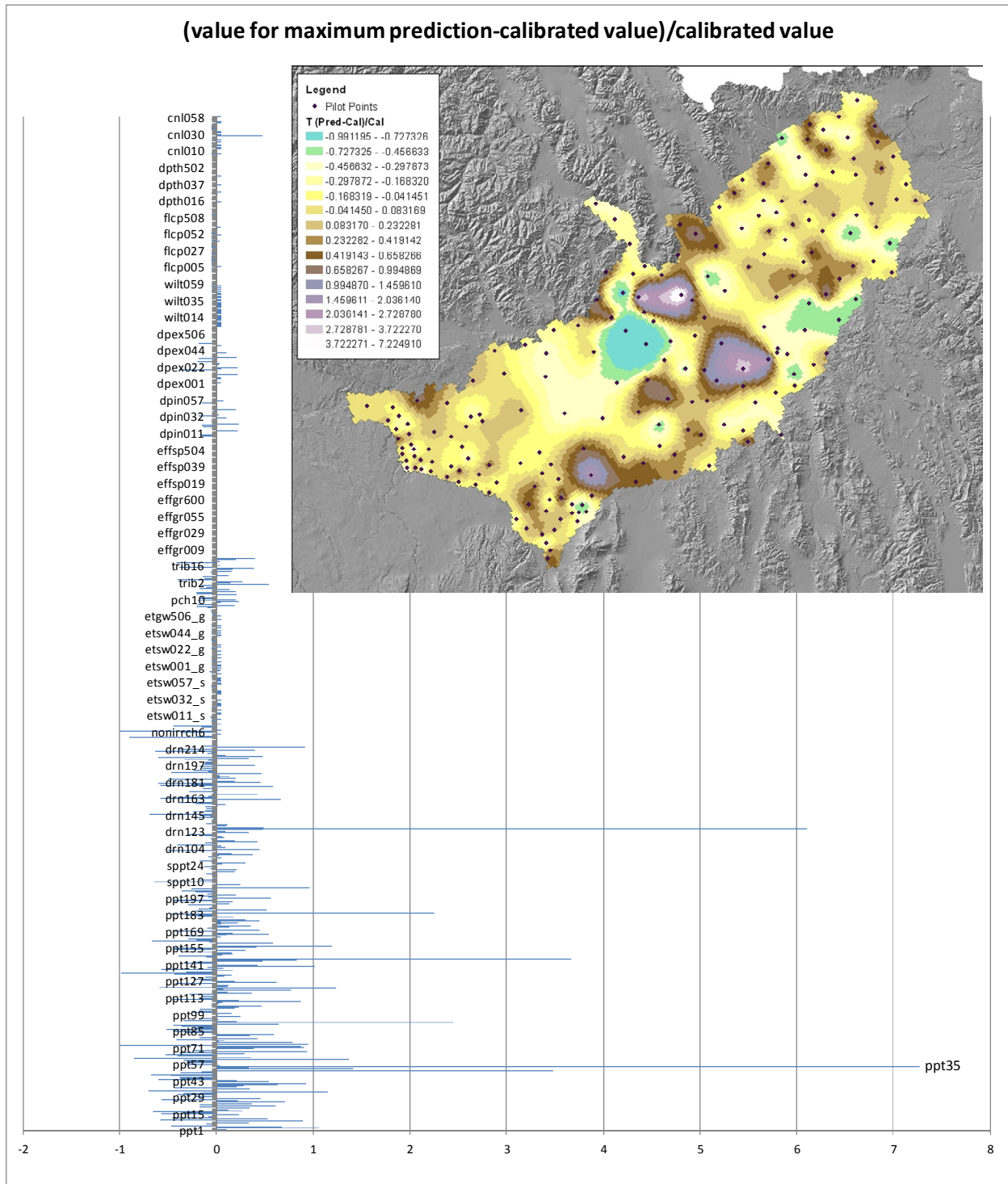
Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116Afilt.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116Afilt.



Impact of Water District 34 on nr Blackfoot-Minidoka using calibration run E120116Afilt.





## **Appendix C; Parameter List and Descriptions**

ppt1 Pilot point 1  
ppt2 Pilot point 2  
ppt3 Pilot point 3  
ppt4 Pilot point 4  
ppt5 Pilot point 5  
ppt6 Pilot point 6  
ppt7 Pilot point 7  
ppt8 Pilot point 8  
ppt9 Pilot point 9  
ppt10 Pilot point 10  
ppt11 Pilot point 11  
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ppt201 Pilot point 201  
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sppt03 Specific yield point 3  
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 sppt27 Specific yield point 27  
 sppt28 Specific yield point 28  
 a\_r\_cond Riverbed conductance for Ashton-Rexburg reach  
 h\_s\_cond Riverbed conductance for Heise-Shelley reach  
 s\_b\_cond Riverbed conductance for Shelley-near Blackfoot reach  
 b\_n\_cond Riverbed conductance for near Blackfoot-Neeley reach  
 amf\_cond Riverbed conductance for bottom of American Falls Reservoir  
 n\_m\_cond Riverbed conductance for Neeley-Minidoka reach  
 drn101 Conductance for drain 101  
 drn102 Conductance for drain 102  
 drn103 Conductance for drain 103  
 drn104 Conductance for drain 104  
 drn105 Conductance for drain 105  
 drn106 Conductance for drain 106  
 drn108 Conductance for drain 108  
 drn109 Conductance for drain 109  
 drn110 Conductance for drain 110  
 drn112 Conductance for drain 112  
 drn113 Conductance for drain 113  
 drn114 Conductance for drain 114  
 drn116 Conductance for drain 116  
 drn117 Conductance for drain 117  
 drn119 Conductance for drain 119  
 drn120 Conductance for drain 120  
 drn122 Conductance for drain 122

drn123 Conductance for drain 123  
drn125 Conductance for drain 125  
drn126 Conductance for one of the drains in the Malad complex  
drn128 Conductance for one of the drains in the Malad complex  
drn129 Conductance for one of the drains in the Malad complex  
drn130 Conductance for one of the drains in the Malad complex  
drn133 Conductance for drain 133  
drn135 Conductance for drain 135  
drn136 Conductance for drain 136  
drn137 Conductance for drain 137  
drn139 Conductance for drain 139  
drn140 Conductance for drain 140  
drn142 Conductance for drain 142  
drn143 Conductance for drain 143  
drn145 Conductance for drain 145  
drn146 Conductance for drain 146  
drn147 Conductance for drain 147  
drn148 Conductance for one of the drains in the Three Springs complex  
drn150 Conductance for one of the drains in the Three Springs complex.  
drn151 Conductance for drain 151  
drn153 Conductance for drain 153  
drn154 Conductance for the drain representing Rangen  
drn155 Conductance for one of the drains representing National Fish Hatchery/Magic  
drn157 Conductance for one of the drains representing National Fish Hatchery/Magic  
drn158 Conductance for one of the drains representing Thousand Springs/Magic  
drn160 Conductance for one of the drains representing Thousand Springs/Magic  
drn161 Conductance for drain 161  
drn162 Conductance for drain 162  
drn163 Conductance for drain 163  
drn164 Conductance for one of the drains representing Sand Springs  
drn165 Conductance for one of the drains representing Sand Springs  
drn166 Conductance for drain 166  
drn167 Conductance for drain 167  
drn170 Conductance for drain 170  
drn171 Conductance for drain 171  
drn172 Conductance for drain 172  
drn173 Conductance for the drain representing Briggs  
drn174 Conductance for one of the drains representing Clear Lakes  
drn176 Conductance for one of the drains representing Clear Lakes  
drn177 Conductance for one of the drains representing Clear Lakes  
drn179 Conductance for one of the drains representing Clear Lakes  
drn180 Conductance for drain 180

drn181 Conductance for drain 181  
 drn182 Conductance for drain 182  
 drn184 Conductance for drain 194  
 drn185 Conductance for one of the drains representing Niagara  
 drn186 Conductance for one of the drains representing Niagara  
 drn187 Conductance for drain 187  
 drn188 Conductance for drain 188  
 drn189 Conductance for drain 189  
 drn190 Conductance for drain 190  
 drn191 Conductance for drain 191  
 drn193 Conductance for drain 193  
 drn194 Conductance for drain 194  
 drn195 Conductance for drain 195  
 drn196 Conductance for drain 196  
 drn197 Conductance for drain 197  
 drn199 Conductance for drain 199  
 drn200 Conductance for drain 200  
 drn201 Conductance for drain 201  
 drn202 Conductance for the drain representing Blue Lake  
 drn203 Conductance for drain 203  
 drn205 Conductance for drain 205  
 drn206 Conductance for drain 206  
 drn208 Conductance for drain 208  
 drn209 Conductance for one of the drains representing Devils Corral  
 drn210 Conductance for one of the drains representing Devils Corral  
 drn211 Conductance for the drain representing Devils Washbowl  
 drn212 Conductance for drain 212  
 drn213 Conductance for drain 213  
 drn214 Conductance for drain 214  
 drn216 Conductance for drain 216  
 drn217 Conductance for drain 217  
 ghb001 General head boundary conductance for Lower Salmon Falls-King Hill reach  
 ghb002 General head boundary conductance for Buhl-Lower Salmon Falls reach  
 ghb003 General head boundary conductance for Thousand Springs/Magic/Ntl Fish Hatchery  
 ghb004 General head boundary conductance for Blue Heart  
 ghb005 General head boundary conductance for Kimberly-Buhl reach  
 ghb006 General head boundary conductance for Crystal Springs  
 nonirrch1 Scalar for non-irrigated recharge on thin soil in polygon 1  
 nonirrch2 Scalar for non-irrigated recharge on thin soil in polygon 2  
 nonirrch3 Scalar for non-irrigated recharge on thin soil in polygon 3  
 nonirrch4 Scalar for non-irrigated recharge on thin soil in polygon 4  
 nonirrch5 Scalar for non-irrigated recharge on thin soil in polygon 5

nonirrch6 Scalar for non-irrigated recharge on rock in polygon 6  
nonirrch7 Scalar for non-irrigated recharge on rock in polygon 7  
nonirrch8 Scalar for non-irrigated recharge on rock in polygon 8  
nonirrch9 Scalar for non-irrigated recharge on thick soil in polygon 9  
nonirrch10 Scalar for non-irrigated recharge thick soil in polygon 10  
nonirrch11 Scalar for on-irrigated recharge thick soil in polygon 11  
wetlands ET from wetlands scalar  
etsw000\_s ET scalar for sprinkler irrigated land in the null entity  
etsw001\_s ET scalar for sprinkler irrigated land in the A&B entity  
etsw002\_s ET scalar for sprinkler irrigated land in the Aberdeen-Springfield entity  
etsw005\_s ET scalar for sprinkler irrigated land in the Big Lost River entity  
etsw008\_s ET scalar for sprinkler irrigated land in the Blaine Co entity  
etsw009\_s ET scalar for sprinkler irrigated land in the Burgess entity  
etsw010\_s ET scalar for sprinkler irrigated land in the Burley entity  
etsw011\_s ET scalar for sprinkler irrigated land in the Butte/Market Lake entity  
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etsw025\_s ET scalar for sprinkler irrigated land in the Little Wood entity  
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etsw053\_s ET scalar for sprinkler irrigated land in the Howe entity  
etsw055\_s ET scalar for sprinkler irrigated land in the Labelle entity  
etsw056\_s ET scalar for sprinkler irrigated land in the Sugar City entity

etsw057\_s ET scalar for sprinkler irrigated land in the Blackfoot-Chubbuck entity  
etsw058\_s ET scalar for sprinkler irrigated land in the American Falls 2 entity  
etsw059\_s ET scalar for sprinkler irrigated land in the Gooding-Richfield entity  
etgw501\_s ET scalar for sprinkler irrigated land in Ground Water entity 501  
etgw502\_s ET scalar for sprinkler irrigated land in Ground Water entity 502  
etgw503\_s ET scalar for sprinkler irrigated land in Ground Water entity 503  
etgw504\_s ET scalar for sprinkler irrigated land in Ground Water entity 504  
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etgw507\_s ET scalar for sprinkler irrigated land in Ground Water entity 507  
etgw508\_s ET scalar for sprinkler irrigated land in Ground Water entity 508  
etgw509\_s ET scalar for sprinkler irrigated land in Ground Water entity 509  
etgw600\_s ET scalar for sprinkler irrigated land in Ground Water entity 600  
etsw000\_g ET scalar for gravity irrigated land in the null entity  
etsw001\_g ET scalar for gravity irrigated land in the A&B entity  
etsw002\_g ET scalar for gravity irrigated land in the Aberdeen-Springfield entity  
etsw005\_g ET scalar for gravity irrigated land in the Big Lost River entity  
etsw008\_g ET scalar for gravity irrigated land in the Blaine Co entity  
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etsw011\_g ET scalar for gravity irrigated land in the Butte/Market Lake entity  
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etsw022\_g ET scalar for gravity irrigated land in the Idaho entity  
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etsw027\_g ET scalar for gravity irrigated land in the Milner entity  
etsw028\_g ET scalar for gravity irrigated land in the Minidoka entity  
etsw029\_g ET scalar for gravity irrigated land in the Mud Lake entity  
etsw030\_g ET scalar for gravity irrigated land in the New Sweden entity  
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etsw038\_g ET scalar for gravity irrigated land in the Rexburg entity  
etsw039\_g ET scalar for gravity irrigated land in the Chester entity  
etsw040\_g ET scalar for gravity irrigated land in the Oakley entity



etsw044\_g ET scalar for gravity irrigated land in the Montevue entity  
 etsw051\_g ET scalar for gravity irrigated land in the Dubois entity  
 etsw052\_g ET scalar for gravity irrigated land in the Small entity  
 etsw053\_g ET scalar for gravity irrigated land in the Howe entity  
 etsw055\_g ET scalar for gravity irrigated land in the Labelle entity  
 etsw056\_g ET scalar for gravity irrigated land in the Sugar City entity  
 etsw057\_g ET scalar for gravity irrigated land in the Blackfoot-Chubbuck entity  
 etsw058\_g ET scalar for gravity irrigated land in the American Falls 2 entity  
 etsw059\_g ET scalar for gravity irrigated land in the Gooding-Richfield entity  
 etgw501\_g ET scalar for gravity irrigated land in Ground Water entity 501  
 etgw502\_g ET scalar for gravity irrigated land in Ground Water entity 502  
 etgw503\_g ET scalar for gravity irrigated land in Ground Water entity 503  
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 etgw507\_g ET scalar for gravity irrigated land in Ground Water entity 507  
 etgw508\_g ET scalar for gravity irrigated land in Ground Water entity 508  
 etgw509\_g ET scalar for gravity irrigated land in Ground Water entity 509  
 etgw600\_g ET scalar for gravity irrigated land in Ground Water entity 600  
 pch1 Perched seepage scalar for Camas Cr  
 pch2 Perched seepage scalar for segment 2 of the Big Lost River  
 pch3 Perched seepage scalar for segment 3 of the Big Lost River  
 pch4 Perched seepage scalar for segment 4 of the Big Lost River  
 pch5 Perched seepage scalar for the Little Lost River  
 pch6 Perched seepage scalar for Medicine Lodge Cr  
 pch7 Perched seepage scalar for Malad River  
 pch8 Perched seepage scalar for Birch Cr  
 pch9 Perched seepage scalar for segment 1 of the Big Lost River  
 pch10 Perched seepage scalar for Lone Tree  
 pch11 Perched seepage scalar for Basin 31 flood control basin  
 pch13 Perched seepage scalar for Mud Lake  
 pch14 Perched seepage scalar for Camas National Wildlife Refuge  
 pch15 Perched seepage scalar for Birch Cr hydropower Plant  
 pch16 Perched seepage scalar for Big Lost flood control basins  
 pch17 Perched seepage scalar for part of Twin Falls Canal  
 pch18 Perched seepage scalar for Lake Murtaugh  
 pch19 Perched seepage scalar for segment 1 of Beaver Cr  
 pch20 Perched seepage scalar for segment 2 of Beaver Cr  
 pch21 Perched seepage scalar for segment 1 of Little Wood River  
 pch22 Perched seepage scalar for Big Wood and segment 2 of Little Wood River  
 trib1 Tributary underflow scalar for Little Lost River  
 trib2 Tributary underflow scalar for Medicine Lodge Cr

trib3 Tributary underflow scalar for Birch Cr  
 trib4 Tributary underflow scalar for Beaver Cr  
 trib5 Tributary underflow scalar for Blackfoot River  
 trib6 Tributary underflow scalar for Silver Cr  
 trib7 Tributary underflow scalar for Little Wood River  
 trib8 Tributary underflow scalar for Big Wood River  
 trib9 Tributary underflow scalar for Teton River  
 trib10 Tributary underflow scalar for Rexburg Bench  
 trib11 Tributary underflow scalar for South Fork (Palisade)  
 trib12 Tributary underflow scalar for Willow Cr  
 trib13 Tributary underflow scalar for Bannock Cr (Am Falls)  
 trib14 Tributary underflow scalar for Raft River  
 trib15 Tributary underflow scalar for Big Lost River  
 trib16 Tributary underflow scalar for Henrys Fork  
 trib17 Tributary underflow scalar for Thorn Cr  
 trib18 Tributary underflow scalar for Clover Cr  
 trib19 Tributary underflow scalar for Lincoln and Ross Cr  
 trib20 Tributary underflow scalar for Portneuf River  
 trib21 Tributary underflow scalar for Rock Cr  
 trib22 Tributary underflow scalar for Goose Cr  
 trib23 Tributary underflow scalar for Rattle Snake and Pine Cr  
 trib24 Tributary underflow scalar for Camas Cr@  
 effgr000\_g Maximum efficiency for gravity irrigated land in the null entity  
 effgr001\_g Maximum efficiency for gravity irrigated land in the A&B entity  
 effgr002\_g Maximum efficiency for gravity irrigated land in the Aberdeen-Springfield entity  
 effgr005\_g Maximum efficiency for gravity irrigated land in the Big Lost River entity  
 effgr008\_g Maximum efficiency for gravity irrigated land in the Blaine Co entity  
 effgr009\_g Maximum efficiency for gravity irrigated land in the Burgess entity  
 effgr010\_g Maximum efficiency for gravity irrigated land in the Burley entity  
 effgr011\_g Maximum efficiency for gravity irrigated land in the Butte/Market Lake entity  
 effgr012\_g Maximum efficiency for gravity irrigated land in the Canyon entity  
 effgr014\_g Maximum efficiency for gravity irrigated land in the Blackfoot entity  
 effgr015\_g Maximum efficiency for gravity irrigated land in the Dewey entity  
 effgr016\_g Maximum efficiency for gravity irrigated land in the Egin entity  
 effgr018\_g Maximum efficiency for gravity irrigated land in the Falls entity  
 effgr019\_g Maximum efficiency for gravity irrigated land in the Fort Hall entity  
 effgr020\_g Maximum efficiency for gravity irrigated land in the Harrison entity  
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 effgr025\_g Maximum efficiency for gravity irrigated land in the Little Wood entity  
 effgr027\_g Maximum efficiency for gravity irrigated land in the Milner entity  
 effgr028\_g Maximum efficiency for gravity irrigated land in the Minidoka entity  
 effgr029\_g Maximum efficiency for gravity irrigated land in the Mud Lake entity

effgr030\_g Maximum efficiency for gravity irrigated land in the New Sweden entity  
 effgr032\_g Maximum efficiency for gravity irrigated land in the Northside entity  
 effgr034\_g Maximum efficiency for gravity irrigated land in the Peoples entity  
 effgr035\_g Maximum efficiency for gravity irrigated land in the Progressive entity  
 effgr036\_g Maximum efficiency for gravity irrigated land in the Liberty entity  
 effgr037\_g Maximum efficiency for gravity irrigated land in the Reno entity  
 effgr038\_g Maximum efficiency for gravity irrigated land in the Rexburg entity  
 effgr039\_g Maximum efficiency for gravity irrigated land in the Chester entity  
 effgr040\_g Maximum efficiency for gravity irrigated land in the Oakley entity  
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 effgr051\_g Maximum efficiency for gravity irrigated land in the Dubois entity  
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 effgr056\_g Maximum efficiency for gravity irrigated land in the Sugar City entity  
 effgr057\_g Maximum efficiency for gravity irrigated land in the Blackfoot-Chubbuck entity  
 effgr058\_g Maximum efficiency for gravity irrigated land in the American Falls 2 entity  
 effgr059\_g Maximum efficiency for gravity irrigated land in the Gooding-Richfield entity  
 effgr501\_g Maximum efficiency for gravity irrigated land in Ground Water entity 501  
 effgr502\_g Maximum efficiency for gravity irrigated land in Ground Water entity 502  
 effgr503\_g Maximum efficiency for gravity irrigated land in Ground Water entity 503  
 effgr504\_g Maximum efficiency for gravity irrigated land in Ground Water entity 504  
 effgr505\_g Maximum efficiency for gravity irrigated land in Ground Water entity 505  
 effgr506\_g Maximum efficiency for gravity irrigated land in Ground Water entity 506  
 effgr507\_g Maximum efficiency for gravity irrigated land in Ground Water entity 507  
 effgr508\_g Maximum efficiency for gravity irrigated land in Ground Water entity 508  
 effgr509\_g Maximum efficiency for gravity irrigated land in Ground Water entity 509  
 effgr600\_g Maximum efficiency for gravity irrigated land in Ground Water entity 600  
 effsp000\_g Maximum efficiency for sprinkler irrigated land in the null entity  
 effsp001\_g Maximum efficiency for sprinkler irrigated land in the A&B entity  
 effsp002\_g Maximum efficiency for sprinkler irrigated land in the Aberdeen-Springfield entity  
 effsp005\_g Maximum efficiency for sprinkler irrigated land in the Big Lost River entity  
 effsp008\_g Maximum efficiency for sprinkler irrigated land in the Blaine Co entity  
 effsp009\_g Maximum efficiency for sprinkler irrigated land in the Burgess entity  
 effsp010\_g Maximum efficiency for sprinkler irrigated land in the Burley entity  
 effsp011\_g Maximum efficiency for sprinkler irrigated land in the Butte/Market Lake entity  
 effsp012\_g Maximum efficiency for sprinkler irrigated land in the Canyon entity  
 effsp014\_g Maximum efficiency for sprinkler irrigated land in the Blackfoot entity  
 effsp015\_g Maximum efficiency for sprinkler irrigated land in the Dewey entity  
 effsp016\_g Maximum efficiency for sprinkler irrigated land in the Egin entity  
 effsp018\_g Maximum efficiency for sprinkler irrigated land in the Falls entity  
 effsp019\_g Maximum efficiency for sprinkler irrigated land in the Fort Hall entity

effsp020\_g Maximum efficiency for sprinkler irrigated land in the Harrison entity  
 effsp022\_g Maximum efficiency for sprinkler irrigated land in the Idaho entity  
 effsp025\_g Maximum efficiency for sprinkler irrigated land in the Little Wood entity  
 effsp027\_g Maximum efficiency for sprinkler irrigated land in the Milner entity  
 effsp028\_g Maximum efficiency for sprinkler irrigated land in the Minidoka entity  
 effsp029\_g Maximum efficiency for sprinkler irrigated land in the Mud Lake entity  
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 effsp036\_g Maximum efficiency for sprinkler irrigated land in the Liberty entity  
 effsp037\_g Maximum efficiency for sprinkler irrigated land in the Reno entity  
 effsp038\_g Maximum efficiency for sprinkler irrigated land in the Rexburg entity  
 effsp039\_g Maximum efficiency for sprinkler irrigated land in the Chester entity  
 effsp040\_g Maximum efficiency for sprinkler irrigated land in the Oakley entity  
 effsp044\_g Maximum efficiency for sprinkler irrigated land in the Montevue entity  
 effsp051\_g Maximum efficiency for sprinkler irrigated land in the Dubois entity  
 effsp052\_g Maximum efficiency for sprinkler irrigated land in the Small entity  
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 effsp055\_g Maximum efficiency for sprinkler irrigated land in the Labelle entity  
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 effsp057\_g Maximum efficiency for sprinkler irrigated land in the Blackfoot-Chubbuck entity  
 effsp058\_g Maximum efficiency for sprinkler irrigated land in the American Falls 2 entity  
 effsp059\_g Maximum efficiency for sprinkler irrigated land in the Gooding-Richfield entity  
 effsp501\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 501  
 effsp502\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 502  
 effsp503\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 503  
 effsp504\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 504  
 effsp505\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 505  
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 effsp508\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 508  
 effsp509\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 509  
 effsp600\_g Maximum efficiency for sprinkler irrigated land in Ground Water entity 600  
 dpin000 Deep percolation fraction for inefficient loss for irrigated land in the null entity  
 dpin001 Deep percolation fraction for inefficient loss for irrigated land in the A&B entity  
 dpin002 Deep percolation fraction for inefficient loss for irrigated land in the Aberdeen-Springfield entity  
 dpin005 Deep percolation fraction for inefficient loss for irrigated land in the Big Lost River entity  
 dpin008 Deep percolation fraction for inefficient loss for irrigated land in the Blaine Co entity  
 dpin009 Deep percolation fraction for inefficient loss for irrigated land in the Burgess entity  
 dpin010 Deep percolation fraction for inefficient loss for irrigated land in the Burley entity

dpin011 Deep percolation fraction for inefficient loss for irrigated land in the Butte/Market Lake entity

dpin012 Deep percolation fraction for inefficient loss for irrigated land in the Canyon entity

dpin014 Deep percolation fraction for inefficient loss for irrigated land in the Blackfoot entity

dpin015 Deep percolation fraction for inefficient loss for irrigated land in the Dewey entity

dpin016 Deep percolation fraction for inefficient loss for irrigated land in the Egin entity

dpin018 Deep percolation fraction for inefficient loss for irrigated land in the Falls entity

dpin019 Deep percolation fraction for inefficient loss for irrigated land in the Fort Hall entity

dpin020 Deep percolation fraction for inefficient loss for irrigated land in the Harrison entity

dpin022 Deep percolation fraction for inefficient loss for irrigated land in the Idaho entity

dpin025 Deep percolation fraction for inefficient loss for irrigated land in the Little Wood entity

dpin027 Deep percolation fraction for inefficient loss for irrigated land in the Milner entity

dpin028 Deep percolation fraction for inefficient loss for irrigated land in the Minidoka entity

dpin029 Deep percolation fraction for inefficient loss for irrigated land in the Mud Lake entity

dpin030 Deep percolation fraction for inefficient loss for irrigated land in the New Sweden entity

dpin032 Deep percolation fraction for inefficient loss for irrigated land in the Northside entity

dpin034 Deep percolation fraction for inefficient loss for irrigated land in the Peoples entity

dpin035 Deep percolation fraction for inefficient loss for irrigated land in the Progressive entity

dpin036 Deep percolation fraction for inefficient loss for irrigated land in the Liberty entity

dpin037 Deep percolation fraction for inefficient loss for irrigated land in the Reno entity

dpin038 Deep percolation fraction for inefficient loss for irrigated land in the Rexburg entity

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dpin040 Deep percolation fraction for inefficient loss for irrigated land in the Oakley entity

dpin044 Deep percolation fraction for inefficient loss for irrigated land in the Montevue entity

dpin051 Deep percolation fraction for inefficient loss for irrigated land in the Dubois entity

dpin052 Deep percolation fraction for inefficient loss for irrigated land in the Small entity

dpin053 Deep percolation fraction for inefficient loss for irrigated land in the Howe entity

dpin055 Deep percolation fraction for inefficient loss for irrigated land in the Labelle entity

dpin056 Deep percolation fraction for inefficient loss for irrigated land in the Sugar City entity

dpin057 Deep percolation fraction for inefficient loss for irrigated land in the Blackfoot-Chubbuck entity

dpin058 Deep percolation fraction for inefficient loss for irrigated land in the American Falls 2 entity

dpin059 Deep percolation fraction for inefficient loss for irrigated land in the Gooding-Richfield entity

dpin501 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 501

dpin502 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 502

dpin503 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 503

dpin504 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 504

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dpin506 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 506

dpin507 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 507

dpin508 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 508

dpin509 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 509

dpin600 Deep percolation fraction for inefficient loss for irrigated land in Ground Water entity 600  
 dpex000 Deep percolation fraction for excess water for irrigated land in the null entity  
 dpex001 Deep percolation fraction for excess water for irrigated land in the A&B entity  
 dpex002 Deep percolation fraction for excess water for irrigated land in the Aberdeen-Springfield  
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 dpex005 Deep percolation fraction for excess water for irrigated land in the Big Lost River entity  
 dpex008 Deep percolation fraction for excess water for irrigated land in the Blaine Co entity  
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 dpex057 Deep percolation fraction for excess water for irrigated land in the Blackfoot-Chubbuck  
 entity  
 dpex058 Deep percolation fraction for excess water for irrigated land in the American Falls 2 entity  
 dpex059 Deep percolation fraction for excess water for irrigated land in the Gooding-Richfield entity  
 dpex501 Deep percolation fraction for excess water for irrigated land in Ground Water entity 501



dpex502 Deep percolation fraction for excess water for irrigated land in Ground Water entity 502  
dpex503 Deep percolation fraction for excess water for irrigated land in Ground Water entity 503  
dpex504 Deep percolation fraction for excess water for irrigated land in Ground Water entity 504  
dpex505 Deep percolation fraction for excess water for irrigated land in Ground Water entity 505  
dpex506 Deep percolation fraction for excess water for irrigated land in Ground Water entity 506  
dpex507 Deep percolation fraction for excess water for irrigated land in Ground Water entity 507  
dpex508 Deep percolation fraction for excess water for irrigated land in Ground Water entity 508  
dpex509 Deep percolation fraction for excess water for irrigated land in Ground Water entity 509  
dpex600 Deep percolation fraction for excess water for irrigated land in Ground Water entity 600  
wilt000 Wilting point for irrigated land in the null entity  
wilt001 Wilting point for irrigated land in the A&B entity  
wilt002 Wilting point for irrigated land in the Aberdeen-Springfield entity  
wilt005 Wilting point for irrigated land in the Big Lost River entity  
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## **Appendix D; Color Ramp for Pie Diagrams**



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 ■ THREEEP  
 ■ TUCKER  
 ■ RANGEN  
 ■ NTLFSHH  
 ■ THOUSAND  
 ■ D045011  
 ■ D045012  
 ■ SAND  
 ■ D047011  
 ■ BOX  
 ■ BANBURY  
 ■ ASH\_REX  
 ■ BRIGGS  
 ■ HEISE\_SHEL  
 ■ CLEARLK  
  
 ■ D050014  
 ■ D051014  
 ■ NIAGARA  
 ■ CRYSTAL  
 ■ D057020  
 ■ D058020  
 ■ ELISON  
 ■ D059021  
 ■ D059022  
 ■ D061023  
 ■ D062023  
 ■ BLUELK  
 ■ D064026  
 ■ D065027  
 ■ DEVILC  
 ■ DEVILW  
 ■ D068029  
 ■ D069029  
 ■ D070030  
 ■ SHELNRBLKF  
 ■ NRBLKFMIN

## **Appendix E; ESHMC Review Comments and IDWR Responses**

## Comments from Chuck Brendecke

The procedure that was used is termed “predictive analysis” by Doherty and I think it’s important to maintain the fine points of the distinctions between predictive analysis, predictive uncertainty (which is a larger topic) and model uncertainty (which is larger still). Otherwise there is a risk that the reader will view the predictive analysis as the whole story.

**IDWR response: Partial accept. We recognize that our analysis is not the whole story, and will enhance our discussion of its shortcomings, but pg 27 of Doherty and others (2010) includes a discussion of the maximization/minimization technique, so it seems to us that it is a legitimate predictive uncertainty analysis.**

The last sentence of the abstract proposes the filtered/unfiltered analysis to “try and reduce” the uncertainty identified in the analysis. It seems to be that “evaluate the impact of data noise on” would be a better phrase. The former suggests that our goal is more to improve the optics than it is to get a complete understanding.

**IDWR response: Accept.**

Chuck

Charles M. Brendecke, PhD, PE

Principal

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## Comments from Lyle Swank

Allan,

Here are a couple of comments from the WD100, WD110 and WD120 areas that were forwarded to me. My thoughts on the various steady state vs. steady flow and transient conditions are included also. Although we are late with the comments, I hope these comments are valuable and worthwhile.

### 1) Centroid Location:

There is a concern in the methodology of the uncertainty analysis of the first parameter of the report. "Identify the centroid of the irrigated lands within the water district."

Some centroids near a reach of the river may not be a good representation of the entire water district. Specifically WD120 and 100 have a Centroid that is in close proximity to the river reaches. This could skew the accuracy of the analysis.

My understanding of the Centroid is that it is defined by the irrigated lands within the water district. Perhaps it would be more accurate to create a centroid based on an equidistance of travel time to river from wells. This would pull the Centroid away from the river reach and place it in a better represented location of the average flow time in the water district.

Scott Bergendorf  
Water Right Agent,  
WD100, WD110, WD120

James Cefalo  
WD100, WD110, WD120  
Watermaster

**IDWR Response: Partial accept. We will add a discussion stating that we are using water districts to position centroids so that we have a wide geographic distribution of stress locations, not so that we can assign uncertainty to a particular water district. We chose the centroid of the irrigated lands rather than the geographic center so that the stress would be applied in an irrigated area not in an un-irrigated area. Much of irrigated land is near the Snake River, so we would have been concerned if none of the centroids had been near the river.**

2) Models are most accurate when they are representing either Steady-State/Steady Flow or a more transient condition. For a transient condition such as the timing of a runoff, the time period can be critically important. Because ESPAM V.2 is modeling a change in water table levels over years, it has elements of both steady state/steady flow and transient properties. Within the highly variable years, you have time periods when the groundwater is being replenished by surface water flows and time periods when surface water is being replenished by groundwater depending on the water table at the time of the year. Not all reaches of the Snake River will change with the same level of flood or drought. This changing gain/loss and how various reaches change based on the "communication" of the groundwater to surface water is still not well understood. Until these timing issues and groundwater levels are better understood, there are limits to how well the ESPAM V.2 can be used to model conditions ranging from flood to drought within long periods of records. There is an obvious uncertainty

band width to go along with these unknowns especially in the upper Snake River portion above the Snake River Neeley gage.

**IDWR Response: Accept. There is uncertainty regarding the timing of when reaches of the river are gaining and losing. Unfortunately the reach gain and loss data that we use contain significant noise (see Figure 3). This analysis appears to identify the noisy reach gain and loss data as a weakness. I will add a discussion stating that even when filtered, the timing will remain a weakness until the source of the noise in the reach-gain data can be identified and removed.**

Lyle Swank, P.E.

Watermaster WD01

900 N. Skyline

Idaho Falls, Id. 83402

## Comments from Dave Colvin

---

Excellent summary of the dual calibration process. I believe you said it in a more concise, comprehensive, and understandable way than Doherty himself! Can I quote you in the future?

I am a little concerned that people will read the abstract, the summary, and nothing else. That's not necessarily a comment on the report itself, but rather a concern with the audience.

I was left wanting a little more explanation of the difference between predictive uncertainty analysis, and different types of error analysis. Is there a way to summarize or at least reference the issues presented

in <http://www.idwr.idaho.gov/Browse/WaterInfo/ESPAM/ESHMC%20Updated%20White%20Paper/> ?

The main issues I'd like to see brought up are the sources of uncertainty, the spatial/temporal variability of these uncertainty sources, and which of these uncertainty sources are evaluated by the constrained minimization/maximization method. I think that characterizing the dual calibration approach as predictive uncertainty analysis is a bit of a stretch, but I understand your dilemma in how to explain this to such a wide audience.

### **IDWR Response: Accept.**

You allude to the benefit that uncertainty analysis gives to identifying the adjustable parameters that need additional information collected for. I personally think that this is the greatest benefit of uncertainty analysis, but of course everyone always focuses on the "predictive" uncertainty results. If you agree, could you make an abstract and/or summary statement somewhere that the original calibration result is the most probable given the available data, and that the predictive uncertainty result ranges necessarily rely on models that have a poorer calibration?

I also have some minor comments:

1. Page 3, second paragraph: "...18% (3/17) of the uncertainty analyses identified predictions with uncertainty greater than 0.10. Interestingly all the predictions with high uncertainty evaluated..."  
If someone reads this independent of the rest of the report, I'm not sure they'll understand what 0.10 means. Maybe include something similar to page 8, paragraph 4 explanation?

### **IDWR Response: Accept.**

2. Page 10, paragraphs 2, 3, and 4: The descriptions of why these results had small ranges seems to imply that the uncertainty analysis was deficient in some, way, which maybe it was. But couldn't it also be explained that the available observation data constrain the calibration results so that ESPAM 2.0 is actually an excellent predictor at these locations?

**IDWR Response: Accept. We are puzzled, the descriptions were supposed to imply that the data constrained the calibration, we will firm up that discussion.**



Dave Colvin, P.G. | Hydrogeologist / Project Manager | Leonard Rice Engineers

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## Comments from Bryce Contor

**From:** bcontor.rm@gmail.com on behalf of Bryce Contor  
[bcontor@rockymountainenvironmental.com]

**Sent:** Thursday, November 01, 2012 8:25 PM

**To:** Wylie, Allan

**Cc:** Blew, David; Chuck Brockway; chuck.brendecke; Dave Colvin; David Hoekema; David Kampwerth; Greg Sullivan; Gregg S. Ten Eyck; Hal Anderson; J. D. May; Jack Harrison; Janak Timilsena; Jeff Sondrup; Jennifer Johnson; Jim Bartolino; Jim Brannon; John Koreny; John Lindgren; Johnson, Gary; Jon Bowling; Ken Skinner; Linda Lemmon

**Subject:** Uncertainty report

Allan -

I realize the report is final and that I am delinquent in my single comment:

On page 9 the report states

"It is only after the impact differences (range) becomes large, say 0.10 or greater, that the uncertainty becomes a practical issue."

The practical effect of a difference in modeled results depends entirely upon the administrative question to which the model is applied. My understanding from both Jeff Peppersack and Shelley Keen is that there is no de minimus consideration for mitigation requirements for new water rights. Our experience has been that sometimes large mitigation events are required to satisfy very small modeled requirements. Even with groundwater transfers, when the modeled effects are just barely over the de minimus threshold, it often requires mitigation of many tens of acre feet per trimester to satisfy single-digit modeled impacts. While doubling a single-digit effect seems trivial, the resultant doubling of a large mitigation effort may not be trivial.

**IDWR Response: Accept. We will adjust the paragraph to point out that, from a model development perspective, uncertainty will always exist. The model weaknesses we are looking for with the analyses are large.**

I apologize for not getting this to you sooner.

Bryce

--

Bryce A. Contor

Senior Hydrologist

482 Constitution, Idaho Falls, ID 83402

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